



Attachment

Appendix 10

***High Voltage Overhead
Transmission to Scope Book
(Exhibit A)***

for

2021 Request for Proposals

for
Build-Own-Transfer Acquisition
Agreement

~~Solar Photovoltaic Resources~~

Entergy Louisiana, LLC

~~March 10,~~[July 29], 2021 ~~DRAFT~~

CONFIDENTIAL

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1. INTRODUCTION¹

1.1 Purpose

This ~~Attachment~~Appendix 10 to the Scope Book (“(this ~~Attachment~~“Appendix 10”) provides design requirements and reference material for the design of the high voltage (“HV”) (69 kV and above) overhead transmission lines that will be built and/or connected to the Entergy transmission system by or for Seller as part of the Project (“Transmission Lines”). This document pertains to the transmission line between the collector substation and the deadend structure delivered by the GIA. This document is intended to provide to Seller and others acting at Seller’s request requirements, recommendations, and guidance in the planning, design, construction, asset management, use, and operation of the Transmission Lines.

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1.2 Scope

This ~~Attachment~~Appendix 10 applies to all Transmission Lines.

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This ~~Attachment~~Appendix 10 primarily describes technical requirements, both performance-based and prescriptive for the design and installation of the Transmission Lines. Refer to the Scope Book and other parts of the Agreement for information regarding project sequencing and milestones, the project execution plan, project schedule and schedule management, project controls reporting, health and safety information, factory acceptance tests, training, required submittals, design reviews, equipment records, specified deliverables, project documentation, and other relevant matters not covered by this ~~Attachment~~Appendix 10.

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1.3 General Data

This ~~Attachment~~Appendix 10 addresses aspects of the Work relating to the Transmission Lines. It is not intended to be, and shall not be construed to be, a comprehensive list of each and every element or other requirement applicable to the Work and shall in no way limit Seller’s obligations under the Agreement or any Ancillary Agreement. Without limiting the other terms of the Agreement or any Ancillary Agreement, in performing the Work relating to the Transmission Lines, Seller shall comply with, and cause its Contractors and Subcontractors to comply with, the terms of this ~~Attachment~~Appendix 10, all Laws (including codes) and applicable Permits, and the other elements of the Performance Standard.

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This ~~Attachment~~Appendix 10 provides the minimum functional specification (“MFS”) for the Transmission Lines, including scope and design requirements. In addition to the requirements set

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¹ **NTD:** The document remains subject in all respects to Buyer’s continued due diligence and internal review (including by Buyer’s subject matter experts). This draft may need to be revised to reflect certain matters included or not addressed in the Agreement or the RFP or that have been reconsidered. ELL reserves the right to issue an updated version of this document.

forth in the Agreement (including the Scope Book), the Transmission Lines shall comply with all requirements specified in the GIA or any other Required Deliverability Arrangement.

This AttachmentAppendix 10 is part of the Scope Book.

Article, Section, Table, Figure, and Attachment references in this AttachmentAppendix 10 are to this AttachmentAppendix 10 unless otherwise provided or the context otherwise requires.

⁴ The document remains subject in all respects to Buyer's continued due diligence and internal review (including by Buyer's subject matter experts). This draft may need to be revised to reflect certain matters included or not addressed in the Agreement or the RFP or that have been reconsidered. ELL reserves the right to issue an updated version of this document.

1.4 Changes in this Revision

Document created 02/03/26/2021.

1.5 Deviations

Any deviations from the MFS for the Transmission Lines or the terms of this AttachmentAppendix 10 shall require Buyer's prior approval and will be subject to the terms of the Agreement.

2. DEFINITIONS

2.1 Definitions

2.1.1 BIL - Basic Lightning Impulse Insulation Level is a reference insulation level in terms of the crest voltage of a standard lightning impulse.

2.1.2 Conductor Displacement

With respect to clearances, conductor displacement is the conductor movement, including the effects of insulator swing and structure deflection, due to a prescribed ice, wind, or thermal load case.

With respect to right-of-way ("ROW") determinations, conductor displacement is the maximum horizontal conductor displacement from its initial unloaded position, including the effects of insulator swing and structure deflection due to the extreme wind load case. See also (W_{CD}) in Figure 6.3.4.1-3.

2.1.3 Conductor Movement Envelope

With respect to clearances, the conductor movement envelope is the full range of conductor positions in the prescribed ice, wind, or thermal load cases.

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With respect to ROW determinations, the conductor movement envelope is the full range of conductor movement, including the effects of insulator swing and structure deflection due to the extreme wind load case applied from both directions, and including the initial effective structure width. See also (WCME) in Figure 6.3.4.1-3.

2.1.4 Designer – Individual (in-house or contractor) responsible for analyzing and selecting transmission line components, structures, or foundations.

2.1.5 Effective Structure Width – the width between a structure’s outboard conductors (e.g., for an H-frame configuration, it is twice the phase spacing, and for a vertical conductor configuration it is effectively zero). See also (wS) in Figure 6.3.4.1-3.

2.1.6 LIDAR (Light Detection and Ranging) – A method of detecting and determining the position, velocity, or other characteristics of distant objects by analysis of pulsed laser light reflected from the surfaces of such objects.

2.1.7 Meridian – Electronic document management system used to archive transmission standards and documents and track revisions.

2.1.8 PLS-CADD – A software package used during optimization of pole spotting, design analysis, and the development of material lists.

2.1.9 Vegetation Management Width – Right of way width outside of the conductor movement envelope, purchased solely for establishment of a vegetation management cycle. See (WVM) in Figure 6.3.4.1-1 and Figure 6.3.4.1-2.

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2.2 Acronyms and Abbreviations

ACAR Aluminum Conductor Alloy Reinforced

ACCC Aluminum Conductor Composite Core

ACCR Aluminum Conductor Composite Reinforced

ACSR Aluminum Conductor Steel Reinforced

ACSS Aluminum conductor Steel Supported

BIL Basic Lightning Impulse Insulation Level

EPRI Electric Power Research Institute

FAA Federal Aviation Administration

FAD Foundation Analysis & Design

GFD Ground Flash Density

IEEE Institute of Electrical and Electronics Engineers

LIDAR Light Detection and Ranging

MFAD Moment Foundation Analysis & Design

MVATD Minimum Vegetation Action Threshold Distance

MVCD Minimum Vegetation Clearance Distance

NESC National Electrical Safety Code

OCF Overload Capacity Factor

ROW Right of Way

SRF Strength Reduction Factor

UBS Ultimate Breaking Strength

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3.1 Industry Standards

ASCE MOP 91	Design of Guyed Electrical Transmission Structures
ASCE MOP 123	Prestressed Concrete Transmission Pole Structures
ASCE 48	Design of Steel Transmission Pole Structures
ASCE 74	Guidelines for Electrical Transmission Line Structural Loading
ANSI C2	National Electric Safety Code (NESC)
IEEE Std 80	IEEE Guide for Safety in AC Substation Grounding
IEEE Std 524	Guide to the Installation of Overhead Transmission Line Conductors
IEEE Std 738	Standard for Calculating the Current-Temperature of Bare Overhead Conductors
IEEE Std 1313.2	Guide for the Application of Insulation Coordination
IEE Std 1542	Guide for Installation, Maintenance, and Operation of Irrigation Equipment Located Near or Under Power Lines
APLIC 2012	Reducing Avian Collisions with Power Lines – State of the Art– 2012
APLIC 2006	Suggested Practices for Avian Protection on Power Lines
NACE RP0177	Mitigation of Alternating Current and Lightning Effects of Metallic Structures and Corrosion Control System
OSHA Std 2207, Part 1926	Safety and Health Regulations for Construction
IEEE 738	Standard for Calculating Current-Temperature Relationship of Bare Conductors
IEEE Std.- 1243-1997	Guide for Improving the Lightning Performance of Transmission Lines
EPRI	Handbook for Improving Overhead Transmission Line Lightning Performance
EPRI	AC Transmission Line Reference Book - 200kV and Above
EPRI	Guide for Transmission Line Grounding
EPRI	Outline of Guide for Application of Transmission Line Surge Arrestors – 42 to 765 kV

	Pre-stressed Concrete Institute Guide Specifications
	FAA Advisory Circular AC 70/7460-1K, Obstruction Marking and
	Lighting

The latest issued Standards and Codes at the issuance of the effective date of the Agreement shall be used. Earlier editions are not allowed unless specifically identified in this [AttachmentAppendix 10](#).

If a revision to a standard or code is issued, it is not required to be implemented unless the Authority Have Jurisdiction (AHJ) has adopted it, in which case, ~~the~~ Seller is obligated to any increased compliance above what is required by the Standards and Codes at the effective date of the Agreement. This risk is ~~to be~~ borne by ~~the~~ Seller.

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3.1.1 Materials

Seller shall use the descriptions of materials set out in the standard drawings provided in ~~Attachment~~ ~~Attachment 1~~ along with the Approved Vendor List in ~~Attachment 5~~ ~~Attachment 5~~ to procure the equipment, materials, systems, and other items required for the development, engineering, design, procurement, construction, testing, commissioning, use, and operation of the Transmission Lines in accordance with the terms of the Agreement.

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4. SAFETY AND ENVIRONMENT

4.1 Safety

The safety of individuals, the Project, and other life or property in the development, engineering, design, procurement, construction, testing, commissioning, use, and operation shall be the Designer's highest priority.

4.2 Avian Design

The primary issues to consider for avian protection on transmission lines are clearances, marking, and nests. Transmission clearances for all voltages shall exceed the established minimums, shown in ~~Attachment 2~~Attachment 2. Where Entergy standard structure configurations, shown in ~~Attachment 1~~Attachment 1, are used, the design will meet the guidelines. Marking of wires is addressed in ~~Section 7.13.4~~ and is to be done only in areas where such marking is required by authorized wildlife agencies, Laws, or applicable Permits.

4.3 Future Impacts

Proper consideration shall be given to working space and access during siting to address direct impacts on both work safety and the need for environmental remediation. Similarly, proper consideration shall be given to the ability to re-conductor a line vs. rebuilding to address the potential considerable ecological benefits.

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5. LOAD COMBINATIONS

5.1 Loading Combinations

This section covers the transmission line load cases and load case combinations to be used in the design of the Transmission Lines for the Project. It also includes the Overload Capacity Factors (“OCF”) and Strength Reduction Factors (“SRF”) used to calculate forces on the individual components of each structure within the Transmission Lines. The load combinations below are consistent with the loading requirements of NESC Rule-250; however, the boundaries for loading areas have been shifted from those in NESC Rule-250. All references to NESC 250B, 250C, and 250D refer to the District Loading, Extreme Wind, and Concurrent Ice and Wind as modified based on these shifts in loading areas.

5.1.1 District Maps

Based on the NESC figures, districts were established along county and parish boundaries which envelope the NESC requirements. These boundaries were further modified to address other commitments and past operating experience. Notably, several coastal parishes and counties have design wind speeds increased to 140 mph to address hardening study recommendations and other commitments; roughly the NW half of Arkansas has been treated as NESC Heavy rather than NESC Medium based upon past operating experience and design practice; and the 1” ice loading was extended throughout Arkansas and much of northern Mississippi based on extensive damage from past ice storms. They are collectively presented as Attachment 6 illustrating the enveloping districts as follows:

Transmission Line Designers shall use the most conservative loading requirements required along the entire line if the line crosses several counties or parishes requiring different loadings. Exception to this requirement may be taken where a containment structure is placed at the district boundary.

5.1.2 Load Cases - Summary

Table-5.1.12 summarizes the various load cases used to design and analyze structures.

Table-5.1.12 – Structural Load Cases

Description	Wind Loading	Ice Loading	Temperature	NESC Ref.
NESC 250B District Loading				
Heavy	4 psf	0.50 in.	0°F (-20°C)	250B, Table 250-1
Medium	4 psf	0.25 in.	15°F (-10°C)	250B, Table 250-1
Light	9 psf	0.00 in.	30°F (-1°C)	250B, Table 250-1

5.1.7 Single Dead-End and Failure Containment (Dead-End Structures)

All wires up, One Side Only Loading, Initial or Final Condition using the Structural Load Cases in Table 5.1.12.

5.1.8 Stringing Longitudinal Unbalanced Load (Tangents & Run. Angles)

0 mph Wind & 0" Ice, 60°F (15°C), Initial (Everyday Loads) with 3000-lb. Longitudinal Force (1000 lb. per phase) or with 2000 lb. Longitudinal Force per conductor (H-Frames only).

5.1.9 Pole without Conductors (NESC 261A1c) (Guyed Poles)

Extreme Wind applied on pole in any direction.

5.1.10 Stringing loads on Dead-Ends

Everyday loads on one side only (0 mph wind, 0" ice, 60F (15C), Initial.

5.1.11 PLS Wind Direction for Structure Loading

Designers shall conservatively use wind applied normal to all spans simultaneously when selecting structures for new designs.

5.2 Load Cases – Clearance Verification

The following clearance load cases shall be included to check vertical and horizontal clearances. "Line Design Clearances" are shown in Attachment 2, Attachment 2.

Table 5.2.1 – Clearance Load Cases

Description	Wind Loading	Ice Loading	Temp.	NESC Ref.	Condition	Clearance Check
Max. Temp. (ACSR)	0 psf	0 in.	212°F (100°C)	232A	Final	Vertical Clearance
Max. Temp (ACSS & ACCC)	0 psf	0 in.	347°F (175°C)	232A	Final	Vertical Clearance
Max. Temp (ACAR)	0 psf	0 in.	176°F (80°C)	232A	Final	Vertical Clearance
NESC Zone				230B, Table 230-1, Table 230-2		
Heavy	4 psf	0.5 in.	0°F (-20°C)	230B, Table 230-1, Table 230-2	Final	
Heavy Ice	0 psf	1.0in	32°F (0°C)	232A	Final	Vertical clearance to ground, other

~~(2)~~ (2) Support hardware includes bolts and plates supporting davit arms, braced post and post insulators, brackets, suspension tees and other miscellaneous supports not supporting conductor or shield wire dead-ends. The reduction factors shown are multiplied by the ultimate strength of the part as indicated by the manufacturer.

~~(3)~~ (3) Dead-end fittings include bolts and dead-end tees used to dead-end conductors and shield wires. The manufacturer generally gives the ultimate strength of the tees. This value is then reduced by the reduction factor shown.

The “minimum tensile strength” shown for bolts by the Vendor is the allowable tensile load that shall be used on the bolt without the combined load of shear produced in a guyed structure. These loads are not reduced by the reduction factor; however, the shear values given shall be reduced depending on the actual tensile stress, in accordance with the interaction equation.

~~(4)~~ (4) NESC 2017

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6. CLEARANCE AND RIGHT OF WAY REQUIREMENTS

This section covers vertical and horizontal clearance requirements for the Transmission Lines, which include NESC vertical and horizontal clearance requirements from Section 23 of the 2017 Code or counterpart for subsequent codes for HV transmission lines in Entergy's Service Area plus an added safety buffer, as described below.

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6.1 Vertical Clearance – Over Ground

NESC and Entergy vertical clearances over various ground surfaces are shown in Attachment 2-Attachment 2. These clearances are based on the 2017 Code, Table 232-1, with the voltage adder defined in Rule 232C1a, using the sags calculated under Rules 232A2 and 232A3.

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See Section 5.2Section 5.2 for Clearance Load Cases.

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The actual clearance to ground shall be based on the measurement to ground at the low point in the line as determined when the line is at maximum sag. For purposes of determining the required clearance for the Transmission Lines,

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NESC Clearance = Table 232-1 Clearance + Voltage Adder (.4"/kV in excess of 22kV)

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Entergy-Required Minimum Clearance = NESC Clearance + Safety Buffer

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NESC provides consideration for clearances over water surfaces, including floodwaters. Footnotes 17-21 to Table 232-1 shall be carefully considered when determining necessary clearances. For flood-prone areas that do not typically have standing surface water and are not subject to USACE or other permits, the normal flood level (10-year flood level) shall be considered along with required clearances for areas not suitable for boating. For most spans over such areas, clearances that consider or are based on vehicle access with un-flooded ground surfaces will continue to apply. Lines leading into generating facilities, EHV interconnections, or other lines where increased reliability is desired shall consider less frequent flood events (e.g., 50-year floods or 100-year floods) to avoid potential service interruptions. Such lines shall be designed to higher flood levels where the incremental costs are justified and will generally be compared to NESC requirements for water surface not suitable for sailboats.

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6.2 Other Vertical Clearances

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6.2.1 Supply Conductors (69 kV and above)

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6.2.2 NESC and Entergy vertical clearances between various electricity supply lines and non-current carrying wires are also shown in Attachment 2-Attachment 2. These clearances are based on the 2017 Code, Table 233-1, with the voltage adder defined in Rule 233C2a, using the sags calculated under Rules 233A1a (3)(b) and 233A1a (3)(c).

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The design clearance shall be measured as the distance between the field measured existing line and the design maximum sag.

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The ~~Entergy~~ Required Minimum Clearance: NESC Clearance + Safety Buffer

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~~Attachment 2 shows the minimum vertical clearances over various ground surfaces and uses.~~

Attachment 2 shows the minimum vertical clearances over various ground surfaces and uses.

The line Designer shall establish "Prohibitive Zones" with the appropriate Design Clearances on the plan profiles within PLS-CADD in the areas where ~~special crossings occur~~ these considerations occur. Considerations could be but not limited to environmental, archaeological, landowner constraints, etc.

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6.2.3 Substations

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Transmission line vertical clearances inside substations shall meet the vertical clearance requirements ~~shown in Attachment 2.~~

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6.2.4 Miscellaneous

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To every extent possible, ROW shall be selected, and ROW agreements written, to preclude structures, signage, and other miscellaneous items from being located beneath the transmission circuits. To the extent such items cannot be so precluded, the vertical clearances for the Transmission Line shall meet the basic NESC clearance requirements for each applicable clearance set forth in ~~Attachment 2, Attachment 2,~~ plus an additional 4.5 feet.

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6.3 Horizontal Clearance

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All horizontal clearances shall include the deflection of the structure and the displacement of the conductor added to the clearance requirements defined below. Clearances per ~~Section 6.3.1~~ 6.3.1 and ~~Section 6.3.2~~ 6.3.2 shall be based on the development of the clearance envelopes shown in the NESC for each situation plus 4.5 feet at a minimum. Basic NESC clearances, including horizontal clearances, are summarized in ~~Attachment 2, Attachment 2.~~

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6.3.1 Adjacent Supply Lines

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Horizontal clearances to adjacent supply lines shall be calculated using loads described in ~~Section 5.2, Section 5.2.~~ This clearance is based on an envelope as shown in NESC Figures ~~233-1, 2&3~~ and using the following loadings:

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The horizontal movement shall be calculated using the medium wind defined under Rule 233A1a(1&2) using (1) a 6 lb/sf wind at 60°F (15°C) and no ice or (2) no wind at 60°F (15°C).

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The maximum sag, Rule 233A1a(3), shall be calculated (a) using 120° F (49°C) with no wind; (b) using the max temperature; or (c) the Code Ice thickness with a temperature of 32°F (0°C) and no wind.

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PLS-CADD shall be used to define the envelope vertices and check clearance to adjacent supply lines.

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6.3.2 Adjacent Buildings and other Structures

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The required clearance between conductors and buildings or other structures is covered in Rule 234 and varies between the various structure types. The loadings used for the clearance envelopes are given in Section 5.2.5.2. The Designer shall use PLS-CADD to check these clearances after specifying the required load cases and clearances.

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6.3.3 Insulator/Conductor Swing Clearance

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Clearances to the supporting structure resulting from insulator swing are addressed in Section 8.1.8.1. Additionally, air gap clearances between adjacent circuits on different structures are to be checked under the high wind load case in Section 5.2.5.2. Minimum clearance shall be that associated for the higher voltage for the 100 mph swing clearance given in Table 8.1.2.

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6.3.4 Entry Right of Way Requirements

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6.3.4.1 Rights of Way for New Lines

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Rights of way (ROW) for new transmission lines must provide spacing sufficient to assure reliability and equipment accessibility for maintenance and construction.

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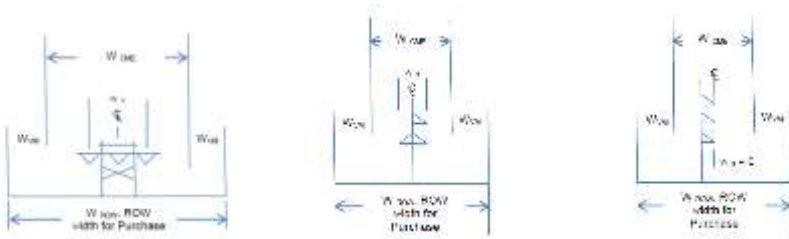
Required ROW widths for new lines must be determined considering four primary parameters: (a) the effective structure width(s), taken as the outboard conductor spacing for the structure; (b) the minimum required spacing between adjacent circuits on separate structures; (c) the conductor displacement due to wind; and (d) a vegetation management width at the edges of the ROW to allow for a cyclical growth and periodic trimming schedules. The sum of the structure widths, any additional circuit spacing dimensions, and the conductor displacements (including the effects of structure deflection, insulator swing, and conductor movement) is called the conductor movement envelope (W_{CME}). Adding the appropriate vegetation management width on each side of W_{CME} gives the minimum allowed ROW width for purchase. Note that total minimum allowed ROW widths for purchase will be rounded upward in whole 5'-increments (e.g., 161' is rounded to 165'.) The four parameters described above are illustrated for typical ROW situations in Figure 6.3.4.1-1 and Figure 6.3.4.1-2. Additional figures are found in Attachment 4.

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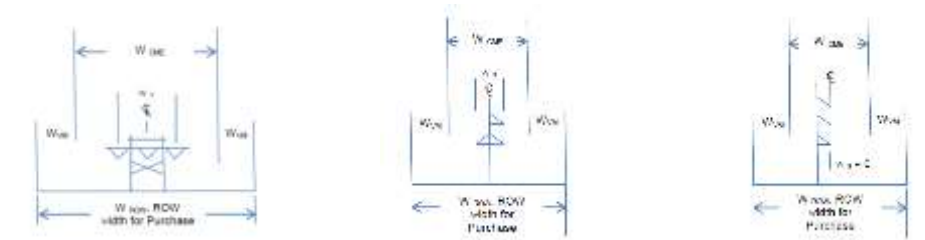
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Figure 6.3.4.1-1 – Typical Single Structure ROW



(a) H-Frame (b) Monopole Delta (c) Monopole Vertical



(a) H-Frame (b) Monopole Delta (c) Monopole Vertical

Notes: W_s = Effective Structure Width (Outboard Conductor Spacing) W_{VM} = Vegetation Management Width; W_{CME} = Width, Conductor Movement Envelope; Add Width = c/c Spacing

Figure 6.3.4.1-2 – Typical Double Structure ROW



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Table 6.3.4.2-1 – Typical Effective Structure Widths

Voltage	H-frames (ft.)	Single Pole	
		Delta/ Vert. Double Circuit (ft.)	Single Circuit Vertical (ft.)
500kV	67.66	28.00	0.00
345kV	51.00	24.00	0.00
230kV	40.00	18.00	0.00
161/138/115 kV	32.00	14.33	0.00
69kV	24.00	12.00	0.00

Note that for vertical conductor configurations, the conductors fall on the centerline of the circuit/ROW and the monopole structure itself is offset by a function of the insulator length. In such configurations there are no outboard conductors, and the effective width of the structure is treated as zero.

When determining ROW requirements for constructing a new transmission line adjacent to an existing transmission line (discussed in more detail below), the actual effective widths of the existing structure shall be determined and used in the calculation.

Adjacent Circuit Separation (W_{c-c})

Circuit center to center horizontal spacing for ROW determinations shall be as shown in Table 6.3.4.2-2 unless the Performance Standard requires use of a higher value.

Table 6.3.4.2-2 – Minimum Spacing for Adjacent Circuits (W_{c-c})

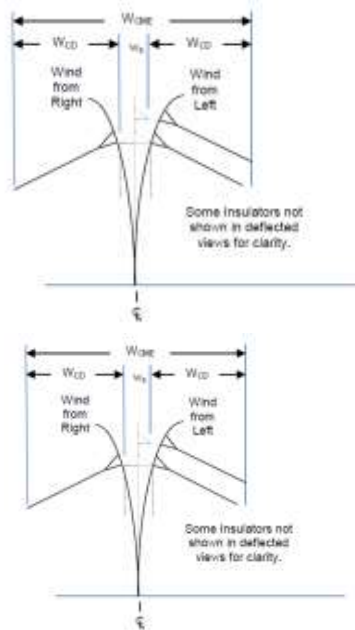
Voltage	H-frames (ft.)	Single Pole	
		Delta/ Vert. Double Circuit (ft.)	Single Circuit Vertical (ft.)
500kV	140	96	70
345kV	120	65	45
230kV	75	50	35
161/138/115 kV	60	40	30
69kV	45	30	20

For 345 kV and 500 kV Transmission Lines, the distances specified for adjacent single pole circuits reflect geometrical limits only. Electrical effects (audible noise, EMF, etc.) must be studied, and will require additional separation if indicated by the study. For two adjacent circuits of different voltage or framing, the larger of the two required separation distances shall be used.

6.3.4.3 Displaced Conductor Position (WCD)

During detailed line design, the displaced conductor positions are calculated including the effects of structure deflection and insulator/hardware swing; and using the load cases contained in Section 5.5. Wind loads are applied transversely in each direction to displace the conductor away from the centerline as illustrated below.

Figure 6.3.4.3-1-3 – Displaced Conductor Position & Relationship to W_{CME} and w_s



Notes: w_s = Effective Structure Width (Outboard Conductor Spacing) W_{CME} = Width, Conductor Movement Envelope; W_{CD} = Displaced Conductor Position Including Structure Deflection

In addition to checking required horizontal clearances per Sections ~~6.3.1~~ 6.3.1 and ~~6.3.2~~ 6.3.2, the displaced conductor position shall stay within the available conductor movement envelope under the extreme wind ~~cases~~ described in ~~Table 5.1.1-2~~. As part of the line design, pole placements and span lengths must be adjusted if required to maintain required clearances and keep the conductor within the available width.

The available CME widths in ~~Table 6.3.4-4-1~~ and ~~Table 6.3.4-5-1~~ contemplate and accommodate standard framings, typical spans, the current list of typical conductors and their specified stringing limits, etc. Markedly atypical designs may require a more rigorous evaluation of the ROW requirements. Conversely, severe ROW restrictions will likely require atypical design such as shortened spans.

Note that all tabulated values consider the use of V-string assemblies, braced-post assemblies, suspension units with struts, or other configurations where insulator swing is confined.

6.3.4.4 Vegetation Management Width (WVM)

It is assumed that trees grow or someday will grow at the edge of the ROW, and that normal growth cycles will result in further encroachment into the Vegetation Management Width. Therefore, the conductor movement envelope (CME) alone is insufficient as a ROW. Vegetation management in the area adjacent to ROW edges is required to prevent grow-in and to comply with the Minimum Vegetation Clearance Distance (MVCD see also definitions). Thus, additional width between the ROW edge and the outboard conductors is essential to allow planned, efficient vegetation management without violating the MVCD.

To accomplish this ~~Asset Management establishes~~, apply a Minimum Vegetation Action Threshold Distance (MVATD) for prioritizing corrective maintenance. The Vegetation Management Width (W_{VM}) to be used when determining ROW width shall bound the MVATD and MVCD, and is tabulated below (values for MVATD and MVCD are provided for reference):

Table ~~6.3.4-3.4-1~~ – Vegetation Management Widths

	WVM	MVATD	MVCD
Voltage	(ft.)	(ft.)	(ft.)
500kV	22.5	14.68	7.4
345kV	15.0	9.44	4.5
230kV	12.5	5.14	4.3

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161/138/115 kV	10	3.42 / 2.94 / 2.45	2.9 / 2.4 / 2.0
69kV	7.5	2.45	1.2

Where a circuit is to be built at a given voltage but operated at a lower voltage, the W_{VM} for the higher voltage shall be used to determine ROW width.

6.3.4.5 Calculation of Minimum Allowed ROW Width for Purchase - New Single -Circuit Line or Double Circuit on the Same Structures

As illustrated in the preceding figures, at any given point, the minimum allowed ROW shall equal the applicable CME plus the applicable vegetation management width (W_{VM}) on each side of the ROW. Assuming multiple circuits are the same voltage, standard ROW widths are determined as:

$$ROW = W_{CME} + 2(W_{VM}) - f, \text{ rounded up to the next whole 5' increment}$$

and are tabulated by voltage and framing type in Table 6.3.4-5-1 and Table 6.3.4-5-2.

Table 6.3.4-5-1 – Minimum Required ROW Widths for Single Structures (Single Circuit or Multi-Circuit on Same Structure)

Line Voltage (kV)	W _{VM} (ft.)	Typical ROW Width (ft.) for Purchase			Conductor Movement Envelope - CME (ft.)		
		H-Frame	Single Pole Delta/Vertical Double Circuit	Single Pole Vertical	H-Frame	Single Pole Delta/Vertical Double Circuit	Single Pole Vertical
500	22.50	225	125	125	180	80	80
345	15.00	190	155	135	160	125	105
230	12.50	150	125	110	125	100	85
161	10.00	120	100	90	100	80	70
69	7.50	90	75	65	75	60	50

Table 6.3.4-5-2 – Minimum Allowed ROW Widths for Multiple Structures and Circuits

Line Voltage (kV)	ROW Widths (ft.) assuming two identical lines								
	ROW Width for Purchase (ft.)			Conductor Movement Envelope - CME (ft.)			Add. Width per line (ft.)		
	H-Frame	Single Pole Delta/Vertical Double Circuit	Single Pole Vertical	H-Frame	Single Pole Delta/Vertical Double Circuit	Single Pole Vertical	H-Frame	Single Pole Delta/Vertical Double Circuit	Single Pole Vertical

500	365	225	195	320	180	150	140	96	70
345	310	220	180	280	190	150	120	65	45
230	225	175	145	200	150	120	75	50	35
161	180	140	120	160	120	100	60	40	30
69	135	105	85	120	90	70	45	30	20

Notes regarding Tables 6.3.4-4,5-1 and 6.3.4-5,2:

1. Tabulated 500 kV single pole ROW reflect an atypical short span design intended to compact lines on narrower ROWs.
2. As noted in 6.3.4.1, tabulated values reflect Vee-String, Brace Post, Suspension/Strut or other insulator assemblies where conductor attachments are somewhat restrained. Where suspension I-String assemblies are used: at 230-kV and below the ROW widths given shall be increased by 5-feet; and at 345-kV they shall be increased by 10-feet. Only Vee-String assemblies are currently approved for 500 kV.
3. The ROW values presented are indicative of what would be required in straight sections of ROW containing tangent or light angle structures. Large angle changes using multi-pole structures or extensive guying patterns will require additional ROW in the vicinity of the angle structure.

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7. CONDUCTOR AND SHIELD WIRE INFORMATION

This section includes design information about standard conductors, both in single and in bundled configurations, along with standard shield wires, including fiber optic wires. It includes tension and vibration control data for the NESC and Entergy design conditions. Conductors and shield wires shall be selected from these standards unless Buyer and Seller otherwise agree in a writing signed by authorized representatives of the Parties.

7.1 Entergy Standard Conductors

The required technical standards for conductors are set forth in this Section 7.1 (properties based on Southwire® data unless noted.):

Table 7.1(a)1A – Standard Conductors – Mechanical Properties

Type	Size	Stranding	Code Word	Area (in ²)	Dia. (in.)	Weight (lb/ft)	Strength (lbs)
ACCC/TW ⁽⁵⁾	1949	56/1	LAPWING ⁽⁴⁾	1.647	1.504	1.938	48,900
	1582	33/1	BITTERN ⁽⁴⁾	1.336	1.345	1.566	39,400
	1428.5	33/1	BEAUMONT ⁽⁴⁾	1.232	1.294	1.436	43,700
	1222	33/1	CARDINAL ⁽⁴⁾	1.053	1.198	1.224	37,100
	821.2	18-1	GROSBEAK ⁽⁴⁾	0.725	0.990	0.836	30,400
ACSS	1590	45/7	LAPWING	1.34	1.50	1.79	27,900
	1272	45/7	BITTERN	1.07	1.35	1.43	22,300
	954	54/7	CARDINAL	0.85	1.20	1.23	26,000
	666.6	24/7	FLAMINGO	0.59	1.00	0.86	18,200
	1780	84/19	CHUKAR	1.51	1.60	2.08	51,000
ACSR	1590	45/7	LAPWING	1.34	1.50	1.79	42,200
	1272	45/7	BITTERN	1.07	1.35	1.43	34,100
	1033.5	45/7	ORTOLAN ⁽¹⁾	0.87	1.21	1.163	27,700
	954	54/7	CARDINAL	0.85	1.20	1.23	33,800
	954	45/7	RAIL ⁽²⁾	0.80	1.165	1.075	25,290
	666.6	24/7	FLAMINGO	0.59	1.00	0.86	23,700
	336.4	26/7	LINNET	0.31	0.72	0.46	14,100
ACAR	1024.5	34/13	N/A ⁽³⁾	0.80	1.165	0.96	23,100
	649.5	18/19	N/A	0.51	0.93	0.61	17,100
	395.2	15/7	N/A	0.31	0.72	0.37	10,100

(1) Not for New Construction, Capital Maintenance only

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(2) 345 kV and 500 kV only – Use for new construction

(3) 500 kV only – for Capital Maintenance work only

(4) Source: General Cable/LAMIFIL Data

(5) It is generally preferential to develop a custom conductor solution using an ACCR conductor in lieu of the ACCC conductors. Use of the ACCC standards will generally be limited to extension of existing ACCC lines or other similar circumstances.

Ampacity ratings for the standard conductors shall be determined using the commercially available software SWRate, which is based on the methodology of IEEE 738. Ampacity was determined using design parameters specified in Entergy standards and the conductor properties contained in the SWRate program library. Line ratings are also expressed as conductance in MVA using the expression $MVA = V * A * 0.001 * 3^{0.5}$, where V is voltage in kV, and A is rated ampacity in amps. Ampacity and conductance ratings for the standard conductors are summarized below.

Table 7.1(b)1B – Standard Conductors – Capacity

Type	Size / Code Word	Rated Amps (1)	MVA 69kV	MVA 115kV	MVA 138kV	MVA 161 kV	MVA 230kV	MVA 345kV	MVA 500kV
ACCC/TW (3)	1949 / LAPWING	2490	298	496	595	694	992	-	-
	1582 / BITTERN	2180	261	434	521	608	868	-	-
	1429 / BEAUMONT	2050	245	408	490	572	817	-	-
	1222 / CARDINAL	1857	222	370	444	518	740	-	-
	821.4 / GROSBEAK	1439	172	287	344	401	573	-	-
ACCS	1590 / LAPWING	2263	270	451	541	631	902	-	-
	1272 / BITTERN	1957	234	390	468	546	780	-	-
	954 / CARDINAL	1607	192	320	384	448	640	-	-
	666.6 / FLAMINGO	1312	157	261	314	366	523	-	-
ACSR	1780 / CHUKAR	1608	192	320	384	448	641	-	-

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Type	Size / Code Word	Rated Amps (1)	MVA 69kV	MVA 115kV	MVA 138kV	MVA 161kV	MVA 230kV	MVA 345kV	MVA 500kV
	1590 / LAPWING	1494	179	298	357	417	595	-	-
	1272 / BITTERN	1303	156	260	311	363	519	-	-
	1033.5/ ORTOLAN (2)	1144	137	228	273	319	456	-	-
	954 / CARDINAL	1088	130	217	260	303	433	-	-
	954 / RAIL	1088	130	217	260	303	433	650	942
	666.6 / FLAMINGO	882	105	176	211	246	351	-	-
	336.4 LINNET	575	69	115	137	160	229	-	-
	ACAR 1024.5 (2)	878	105	175	210	245	350	-	760
ACAR	ACAR 649.5	658	79	131	157	183	626	-	-
	ACAR 395.2	483	58	96	115	135	192	-	-

(4) (1) At normal operating temperatures, 212°F (100°C) for ACSR, 347°F (175°C) for ACSS and ACCC, and 176°F (80°C) for ACAR.

(2) (2) Other historical limits may govern.

(3) (3) It is generally preferential to develop a custom conductor solution using an ACCR conductor in lieu of the ACCC conductors. Use of the ACCC standards will generally be limited to extension of existing ACCC lines or other similar circumstances.

7.2 Entergy Standard Shield Wires

The required technical standards for shield wires are set forth in Table 7.2 below:

Table 7.2 – Standard Shield Wires

Code Word	Class Type	Size	Strand- Inch	Area (in^2)	Dia. (in.)	Weight (lb/ft)	Strength (lbs)
7 #7	Alumoweld	0.0	7	0.11	0.43	0.33	19,060

Entergy

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7.3 Standard Optical Ground Wires

The required technical standards for optical ground wires (OPGW) are set forth below:

Table 7.3 – Standard OPGW Wires

Code Word	Class Type	Fibers	Strand-	Area	Dia.	Weight	Strength
			Ing	(in^2)	(in.)	(lb/ft)	(lbs)
DNO-5651	AlumaCore	24LT	13	0.151	0.528	0.36	18,391
DNO-6651	AlumaCore	48LT	9/6	0.221	0.646	0.42	18,053
DNO-3476	AlumaCore	24	13	0.151	0.528	0.36	18,433
DNO-4596	AlumaCore	48	9/6	0.221	0.646	0.42	18,053
DNO-6205	CentraCore	24	10	0.166	0.528	0.41	21,845
DNO-6210	CentraCore	48	10	0.166	0.528	0.41	21,845
DNO-8161 ⁽¹⁾	AlumaCore	48	13	0.151	0.528	0.36	18,391
DNO-9800 ⁽²⁾	AlumaCore	48	13	0.151	0.528	0.36	19,391

(1) DNO-8161, 48 fiber AlumaCore will be the default OPGW selection unless project specifics warrant a different selection.

(2) DNO-9800, 48 fiber AlumaCore will be the default OPGW selection for “backbone” applications where dispersion shifted fibers are required by the telecommunications department.

Alternative optical ground wires may be used, provided they meet the same specifications as the above-referenced wires. Similar hardware to that used for Entergy standard wires specified herein must be used so that nonstandard hardware does not have to be stocked for maintenance.

7.4 Bundled Conductors

7.4.1 Bundled Conductors (New Construction, excluding 500 kV)

The standard bundled configuration is a vertical bundle in which no spacers are required. If other configurations are used, the conductor supplier and/or manufacture of the spacers shall be consulted regarding spacers requirements.

The standard assembly for bundled dead-end structures isshall be the “DEPY” dead-end assembly with a two-insulator attachment to the structure.

Bundled dead-end structures where the maximum tension (with OCF) in each sub-conductor is less than 9700 lbs. may use the “DEP- 2 wire” dead-end assemblies with a single insulator. This assembly shall mainly be used in reduced tension situations.

All bundled structures with angles less than 30 degrees shall be designed as running angle structures, including Structure Types “C”, “F” and “G”. Those with angles greater than 30-degrees shall be designed as dead-end structures.

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7.4.2 Bundled Conductors (500 kV)

The standard 500-kV bundled conductor is a triple delta configuration with spacers at approximately 250-foot intervals.

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7.5 Sag and Tension Limitations

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7.5.1 NESC Tension Limits

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Following are the maximum tension limits allowed in the determination of project sag and tension values. The “Zone Loading” tension limit is an NESC requirement for all load cases with an overload capacity factor of 1.65. The tension limits for extreme wind and heavy ice are Entergy requirements and have an overload capacity factor of 1.0. Load cases are shown in [Section 5.4](#). The limit is a percent of the Ultimate Breaking Strength (UBS) of the wire. Limits are based on the Initial tension of the wire.

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Load	Tension Limits
• Zone loading (OCF=1.65)	60% UBS - @ Initial Ten. (NESC 261H1)
• Extreme Wind (OCF=1.0)	75% UBS - @ Initial Ten.
• Concurrent Ice & Wind (OCF=1.0)	75% UBS - @ Initial Ten.

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Additionally, the NESC (Section- 261 H1) requires that the tension at each of the applicable NESC Zone temperatures shown in [Table- 5.1.12](#), without external load, shall not exceed the following percent of their UBS:

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Initial unloaded tension 35% UBS

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Final unloaded tension 25% UBS

These tension limits apply at each of the applicable NESC Zone temperatures shown in [Table- 5.1.12](#), unless dampers are used, in which case this limitation is at a maximum of 60°F (15°C).

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7.5.2 Tension Limits for Vibration Control

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Except for ACCC and ACCR conductors, for vibration control, maximum catenaries (horizontal tension/weight), or “C” values, will be calculated at 0°F (-20°C), 0 mph wind, and 0-inches ice.

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The following table, "Vibration Control Values", provides Entergy's tension limits for the standard conductors. The table was developed considering 900-ft. ruling spans. However, these values may be used for other ruling spans with only slight variations. Other ruling spans ~~may be used as needed~~ will require approval by Buyer.

Type	Conductor Name	Load Case	Max Tension (pounds)	% of Ultimate Strength
ACSS	LAPWING	0-0-0 (I)	10740	38.5
	LAPWING	0-0-0 (F)	8431	30.2
	BITTERN	0-0-0 (I)	8580	38.5
	BITTERN	0-0-0 (F)	6735	30.2
	CARDINAL	0-0-0 (I)	7380	28.4
	CARDINAL	0-0-0 (F)	5793	22.3
	FLAMINGO	0-0-0 (I)	5160	28.4
	FLAMINGO	0-0-0 (F)	4051	22.3
ACSR	CHUKAR	0-0-0 (I)	12480	24.5
	CHUKAR	0-0-0 (F)	9796	19.2
	LAPWING	0-0-0 (I)	10740	25.5
	LAPWING	0-0-0 (F)	8431	20.0
	BITTERN	0-0-0 (I)	8580	25.2
	BITTERN	0-0-0 (F)	6735	19.8
	ORTOLAN	0-0-0 (I)	6978	25.2
	ORTOLAN	0-0-0 (F)	5478	19.8
	CARDINAL	0-0-0 (I)	7380	21.8
	CARDINAL	0-0-0 (F)	5793	17.1
RAIL	0-0-0 (I)	6450	24.9	

[illegible]

Type	Conductor Name	Load Case	Max Tension (pounds)	% of Ultimate Strength
	RAIL	0-0-0 (F)	5063	19.5
	FLAMINGO	0-0-0 (I)	5160	21.8
	FLAMINGO	0-0-0 (F)	4051	17.1
	LINNET	0-0-0 (I)	2760	19.6
	LINNET	0-0-0 (F)	2167	15.4
ACAR	649.5 ACAR	0-0-0 (I)	3660	21.4
	649.5 ACAR	0-0-0 (F)	2873	16.8
	395.2 ACAR	0-0-0 (I)	2220	22.0
	395.2 ACAR	0-0-0 (F)	1743	17.3
	1024.5 ACAR	0-0-0 (I)	5760	24.9
	1024.5 ACAR	0-0-0 (F)	4522	19.6
SW	7#7 AW	0-0-0 (I)	1980	10.4
	7#7 AW	0-0-0 (F)	1554	8.2
	7/16" Steel	0-0-0 (I)	2400	11.5
	7/16" Steel	0-0-0 (F)	1884	9.1
OPGW	* AlumaCore, DNO-8161	0-0-0 (I)	2160	11.7
	* AlumaCore, DNO-8161	0-0-0 (F)	1696	9.2
	* AlumaCore, DNO-9800	0-0-0 (I)	2160	11.1
	* AlumaCore, DNO-9800	0-0-0 (F)	1696	8.7
ADSS	ADSS-AE024HG611CA2	0-0-0 (I)	546	18.2
	ADSS-AE024HG611CA2	0-0-0 (F)	429	14.3

*AlumaCore, DNO-8161 is the default.

Note ADSS is not a transmission standard transmission conductor but is frequently used as an under-built non-transmission conductor. Typical ADSS span is on the order of 200- feet.

Also note that (F) load cases shall be controlled by both Creep RS and Load RS, and that bimetallic conductors shall consider the effects of compression at high temperatures

7.5.3 Vibration Control for Long Spans Exceeding the Ruling Span

For span lengths greater than the ruling span, the Designer shall take special care to compare the conductor and shield wire sags, to ensure that adequate clearances at mid-span are maintained under all conditions. The shield wire tension shall not exceed 16% of its ultimate strength at 60°F (15°C), final. To account for unusual circumstances (e.g., ravine crossings), it may be necessary to dead-end the shield wire to account for tension differentials and/or increase the tensions along with adding dampers ~~as necessary per manufacturer's specifications.~~

7.6 Correction to Sag when Final Installation is Interrupted

Prolonged stringing durations can affect final sags due to creep beyond that considered in the sagging algorithm. Conductors and shield wires shall be clipped in within 72 hours of achieving the intended stringing tension. Where stringing operations are interrupted or extend beyond this 72-hour threshold, engineering evaluation/approval is required with final approval by Buyer, and the cable manufacturer shall be contacted to obtain technical instructions on the issue. ~~With their involvement, engineering will typically allow stringing to resume using the original sagging charts but considering an increased stringing temperature that will account for the additional creep.~~

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7.7 Galloping

Certain areas within the Entergy Service Area have been identified as areas prone to galloping and shall require the installation of vibration control devices. These areas are generally in north Arkansas along the Mississippi River in open, flat areas where it is possible for ice to form on the cables.

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Phase spacing shall be set to avoid mid-span interference between phases through the required assumption that double ellipse galloping will occur on any span exceeding 400 feet. A galloping overlap of less than 10 percent between phases will be allowed in the design process. It is generally assumed that using span lengths between 400 and 900 feet would eliminate this overlap. The ruling span is set at 80% of the limiting span for this analysis.

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7.8 Aeolian Vibration

Aeolian vibration fatigue damage typically occurs in flat, open areas. The most effective way to reduce this type of vibration is to reduce the line tension. Also, the installation of dampers may eliminate or reduce this vibration; however, the conductor and damper suppliers shall be consulted regarding ~~this condition when lines are constructed in these areas~~ these conditions.

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The use of ACSS type conductors may also reduce this vibration after one year of operation because of the self-damping characteristics built into this type of conductor.

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7.9 Conductor Corona

Two solutions to reduce conductor corona are larger conductors and/or bundled conductors.

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For 161 kV, 115 kV, and 69 kV, ~~Entergy uses~~ 336 kcmil ACSR "Linnet" ~~as shall be the~~ minimum conductor size.

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At 230 kV, ~~Entergy has historically installed~~ bundled 395 kcmil ACAR conductors or, for single conductor lines, a recommended standard wire size of 954 kcmil ACSR. The minimum wire size for 230 kV using industry standards is approximately one inch in diameter. ~~Entergy's~~ The smallest

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standard wire size that meets the industry standard minimum wire size is “Flamingo” 666.6-kcmil ACSR.

For 500 kV transmission lines, ~~Entergy uses~~ 1024-kcmil ACAR and 954-kcmil ACSR “Rail” ~~as shall be the~~ minimum conductor sizes to avoid corona effects. The standard for new construction is 954-kcmil “Rail”.

The selection of conductor size, considering corona losses, shall be estimated using the attached figure (obtained from the Westinghouse Transmission and Distribution Manual) entitled “Fig. 31 - Quick Estimating Corona-Loss Curves”. This figure is attached as ~~Attachment 3~~ Attachment 3.

7.10 ACSS and ACSS/TW Conductor

7.10.1 ACSS Sags – Tensions - Stringing

ACSS suppliers have recommended that the ACSS & ACSS/TW conductors be pre-tensioned for approximately 10 to 15-minutes before final sagging of the line. This procedure inelastically stretches and elongates the aluminum wires and the steel core provides total support of the conductor in normal operation. Since little or no stress is left in the aluminum wires, initial and final sags and tensions are nearly the same. Pre-stressing is a means of reducing creep and enhancing self-damping capability. Recommendations for pre-stressing vary and range from the maximum tension ~~the line will experience to 15% above initial tension.~~ Consult with cable manufacturer for prestressing methodology and specifications.

7.11 Fiber Optic/Shield ~~wire~~ Wire Requirements

Fiber Optic Shield Wire (OPGW) is often the preferred shield wire. For structures with two shield wires, one shield wire will typically be OPGW and one shield wire will typically be 7#7. ~~Confirm with Entergy for project~~ Project specific shield wire requirements: ~~is subject to approval by Buyer.~~ Substation Relay Design, SCADA, Substation Networking and Corporate Telecommunications will need to determine the number of fibers that they will need. Standard Entergy shield wires are found in ~~Section 7.~~

7.11.1 Fiber Optic Details

The fiber optic line ~~shall~~may be dead-ended if the line angle is over 30°. For line angles between 30° and 50°, a heavy angle suspension assembly ~~is preferred.~~may be utilized. Fiber optic construction details are shown on the standard assembly drawings, shown in ~~Attachment 1.~~Attachment 1.

7.11.2 Splice Box Locations

Splice boxes shall be placed at existing or expected future laterals and substations. Additional boxes will be needed at intervals along the line, generally corresponding to reel wire length, ~~line angles,~~ and considering the nearest points of access. ~~A site visit with all concerned parties may be necessary to select the best locations for splice boxes.~~

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7.12 SW Sagging Relative to Conductors

Every effort shall be made to ensure that the shield wire(s) have less sag than the conductor, so that any flashovers are encouraged to occur at a structure rather than at mid-span. It is suggested that the shield wire have a lesser amount of sag by approximately 0.33-percent of the span length, or approximately two (2)-feet, under normal stringing loads, i.e., 60°F (15°C). Where this is not feasible, the tension limits to control vibration in Table 7.5.12 may be relaxed to pull the shield wire more tightly and achieve greater separation. Where the tension limits of Table 7.5.12 are relaxed, a conductor vibration study shall be performed, and vibration dampers shall be installed on the shield wire per the recommendations of the vibration study. Alternately, the standard framing may be modified with approval from Buyer to provide greater separation between the shield wire and the conductor.

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7.13 Conductor and Shield Wire Marking

7.13.1 Aerial Patrol Marking

Aerial patrol marking to provide early warning of the hazards due to crossing transmission lines shall be applied— as described herein.

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7.13.2 Marking for Federal Aviation Administration (FAA) regulations

Marking required to comply with Federal Aviation Administration (FAA) regulations shall not be confused with the aerial patrol marking described in paragraph 7.13.1. When routing new lines, it is generally better to avoid selecting routes that pass within close proximity of airports, landing strips, heliports and facilities such as hospitals that might have aircraft landing on improvised landing sites. Such facilities can be generally identified by examining aerial navigation maps available at pilot centers in most public airports, examination of quadrangle maps published by the U.-S. Geological Commission, examination of aerial photographs acquired for the line project, and other sources. Where these facilities cannot be avoided and where it is determined that FAA rules apply, the requirements of FAA Advisory Circular AC 70/7460-1K shall apply.

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7.13.3 Navigable Waterway Marking

Lines crossing navigable waterways shall be marked as delineated in the applicable permits.

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7.13.4 Avian

Avian markers are to be installed where appropriate to make the line more visible to birds. Several forms of markers are commercially available and marketed to increase line visibility and reduce the possibility of avian mortality. Avian markers shall be required only where specified by wildlife agencies or by applicable permits.

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7.13.5 Slow-Moving Vehicle Signs

Slow-moving vehicle signs shall be placed on the third and fourth adjacent structures on both sides of any crossover lines, with the signs facing the approach to the lines from either side of the

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crossover. It is very important that all crossings be marked on the same number of advance structures for safety reasons. One sign on each structure shall be used to indicate a single crossover ahead. If two crossovers in close proximity exist ahead, then two signs shall be installed on each structure, one sign over the other, if possible. Two-crossover situations shall also have single signs on both sides of structures between the crossovers. Details of the installation are covered in an attachment to this [AttachmentAppendix 10](#), but generally the signs shall be near the top of the poles or towers of the structures. When used on wooden poles, the signs shall be outside any woodpecker wire covering the pole.

7.13.6 Spiral Vibration Dampers (Yellow)

Spiral dampers in addition to slow-moving vehicle signs may be desirable in some cases with extraordinary visibility difficulty. When used, such dampers shall be installed with a minimum of one pair of dampers on both sides of centerline of the line being patrolled at a point just outside the conductor locations but not less than 15 feet between the pairs. If there are two shield wires on the crossover line, half of the dampers shall be installed on each shield wire.

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7.13.7 QuikMark Devices

QuikMark devices, in addition to slow-moving vehicle signs, may be desirable in some cases with extraordinary visibility difficulty. When used, QuikMark devices shall be installed with a minimum of three QuikMark devices on each side of centerline of the line being patrolled at a point just outside the conductor locations but not less than 15 feet between each trio. If there are two shield wires on the crossover line, install half of the QuikMarks on each shield wire.

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7.13.8 QuikMark Devices Combined with Spiral Vibration Dampers

QuikMark devices and spiral dampers may be combined to mark shield wires by keeping equal numbers of each on each side of the line being patrolled so the visual effects are balanced on the line. When the Transmission Line crosses under the line of another, the minimum requirement is for QuikMark devices or spiral dampers or both to be installed on the shield wires of the other line. This is for the safety of Entergy aerial patrollers and to protect Entergy and others from claims by the owner of the other line for property damage, lost revenues on the other line, and other claims.

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8. OTHER ELECTRICAL CRITERIA

8.1 Electrical Insulation

All insulators shall be polymer (non-ceramic). Insulators that are procured from one of Entergy's approved vendors for insulators and adhere to Entergy's standards are assumed to meet this specification. Insulator types include dead-end, braced post, post, suspension and jumpers. All new HV (69 kV and above) Transmission Lines shall have insulators with corona rings installed. Details for these insulators are included in Attachment 1- Attachment 1.

8.1.1 Insulator Swing

8.1.1.1 Mechanical Clearance

Post and braced post assemblies have the potential for contact between their suspension shoe and their post insulator. The suspension shoe may swing towards the supporting post insulator without any wind due to line deflection angle and/or phase position changes between consecutive structures. With a 6_PSF wind (60_degrees Fahrenheit and final wire tension) further displacing the conductor hardware from its everyday displacement, contact with the sheds (or corona ring) is not allowed. With extreme wind specified in Table 5.1.1.2 of the design criteria (60_degrees Fahrenheit and final wire tension) further displacing the conductor hardware from its everyday displacement, contact with the rod's sheath is not allowed. A swing angle adapter shall be used to increase mechanical clearance. This adapter does not preclude mechanical conflict, so conductor position shall still be checked.

8.1.1.2 8.1.1.2 Electrical Clearance

Table 8.1.1.2 requires specifies required certain clearances from the energized conductor shoe to non-energized portions of the structure under the prescribed conditions specified in the footnotes. These clearances were initially built into all of Entergy's standard framings: shown in Attachment 1. Certain atypical conditions, such as short spans, structures in dips, transition between framings or phasing, deflection angles near the top of the range, and higher tensions, can warrant greater scrutiny-deviations from standard, such conditions will require Seller to acquire approval from Buyer. Conductor position shall be checked to verify verified against Table 8.1.1.2, that the required minimum clearances are met, especially for suspension insulators. For posts and braced posts, the standard post lengths will ensure that these clearances are met, except for the no-wind clearance for bundled conductors. For bundled posts and bundled braced posts, the conductor hardware shall not be allowed to swing more than 30 degrees toward the pole without wind (0 degrees F, initial). Note that the swing angle adapters mentioned in Section 8.4.1.1 do not improve electrical clearance.

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Table 8.1.1.2 – Minimum Insulator Swing Clearances

FRAMING VOLTAGE	CONDITION	CLEARANCE TO ARM OR STRUCTURE	CLEARANCE TO GUY
500 kV	6 psf wind ⁽¹⁾	123 in	11 ft.
500 kV	100 mph ⁽²⁾	60 in	5 ft.
500 kV	no wind ⁽³⁾	140 in	12 ft.
500 kV	no wind ⁽⁴⁾	140 in	12 ft.
345 kV	6 psf wind ⁽¹⁾	85 in	8 ft.
345 kV	100 mph ⁽²⁾	41 in	4 ft.
345 kV	no wind ⁽³⁾	105 in	9 ft.
345 kV	no wind ⁽⁴⁾	105 in	9 ft.
230 kV	6 psf wind ⁽¹⁾	52 in	6 ft.
230 kV	100 mph ⁽²⁾	27 in	3 ft.
230 kV	no wind ⁽³⁾	83 in	8 ft.
230 kV	no wind ⁽⁴⁾	88 in	8 ft.
161 kV	6 psf wind ⁽¹⁾	37 in	5 ft.
161 kV	100 mph ⁽²⁾	19 in	2 ft.
161 kV	no wind ⁽³⁾	60 in	7 ft.
161 kV	no wind ⁽⁴⁾	71 in	7 ft.
138 kV	6 psf wind ⁽¹⁾	34 in	5 ft.
138 kV	100 mph ⁽²⁾	16 in	2 ft.
138 kV	no wind ⁽³⁾	54 in	7 ft.
138 kV	no wind ⁽⁴⁾	65 in	7 ft.
115 kV	6 psf wind ⁽¹⁾	28 in	5 ft.
115 kV	100 mph ⁽²⁾	13 in	2 ft.
115 kV	no wind ⁽³⁾	49 in	7 ft.
115 kV	no wind ⁽⁴⁾	60 in	7 ft.
69 kV	6 psf wind ⁽¹⁾	17 in	3 ft.
69 kV	100 mph ⁽²⁾	8 in	1 ft.
69 kV	no wind ⁽³⁾	49 in (36 in) ⁽⁵⁾	6 ft.
69 kV	no wind ⁽⁴⁾	60 in (49 in) ⁽⁵⁾	6 ft.

(1) Max required value between switch surge and NESC air gap. Controlled by NESC with 10% Voltage Surge (1.1 x nom. Voltage).

(2) 60 Hz minimum flash over distance.

(3) No wind clearance for suspension insulator (Impulse Air Gap).

(4) No wind clearance for running angles (Impulse Air Gap).

(5) (5) 69 kV framings use 115 kV no-wind air gaps for improved lightning performance. On existing structures where there isn't room for longer insulators and air gaps, the numbers in parentheses apply.

8.1.1.3 Typical Standard Davit Arms

For the purpose of determining clearances presented in Table 8.1.1.2 accounting for insulator swing; as well as for the purpose of evaluating shield angle and determining conductor coordinates, the following arm lengths and insulator lengths shall be used:

Table 8.1.1.3 – Typical Davit Arm and Insulator Lengths for New Construction

INSULATOR LENGTH ⁽²⁾			
VOLTAGE (kV)	TYPE	INSULATOR LENGTH (IN)	DESIGN LENGTH (IN.)
69	SUS	59	66
161	SUS	73	78
230	SUS	89	96
69	DE/RA	62	80
161	DE/RA	92	98
230	DE/RA	104	110
69	LP/BP	60	60
161	LP/BP	76	78
230	LP/BP	94	94
DAVIT ARM LENGTH ⁽¹⁾			
VOLTAGE (kV)	TYPE	LENGTH	RISE (IN.)
69	Tangent	5'-6"	13
161	Tangent	8'-6"	25
230	Tangent	11'-0"	24
69	Swing	3'-0"	N/A
161	Swing	4'-0"	N/A
230	Swing	5'-0"	N/A
69	DE	5'-0"	12
161	DE	6'-0"	15
230	DE	8'-0"	20

(4) (1) Davit Arm Length is from pole face to conductor attachment

(2) (2) Design length includes hardware.

8.1.1.4 Insulator Attachments – 69 kV, 161 kV, and 230 kV Structures

Braced post and line post insulators are limited to a line angle of 6 degrees based on the limited compression capacities of these insulators. ~~The “Macleane Alliance Insulators binder” by Maclean Power Systems gives the tensile strength of all dead-end insulators and the combined working load charts for all of the standard post and braced post insulators used by Entergy.~~ Insulator capacities shall be obtained from manufacturer.

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8.1.1.5 General

The same insulator type can be used for concrete and steel poles. Insulator attachments for post insulators are required to be provided by thru-bolting standard insulators to the pole structures.

Dead-end and suspension insulators are required to be attached to the poles via vangs on steel poles or pole-eye plates on concrete poles.

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8.1.1.6 Conductor and Shield Wire Vangs

Standard conductor and shield wire attachment vangs on all steel poles shall be 3/4" plate with 1 1/8" diameter holes and 1 1/2" radius and shall be the same on both ends.

Conductor attachment vangs on concrete poles will be 60,000 or 70,000-pound strength pole-eye plates mounted with 7/8" diameter all-thread rods, similar to those provided by Hughes Brothers in Lincoln, Nebraska.

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8.1.1.7 Guy Vangs

Standard guying vangs on all steel poles shall be 3/4" plates with 1 1/8" diameter holes and 1 1/2" radius and shall be the same on both ends. All guy attachment vangs on all concrete poles will be 60,000 or 70,000-pound strength pole-eye plates mounted with 7/8" diameter all-thread rods, similar to those provided by Hughes Brothers in Lincoln, Nebraska.

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8.1.1.8 Polymer Insulator Standard Drawing

~~Attachment I~~ Attachment I has detailed drawings of the Entergy Standard Insulator drawings for 115-kV, 138 kV, 161 kV and 230 kV voltages. Seller shall use the Entergy Standard Insulators and must verify they meet the requirements for the design. The drawing includes the following information:

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Braced Post Insulators

Horizontal Line Post Insulators

Suspension Insulators

Dead-End Insulators

Minimum Flashover Characteristics

Minimum Leakage Distance

8.2 Transmission Line Lightning Protection Design

8.2.1 Reference Guides

IEEE Std. 1243-1997	Guide for Improving the Lightning Performance of Transmission Lines
EPRI	Handbook for Improving Overhead Transmission Line Lightning Performance
EPRI	AC Transmission Line Reference Book - 200kV and Above
EPRI	Guide for Transmission Line Grounding
EPRI	Outline of Guide for Application of Transmission Line Surge Arrestors – 42 to 765 kV

All of Where applicable Seller shall apply the following parameters cannot be controlled by the Designer, but some consideration shall be given for each during the design process.

8.2.2 GFD

The GFD varies greatly throughout Entergy's transmission system and average from 2-7 flashes/Km²/yr. However, the GFD for any area for a particular year can be more than 3X the historic average. Therefore, Entergy's design parameters do not consider the GFD for the specific line but assume the standard design methods will ensure an adequate reliability throughout the system no matter the GFD of any particular location.

8.2.3 Structure BIL

Although local atmospheric conditions can affect the ability of air to insulate against a flashover the typical breakdown rate for a negative dry arc is 650 kV per meter. Therefore, the structure BIL is 650 kV X air gap in meters.

It is very difficult to maintain an acceptable BIL for distribution circuits on a transmission line structure. In order to maintain acceptable lightning performance when attached to tall shielded transmission structures, fiberglass arms and transmission class insulators are required.

Distribution underbuild is considered a last resort for new construction. It complicates maintenance for both organizations.

8.2.4 Shield Wire Installation

The installation of a shield wire is the required method of lightning protection.

8.2.5 Shield Wire Type and Size

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The size and type of shield wire used will be determined by needs other than that required for lightning protection, such as fault current. Any of Entergy's standard shield wires conforming to the parameters set out in the referenced guideline will be adequate for the lightning protection of the line. Note: Supporting distribution phases on transmission structures exposes transmission shield wire to long duration distribution faults for which it was not designed. Therefore, a neutral conductor shall be bonded to each transmission structure.

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8.2.6 Shielding Angle

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The shielding angle, as measured at the structure from the vertical plane of the shield wire clamp to the conductor clamp, shall be no more than 25° for structures adjacent to spans averaging less than 150- feet above ground level. The required shielding angle on structures where the average conductor height is ~~above~~greater than 150- feet ~~above ground level~~ need to be designed on a case by case basis- and shall be subject to approval from Buyer. The average height taken as the height at the structure minus 2/3 the sag.

On single pole structures with one shield wire, the shielding angle shall be checked ~~onto~~ the top conductor as well as ~~to~~ the bottom conductor opposite the shield wire attachment.

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On H-type structures, the shielding angle shall be checked for each shield wire to its corresponding outer conductor. Unless the distance between the shield wires exceeds 60- feet, the shielding angle to the middle conductor is not considered.

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8.2.7 Maximum Grounding Resistance

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The maximum allowable grounding resistance shall be obtained as specified in ~~Section~~ 8.4Section 8.3.

8.2.8 Lightning Arrestors

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Lightning arrestors shall be used on transmission lines only in cases where a shield wire cannot be installed (e.g., clearance near an airport), the maximum allowable grounding resistance cannot be obtained, or adjacent to extremely long spans where the lightning protection software shows the shield wire is insufficient.

~~Refer to Section 8.3 for standards on arrester implementation and design:
4.1 — Arrester Requirements~~

~~Arresters are not usually provided in new capital construction projects except in special conditions where the need for them is predictable.~~

8.3 Grounding and Cathodic Protection

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This section covers the design of the grounding and cathodic protection systems for concrete and steel structures for transmission lines.

8.3.1 Grounding

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8.3.2 Grounding Systems

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Entergy's steel and concrete pole structures shall be "effectively grounded" as defined in Section 2 of the NESC. Shield wires are constructed, along with the associated grounding system, on all of Entergy's transmission lines for lightening protection. The use of proper structure grounding will reduce the ground resistance at the structures and will reduce line outages due to lightning strikes.

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8.3.3 Steel Structure Grounding System

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Steel poles ~~are~~shall be bonded to the shield wire by a copperweld jumper. The pole then acts as a ground rod to the ground line. Because the coating at the bottom of direct embedded steel poles insulates the steel, direct embedded poles shall be grounded. This grounding ~~is~~shall be done with a ~~10-ft. copperclad steel rod~~ground rods driven into the earth and bonded to the pole. The same grounding is used to ground a steel pole bolted to a concrete pier or set in a concrete pile. Steel poles socketed into steel piles shall be bonded to the steel pile. ~~The pile is then considered as an effective grounding rod.~~

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8.3.4 Concrete Structure Grounding System

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Concrete poles ~~are~~shall be bonded to the shield wire through the grounding clip and a terminal lug at the pole top by a copperweld jumper. A copperweld wire ~~is~~shall then run down the pole to another terminal lug below ground. The wire may be internal or external. There are four options for grounding the direct buried pole: (1) ~~connect~~ the ground wire to the pancake at pole bottom; (2) ~~extend~~ the ground wire from the pancake to the ground rod; (3) ~~connect~~ the ground wire from the terminal directly to the ground rod; and (4) ~~connect~~ the ground to the substation ground grid using 4/0 ~~copper~~. Ground wires shall be continuous (no splices). For concrete poles set in steel piles, the ground wire shall be extended from the bottom lug and bonded to the pile.

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8.3.5 Guy Wire Grounding System

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In accordance with NESC requirements, guy wires shall be bonded directly to the steel structure or to the ground wire on a concrete structure using a copperweld wire bonded to the guy wire.

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8.3.6 Achieving Desired Structure Resistance

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Tests to verify that the required footing resistance has been obtained using the standard methods shall be performed by ~~the Contractor~~Seller.

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~~The Contractor~~Seller shall test for grounding resistance, which shall not be greater than:

69 kV & 115kV _____ 13 ohms

138 kV & 161 kV _____ 10 ohms

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230 kV _____ 7 ohms

345 kV & 500 kV (H-frames) 18 ohms

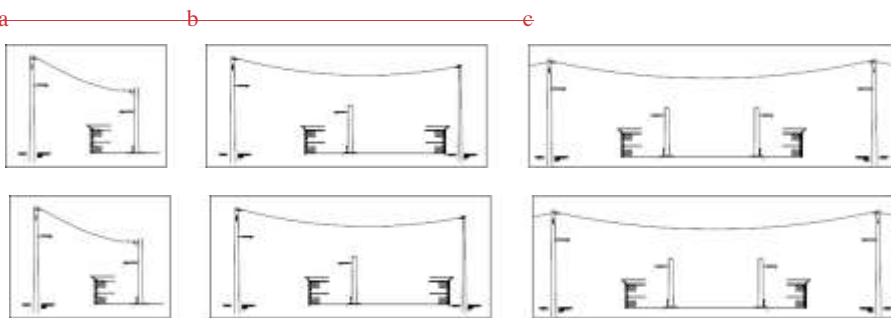
There are two acceptable methods to achieve these requirements: (1) driving additional rods and (2) installing a counterpoise that consists of 100 feet of conductor buried 18" deep parallel to the line.

8.3.7 Grounding at Substations

Bonding of Transmission Line Shield Wire to Substation Ground Grid

Electrical currents can be introduced on shield wires from a variety of sources. To prevent these currents from arcing across mechanical connections to get to the substation ground grid, a bonding conductor shall be provided.

~~There are three~~The following common shielding configurations and requirements shall be permitted are detailed below:



a b c

a. a. Shield wire attached to Substation pull-off structure

Generally, the transmission line will be dead-ended outside the substation and the shield wire slack span into the station will be positively grounded to the pull-off tower with a jumper and the pull-off tower will be connected to the substation ground grid. It is the responsibility of the substation to make these connections. The last transmission structure in the immediate vicinity of the station shall not be bonded to the substation ground grid unless a specific grounding analysis is performed.

b. b. Shield wire across station to dedicated shield wire pole

Since the shield wire pole is usually installed within close proximity to the substation; it shall be bonded to the substation ground grid. The last transmission structure in the immediate vicinity of the station shall not be bonded to the station grid unless a specific grounding analysis is performed.

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c. Shield wire across station to exiting transmission line structure

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One of the transmission structures on either side of the station shall be bonded to the substation ground grid. The structure selected for bonding shall be the one closest to the station or having the fewest physical obstacles between the structure and the station.

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8.3.8 Cathodic Protection

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1.1.1.1 Protection System

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The cathodic protection system is a method of protecting steel transmission line structures from corrosion, generally at the ground-line where moisture can mix with air to cause corrosion and thus deterioration and loss of strength of the structures. The protection system used is to attach either magnesium or zinc anodes to the structure.

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These anodes provide sacrificial protection for the steel in the structures.

Soil Investigations

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The soil investigation shall include soil corrosion recommendations to determine the need for anodes and the number required for each structure.

Anode Types

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Magnesium anodes shall be used except that, in areas such as coastal marshes, zinc anodes may be used where recommended over magnesium anodes by the corrosion engineer: based on in-situ conditions

8.3.9 Structure Protection

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Steel poles, steel piles and steel guy anchors shall be protected as described below.

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Steel Dead-End and Guyed Structures

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All buried steel (embed poles and piles) at dead-end and guyed steel structures shall be installed with anodes as shown on the Framing Drawings and provided Assembly Drawings. The number of anodes per structure shall be as recommended in the corrosion consultation report or as deemed necessary by the corrosion engineer based on in-situ conditions.

Steel Tangent Structures

Steel tangent structures are generally not installed with anodes. ~~Possible reasons for installing,~~ anodes shall be installed on ~~tangent~~ structures ~~are installation~~ in areas of known corrosion problems, ~~and/or~~ when structures are to be installed adjacent to a pipeline or railroad. In these cases, installation shall be in accordance with provided Assembly Drawings in Attachment 1.

Guy Anchors for Steel and Concrete Structures

The steel helix type anchors for both steel and concrete poles shall be installed with anodes.

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9. STRUCTURE DESIGN CRITERIA

9.1 Steel Poles

Entergy standard structure framings are shown in [Attachment 1](#). ~~Attachment 1.~~

9.1.1 Tubular Steel Pole Purchase Specification

Details of structure design that shall be included in the purchase specification are:

ASCE Design Manual Requirements

Material Specifications

Pole Deflection Limitations

Fabrication Requirements

Protective Coating Requirements

Cathodic Protection

Grounding Requirements

Seller shall procure (or cause to be procured) tubular steel poles from tubular steel pole vendors on the Approved Vendor List ~~(Attachment 5)~~ [\(Attachment 5\)](#) for tubular steel pole vendors and direct the vendor to provide items in conformance with [their](#) applicable ~~Entergy Standards~~ [standard Energy specifications](#).

9.1.2 General Design Requirements

9.1.2.1 General

All designs shall be in accordance with the provisions of the latest NESC, ASCE/SEI Standard 48, and the requirements stated in this document. ~~All~~ construction shall be Grade B, as defined in Section ~~24~~ of the NESC Code.

9.1.2.2 Foundation Rotation

In addition to the applied loadings, all self-supported monopole and un-braced H-frame structures shall be designed with a 3-degree foundation rotation. ~~The~~ point of rotation is assumed to be at the ground line. ~~Smaller~~ foundation rotations for braced H-frame structures shall be considered on a case-by-case basis.

9.1.2.3 Deflection Limitations

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The following pole deflection limitations assume 0-degree foundation rotation and shall be adhered to in the design of all poles. The percentage listed is the percent of the pole height above ground.

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[illegible]NA - Not Applicable

(4)	(1)	Camber if Deflection Exceeds 1%
(2)	(2)	Only if Specifically Requested

For new project construction, cambering the pole when deflection exceeds 1% of the pole height above ground is the ~~preferred~~required resolution to concerns arising from what might (aesthetically) appear to be excess pole deflection.

The Designer shall select a pre-designed light duty pole, such as an SW Class-H-6 equivalent, to be used as the pole in guyed framings in the pole spotting procedure. This type of pole will make

available the range of heights to complete the spotting process. PLS-CADD will select the optimal pole height.

9.1.2.6 Selection of Pre-designed Poles – Optimizing Process

To use the line optimization features PLS-CADD, the Designer must select and input the pre-designed pole types and framings most suited for the Transmission Lines. This shall include the material, framings and pole heights, types and sizes.

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9.1.2.7 Pole Design and Verification Process

The purchase order for the structures selected by PLS-CADD during the optimization process is then forwarded to the pole vendor along with a calculated ~~Load Tree~~load tree for each pole. The vendor will then review the design of the selected poles before pricing and fabrication. In some cases the poles selected may have to be revised to meet the design criteria.

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9.1.3 Procurement

To purchase the poles and associated materials, ~~the Entergy Transmission Department uses~~Seller shall use a type of purchase requisition known as a “White Requisition”.

“White Requisition” – This type of order is used to purchase material from Entergy’s preferred vendors including steel and concrete poles, insulators and conductors. The pole order will generally include the preferred item plus most of the assembly attachment material, such as nuts, bolts, vangs. It is the vendor’s responsibility to verify the size and number of each item. “White Requisitions” are also used to order non-stock-coded items. ~~It~~

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~~It is suggested that the Seller use this same procedure with Entergy’s preferred vendors to procure materials.~~

9.1.4 Structure Hardware

The Entergy “Standard Structure Framings” in ~~Attachment 1~~Attachment 1 lists the standard assemblies required for each structure framing. Each assembly drawing lists the bill of materials required for that assembly. The standard hardware parts were designed to meet the maximum tensions and loads calculated for the pre-designed structures previously described but shall be verified by the designer. Unless Buyer grants an exception in writing, poles shall be ordered with sufficient step bolt mounting provisions.

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9.1.5 Grounding and Cathodic Protection

See ~~Section 8.4~~ 8.3 for design information regarding the required grounding and cathodic protection for steel poles.

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9.1.6 Hybrid Structures

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Hybrid structures, a combination of a steel top section and a concrete bottom section, shall be used where ground water conditions may cause excessive corrosion of a steel pole. For such structures, the concrete bottom piece shall directly embedded using standard embedment details. Foundation and grounding details are discussed in ~~Section 10~~ 10 and ~~Section 8.4~~ 8.3, respectively.

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9.2 Concrete Poles

This section covers the design and analysis of concrete pole structures for single and bundled conductor transmission lines. It covers single pole, two pole, and three pole structures with direct-embedded foundations, socket-type foundations and base-plated foundations all for use on tangent, running angle or dead-end structures. All standard structure framings applicable to this work are delineated in Attachment 1.

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9.2.1 Spun Pre-stressed Concrete Pole Purchase Specification

Details of structure design that shall be included in the purchase specification include:

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ASCE and PCI Design Guide Requirements

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Material Specifications Pole Deflection Limitations

Fabrication Requirements

Testing Requirements.

Seller shall select a concrete pole vendor from the list of concrete pole vendors set forth in the Approved Vendor List (Attachment 5) and direct the concrete pole vendor to provide items in conformance with their applicable standard Entergy Standards-specifications.

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9.2.2 General Design Requirements

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9.2.2.1 General

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All concrete pole and related designs shall be in accordance with the provisions of the latest NESC, the PCI and ASCE Guide Specifications, and the requirements stated in this document. All concrete pole construction shall be at least Grade B, as defined in Section 24 of the NESC Code.

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9.2.2.2 Foundation Rotation

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In addition to the applied loadings, all self-supporting structures shall be designed with a 3 degree foundation rotation. The point of rotation shall be assumed to be at the ground line.

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9.2.2.3 Deflection Limitations

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The following pole deflection limitations assume 0-degree foundation rotation and shall be adhered to in the design of all concrete poles. The percentage listed is the percent of the pole height above ground.

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To purchase the poles and associated materials, Seller shall use a type of purchase requisition known as a “White Requisition”.

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“White Requisition” – This type of order is used to purchase material from Entergy’s preferred vendors, including steel and concrete poles, insulators and conductors. The pole order will generally include the poles plus most of the assembly attachment material, such as nuts, bolts, vangs. It is the vendor’s responsibility to verify the size and number of each item.

9.2.4 Structure Hardware

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The applicable Entergy “Standard Structure Framings” included as Attachment 1 lists the standard assemblies required for each structure framing. Each assembly drawing lists the Bill of Materials required for that assembly. The standard hardware parts are designed to meet the maximum tensions and loads calculated for the pre-designed structures previously described. Unless a deviation is granted by Buyer, poles shall be ordered by Seller with sufficient mounting locations for attachment of climbing provisions.

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9.3 H-Frame Design

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This section covers the design of concrete and steel H-Frame structures to be used in construction of the Transmission Lines. These standard framings cover transmission structures for single and double circuit construction using standard suspension insulators. Clearance has been provided for the possible use of bundled conductors.

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9.3.1 Structure Types

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Standard framings are developed for single and double circuit “Light” and “Medium” (HA2) tangent (0° – 1.5°) structures and “Light” and “Medium” (HB2) small angle (1.5° – 6.0°) structures. Standard tubular steel cross arms have been pre-designed and detailed for use in “Light” and “Medium” structures.

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The standard framings are based on the base assumption that steel structures will be X-braced and concrete structures will not be X-braced. The pole supplier shall determine if X-braces are required for each structure and shall detail and supply the X-braces and connection hardware if required.

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Special “Uplift” framings are included for use in certain structures to address uplift forces in those structures. These structures use the “Light” cross arms with extra vangs to dead-end the conductors.

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9.3.2 Cross Arm Design

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The maximum allowable spans for the pre-designed standard cross arms are based on the maximum vertical load imposed on the arms. The load cases reviewed for each cross arm are NESC designated loadings with overload factors. Maximum arm deflections range from 1-inch to 2-inches.

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The tubular steel cross arms are designed to support the vertical load of the various standard conductors used by Entergy on the standard H-Frame framings. The maximum loads for each of the Standard Framings are shown on the Framing Drawings.

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The "Light" and "Medium" standard cross arm sizes are as follows:

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Light Cross Arm – TS 6" x 6" x 3/16"

Medium Cross Arm – TS 8" x 8" x 1/4"

Shield Wire Arm – TS 4" x 4" x 3/16"

The required use (loading) for the standard cross arms is as follows:

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69 kV – Use the Light Cross Arm – for all conditions

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161 kV – Use the Light Cross Arm – for 1/2" Ice loadings

Use the Medium Cross Arm – for 1" Ice loadings

230 kV – Use the Medium Cross Arm for all conditions

9.3.3 Cross Arm Assembly Details

The assembly drawings for attaching cross arms to poles are included in the voltage specific assemblies.

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9.3.4 Rock Anchors

In rock formations, where screw type anchors will not penetrate the rock, rock anchors shall be used. There are two types of rock anchors available, to be selected based on in-situ conditions and engineering calculations.

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9.3.5 Expanding Rock Anchors

Rods have a diameter of 1.0-inch and an ultimate strength of 36,000-lbs. The limitation of 36,000-lbs can be overcome by using twin anchors. A more stringent limitation is that the rods are non-extendable. This prevents the expanding rock anchors from being used when the non-fractured bedrock is deeper than about four feet below the surface.

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9.3.6 Grouted Rock Anchors

The anchors have a 1 1/4-inch diameter round shaft ending in a 4-inch diameter bell. The anchors can be extended with either 1 1/4" round shaft extensions or 1 1/2" square shaft extensions. The anchor assembly has an ultimate strength of 70,000-lbs. The strength of the installed anchor (resistance to pullout) is dependent upon the rock type and the dimensions of the grout column. The characteristic

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of the rock that dominates the calculation for anchor depth is the equivalent cohesion. The installed anchor strength is calculated by multiplying the surface area of the grout column in each layer by the equivalent cohesion of the rock in that layer. For conservatism, any contribution from the overburden shall be ignored.

The High Wind and Heavy Ice Tensions shall be multiplied by 1.65 to provide a safety factor for the anchor installation. For the NESC Zone load case (NESC 250B) a safety factor of 1.0 shall be used as allowed by the code, since that load case already includes an Overload Factor of 1.65. The resulting worst case force shall be resisted by the friction between the grout column and the surrounding rock.

Anchor strength = (circumference)(column length per vertical foot)(constant of 0.9)[(layer 1 thickness)(layer 1 cohesion) + (layer 2 thickness)(layer 2 cohesion) + ...]

Seller shall procure that the anchor manufacturer calculates the required anchor depth using their software, but the effective cohesion shall be the parameter that dominates the result. For simplicity, the formula above uses just the effective cohesion. The constant 0.9 is a factor to account for the possible effects of other rock characteristics

The dimension that is to be specified is the distance along the anchor shaft from the ground surface to the bottom of the anchor. The minimum anchor length engaging rock is five feet.

The grout shall be pumped into the hole to ensure that a solid column is produced.

9.3.7 Guying Hardware

Following are listed the strength values in Entergy's Standard Guying Assembly which limit Lineline conductor tensions and are required for this Project.

9.3.7.1 Insulator Assembly

Entergy's Standard Polymer Dead-End Insulators have an ultimate tension capacity of 50,000 lbs. The NESC Strength Factor for insulators is 0.5, therefore the Routine Test Load (RTL or working load) of 25,000 lbs is used.

9.3.7.2 Steel Vangs (Steel Poles)

Steel Dead-End vangs are thru vangs and can be designed for any applied tensions. The NESC Strength Factor for the vangs is 1.0.

9.3.7.3 Pole Eye Plates for Conductor or Shield Wire (Concrete Poles)

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The standard guying attachment is the “AS2720 Double Guying Tee” from Hughes Bros. The Ultimate Strength (maximum tension load) is 35,000-lbs per hole. The NESC Strength Factor is 1.0 for NESC Rule 250B Tensions (OLF=1.65) and 0.8 for Extreme Load Tensions (OLF=1.0) for Rule 250C.

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9.3.7.4 Pole Eye Plates for Guy Wire (Concrete Poles)

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The standard guying attachment is the “A2132 Heavy Dead End Tee” from Hughes Bros. The Ultimate Strength (maximum tension load) is 70,000-lbs. The Strength Factors are the same as for the above “Double Guying Tee”. The maximum tension is along the guy slope, thus limiting the line tension depending on the actual guy slope.

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9.3.7.5 Double Arming Bolts (Concrete Poles)

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The standard bolt used in Entergy’s Dead-End Assemblies is an ANSI C135.1, 7/8” “Double Arming Bolt”. The maximum Tensile Strength is 25,400-lbs, the maximum ~~Shear Strength~~shear strength through threads is 17,270-lbs. and the maximum ~~Shear Strength~~shear strength through the shaft is 24,350-lbs. The ~~Shear Strength~~shear strength through the threads is always used for the Dead-End Connection. The NESC Strength Factors are also the same as for the “Double Guying Tee”. The allowable bolt strength for combination shear and tension loads, such as the guying assembly, is the calculated “interaction stress”. These bolts are the limiting factor, depending on guy slope, of the line tension in the guying assembly.

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9.3.7.6 Thimble Clevis

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The thimble clevis used in the Dead-End Assembly has a 1” pin and is rated at 60,000-lbs. Ultimate Strength. The NESC Strength Factors are the same as the “Double Guying Tee”.

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9.3.7.7 Extension Link

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The extension link is used in place of the thimble clevis when a double down-guy is used with two anchors. The link uses a 1” pin and is rated at 60,000-lbs. Ultimate Strength. The NESC Strength Factors are the same as the “Double Guying Tee”.

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9.3.7.8 Vari-Grip Dead-End

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The vari-grip shall be rated for a 19#8 guy wire with an ~~ultimate strength~~Ultimate Strength of 43,240-lbs. and 61,500 lbs. with a 19#6 guy wire. The NESC Strength Factor is 1.0.

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9.3.7.9 Turnbuckle

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The turnbuckle shall be a 1” x 6” with jaw and eye ends with an ~~ultimate rated strength~~Ultimate Strength of 50,000 lbs. The NESC Strength Factor is 1.0.

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The following table gives the allowable line tension based on the guy assembly and guy wire slopes. All loads are in Kips.

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9.3.8 Guyed Structure Limitations

9.3.8.1 Concrete Structures

The maximum line tension that can be applied on a guyed concrete structure is limited by the combined stress on the 7/8" D. A. Bolts, where the maximum guy tension is 18.0 kips on the 1.5:1 slope. The governing design condition, which is considerably less than the ultimate applied tensions that shall be applied on the larger standard conductors for the Hurricane loads (140 mph wind speed.).

9.3.8.2 Steel Structures

Welded steel thru vangs replace the tees and bolts on the concrete pole and these vangs shall be designed to support all of the possible applied loads. Therefore, as provided in the table, the 19#8 guys, the standard guy material, will govern the line tension limit when this guy wire is used. Where 19#6 guys are used, the anchor hardware will govern the line tension limit.

9.3.8.3 Heavy Ice Zone

In the heavy ice zones (NESC 250D zones), standard through bolts, guy tees and single 19 #8 guy wire may be inadequate for larger conductors or bundled configurations. Special design considerations shall be investigated under these conditions.

9.3.8.4 Double Down-guy Assemblies

Double down-guy assemblies shall be used when it is determined that the soil is incapable of supporting the applied load with one anchor or where the loads exceed the allowable guy tension. The double down guy assembly shall consist of one attachment to the pole, a link with two rollers, and two guy wires and two anchors. Double Down-guy assemblies shall use 19#8-guy wires. The anchors shall be separated by at least five (5)-feet.

9.3.8.5 Guy Anchor Groups

All standard guyed structure framings reference a particular Guy/Anchor Group which defines the structure voltage, and in turn provides the required number and size of guys, type of anchor, guy configuration and structure type.

9.3.8.6 Cathodic protection

Guy anchor assemblies shall be provided with cathodic protection by the installation of anodes.

Guy anchor assemblies shall be protected by anodes as shown on the "Guy Anchor Group" detail drawings. Refer to [Section 8.4](#) [Section 8.3](#) for details.

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9.4 Spacing of Dead-End Structures

Dead-end structures shall be required where necessary to carry eccentric loads developed due to conductor tensions. Such dead-end structures shall also be required where necessary as anti-cascading structures, or where they are necessary to facilitate construction. At a maximum spacing, dead-end structure shall be spaced such that no more than two reels of conductor and a single splice are needed between them. While the length of conductor contained on a reel can vary based on the conductor's diameter and unit weight, for most commonly used conductors this will result in a maximum spacing of approximately 4 miles between dead-end structures.

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9.5 Considerations at Major Crossings

The Transmission Lines shall be designed to provide additional reliability at major crossings, in particular along major highway crossings serving as evacuation routes from coastal area. Design and maintenance/replacement activities will apply the following:

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- ~~1.~~ 1. All crossing structures are non-wood, for all voltages
- ~~2.~~ 2. If a wood crossing structure is to be replaced, it shall be replaced with non-wood structure
- ~~3.~~ 3. All highways are crossed at an angle as close to perpendicular as possible
- ~~4.~~ 4. No conductor or shield wire splices within two spans of the crossing span unless expressly approved in writing by Buyer
- ~~5.~~ 5. Where conductor/shield wire splices are unavoidable, or where they are installed during conductor maintenance, install implosive, full tension splices or shunt devices in conjunction with the conventional splice.
- ~~6.~~ 6. Install redundant insulator configurations on all crossings (e.g., braced post insulators, V-string insulators, semi-strain insulators, etc.)
- ~~7.~~ 7. Make shield wire connections more robust at the crossings (e.g., use shackles with nut, vs. shackles with pins, etc.)
- ~~8.~~ 8. No guys on crossing structures if possible, and where guys shall be installed, install double guys
- ~~9.~~ 9. Install highway crossing structures in locations difficult for vehicles to hit, e.g. behind ditches
- ~~10.~~ 10. Provide crash barriers on all highway crossing structures that are not installed in locations difficult for vehicles to hit

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10. STRUCTURE FOUNDATIONS

This section covers the design of structure foundations.

Structure foundations shall be designed to meet the NESC District Loading and Everyday Load Cases, as discussed in Section 5.1; 5.1; and considering the safety factors and deflection limitations discussed in Section 10.2; 10.2. Note that loads shall generally be extracted from pole manufacturer calculations where the structure has been optimized for a high percentage of utilization. Where structures are designed in groups, the reaction used shall be that of the group (as opposed to loads derived from PLS or elsewhere for the specific location). Where manufacturer calculations are not available, foundations shall be designed for the published class/capacity of the pole used (to assure that future modifications on the line do not overestimate the foundation capacity based on the strength of the pole). Where this is not done, a notation shall be made on the plan and profile sheet stating that the foundation was determined considering actual loads in lieu of the structure's capacity.

10.1 Soil Information

The Designer shall obtain as much subsurface information as practicable. The basic sources of information are: (1) actual soil boring samples obtained from geotechnical investigations; (2) Geological maps; (3) data from existing U.S. Dept. of Agriculture maps; or (4) other Geotechnical sources (e. g., DOT files, customer soil records, etc.)

Actual soil data obtained from structure locations is preferable. Generally, soil borings are made at angle and dead-end structures and at intervals of approximately two miles within tangent runs depending on the terrain.

Soil information used in design shall be provided by Seller to Buyer.

10.2 Design Methodology – Lateral Loads

10.2.1 Program Description

The Designer shall use the computer programs Moment Foundation Analysis and Design (MFAD), and Foundation Analysis and Design (FAD) to design for lateral loads.

10.2.2 General Acceptance Criteria

The Designer shall apply the following generally accepted factors of safety for the calculated lateral loads as related to the calculated ultimate capacity of the pile and the acceptable deflection and rotation of the pile:

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Description	Normal Soil
Total Ground Line Deflection ⁽¹⁾	3.0 in.
Total Fnd. Rotation ⁽¹⁾	1.5 deg.
Non Recoverable Deflection	1.0 in.
Non Recoverable Rotation	1.0 deg.
Safety Factor (Tangents)	1.2
Safety Factor (Angles/DEs) NESC 250B	1.0
Safety Factor (Angles/DEs) other load cases	1.65

(4) (1) Additionally, for DE Structures, total foundation rotation and ground-line deflection shall be limited to 0.5-degrees and 1-inch under Everyday load case with all conductors on one side only.

10.3 Foundation Types

10.3.1 Basic Foundation Types

The Designer shall select from the following six basic foundation types typically used by Entergy on steel and concrete pole structures: Direct Embedment Foundation, Steel Pile with Socket Foundation, Cap/Base Plate Foundation, Steel Pile with Anchor Bolt Foundation, Drilled Pier with Anchor Bolts Foundation, and Concrete Pile with Steel or Concrete Pole using Socket Foundation. ~~The Designer shall consult with the Seller's foundation engineer for assistance in determining~~ shall determine suitable foundation types and dimensions. Alternative foundation types shall only be used if expressly approved in writing by Buyer.

Foundation elements shall be designed using applicable material design specifications (e.g. AISC 360 for steel elements, ACI 318 for concrete elements, etc.)

Reveal height for concrete or steel socket piles shall be between 4-feet and 5-feet to facilitate concrete placement and to minimize required excavation for the socketed pole. Foundation height for base-plated poles shall be at least 2-feet, to raise anchor bolts above the ground and the bulk of the wet underbrush. The Designer shall require taller reveals in floodplains, where requested for constructability purposes, or where otherwise needed. The Designer shall not all reveals outside these specifications on the foundation drawings and/or staking sheet.

10.3.2 Grounding and Cathodic Protection

The steel pile shall be designed to act as a ground for both steel and concrete structures. Socket connections and anchor bolt connections using steel piles shall be positively connected between the pole and pile using a #4 copperweld wire connected between the pole and the Two Hole NEMA Pad welded to the pile for a good ground. The cap/base plated connections shall be designed to provide a

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good grounded connection. Steel and concrete poles supported by concrete drilled piers shall be grounded to copperclad steel ground rods.

Where cathodic protection is required, the anodes shall be connected to the NEMA Pads as indicated on the cathodic protection detailed drawings. In general, unless an analysis for corrosion potential indicates otherwise or the structure is located in exposed bedrock, anodes will be required at all guy anchors, and dead-end or large angle structures supported on steel foundations or embedments. In general, unless local conditions warrant (brackish marsh, shared ROW with railroads or pipelines protected by impressed current cathodic protection, etc.) anodes are not usually required for tangent structures on structures supported on concrete foundations or embedments. Reference is made to ~~Section 8.4, Section 8.3 of this Appendix 10.~~

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11. ATTACHMENTS

Attachment_1 – Applicable Standard Framing and Assembly Drawings

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Attachment_2 – NESC and Entergy Clearance Requirements

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Attachment_3 – Quick Estimating Corona Loss Curves

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Attachment_4 – Example ROW

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Attachment_5 – Approved Vendor List¹

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Attachment_6 – Entergy Loading Districts

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¹This¹ This Attachment provides an Approved Vendor List. This Approved Vendor List is in addition to that found in the Scope Book and is considered acceptable for use, and actually preferred.

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Attachment 1: Applicable Standard Framing and Assembly Drawings

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~~ATTACHMENT 1 – APPLICABLE STANDARD FRAMING AND
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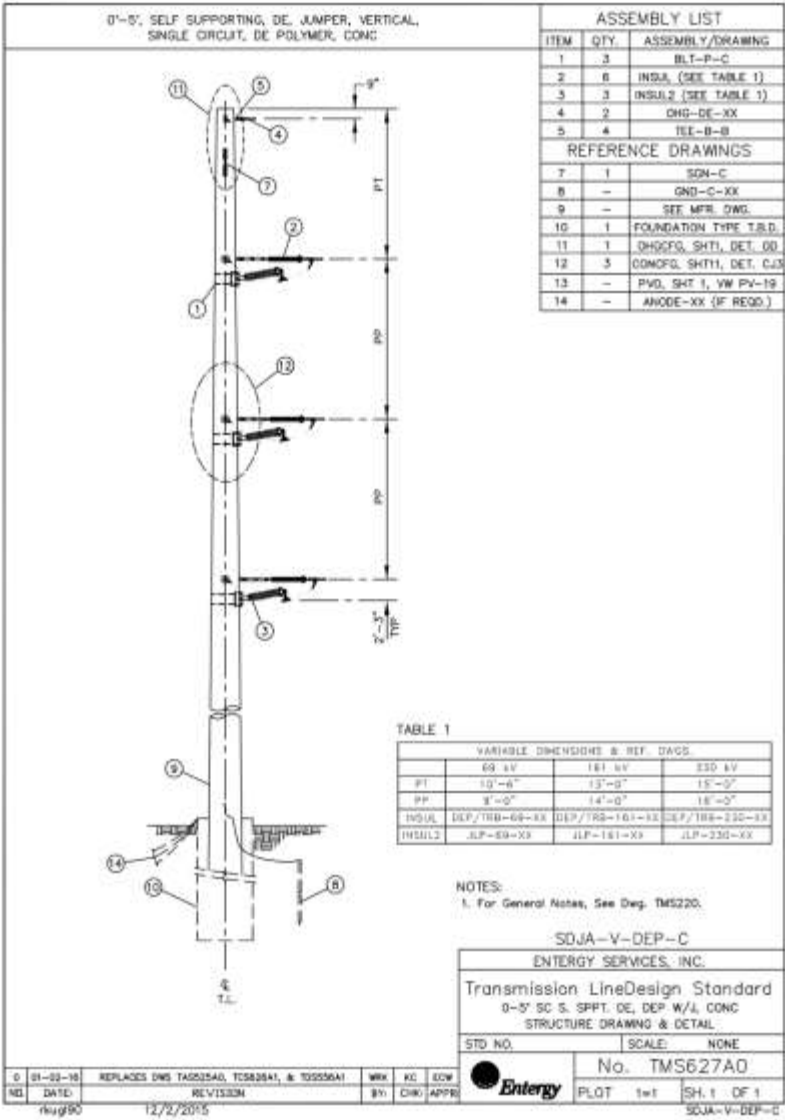
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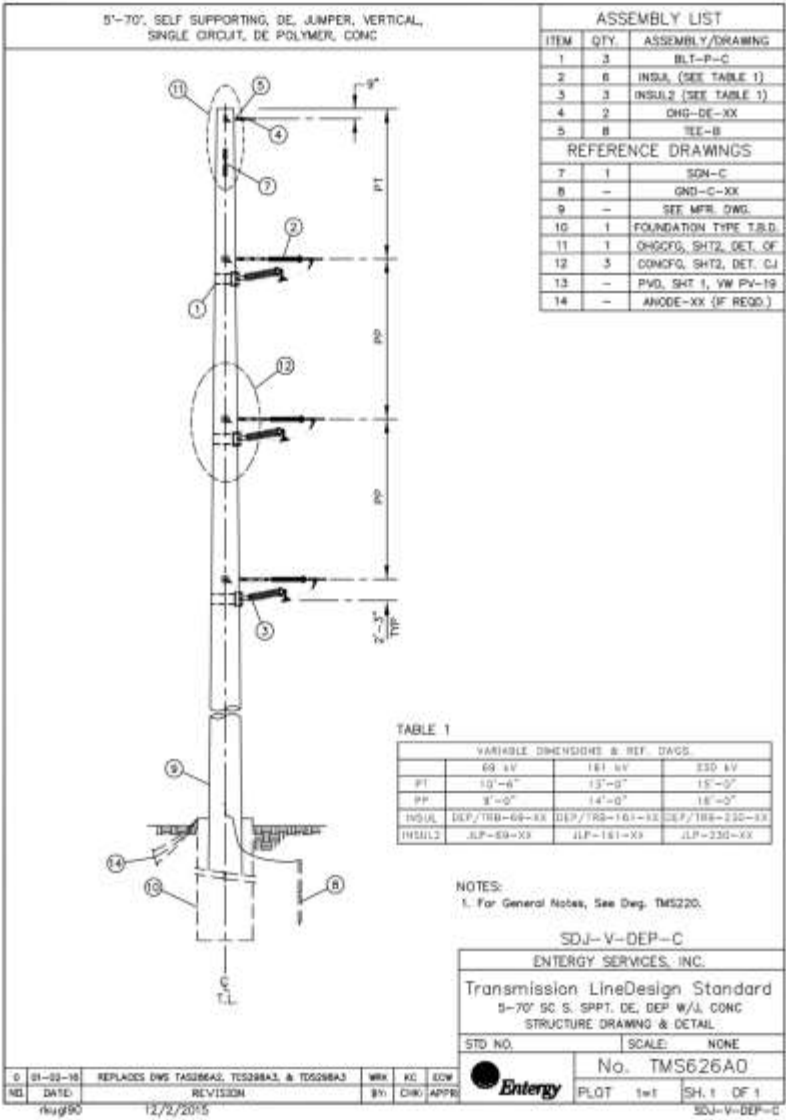
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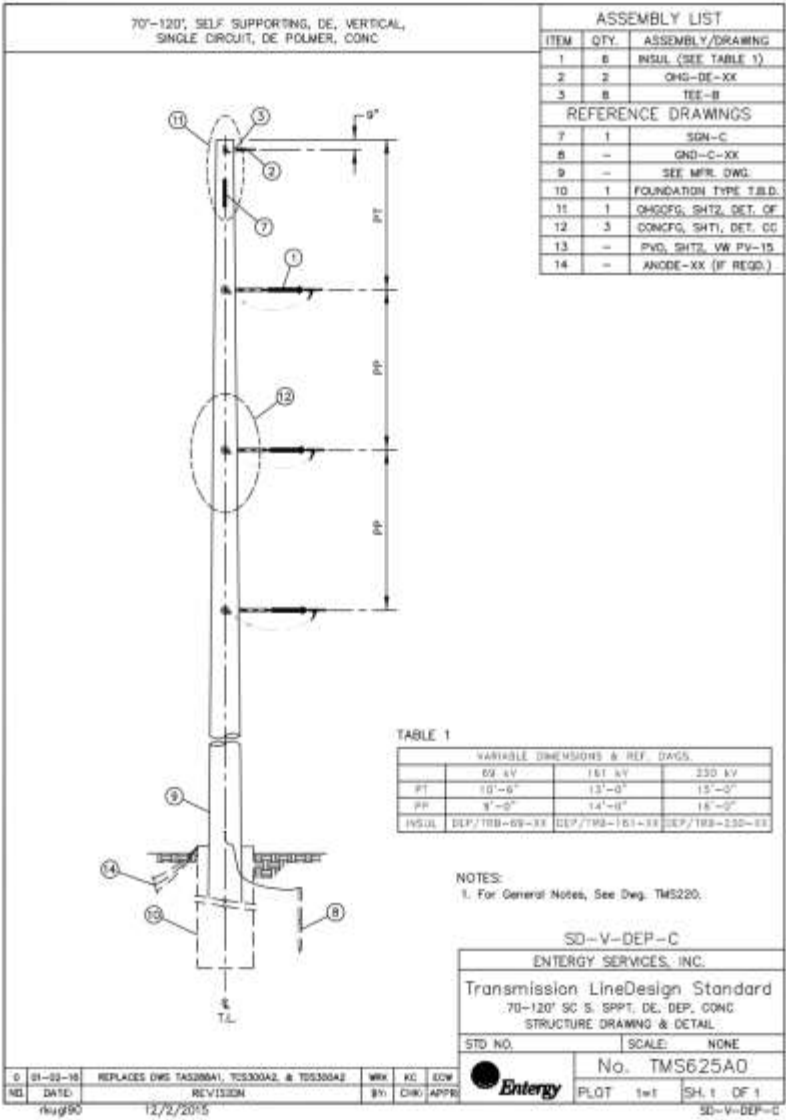
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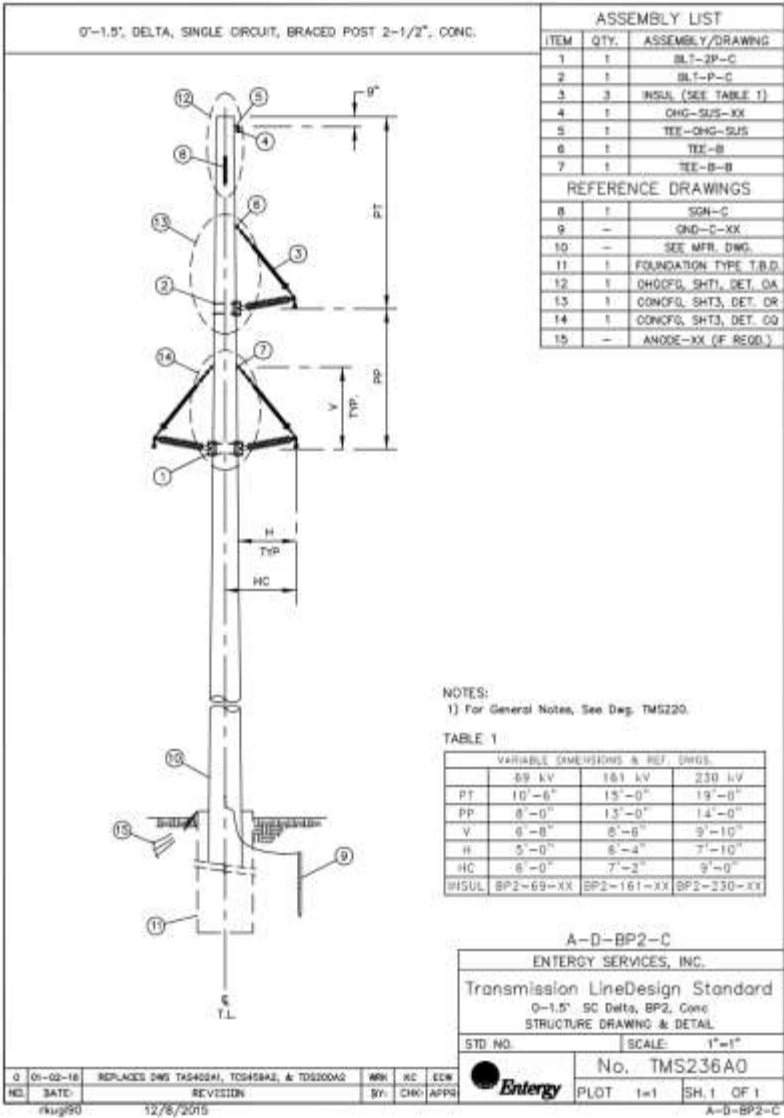
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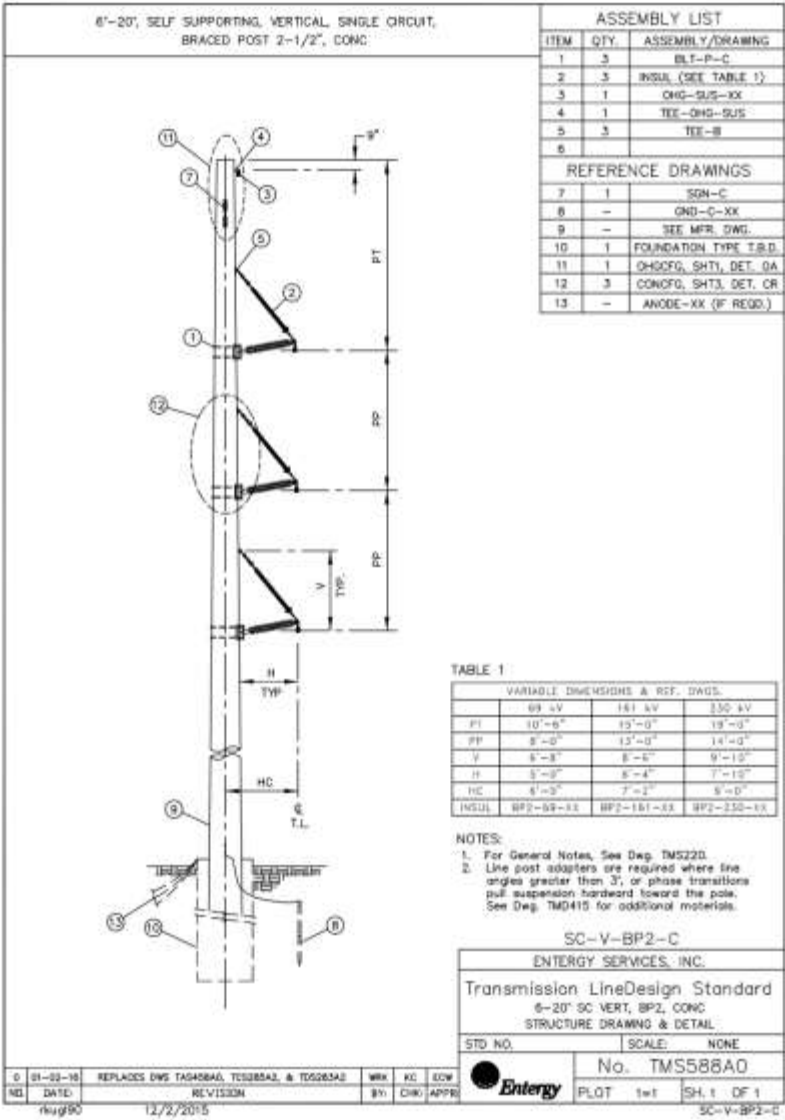
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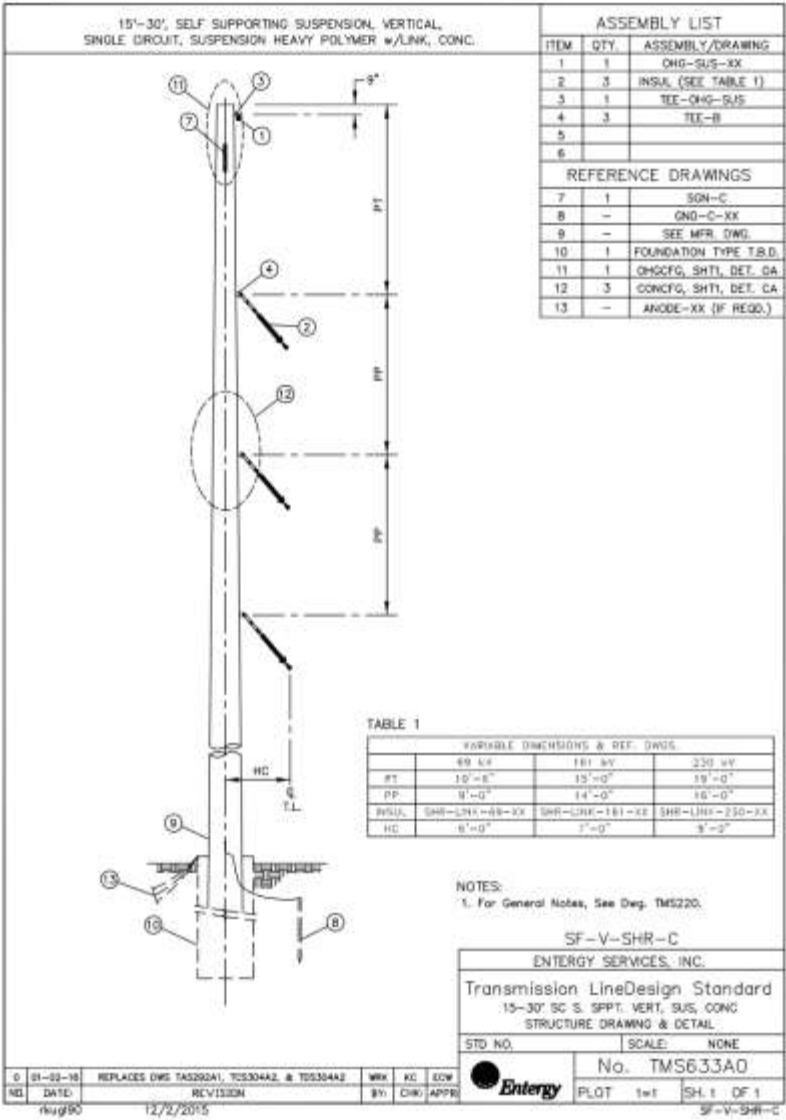
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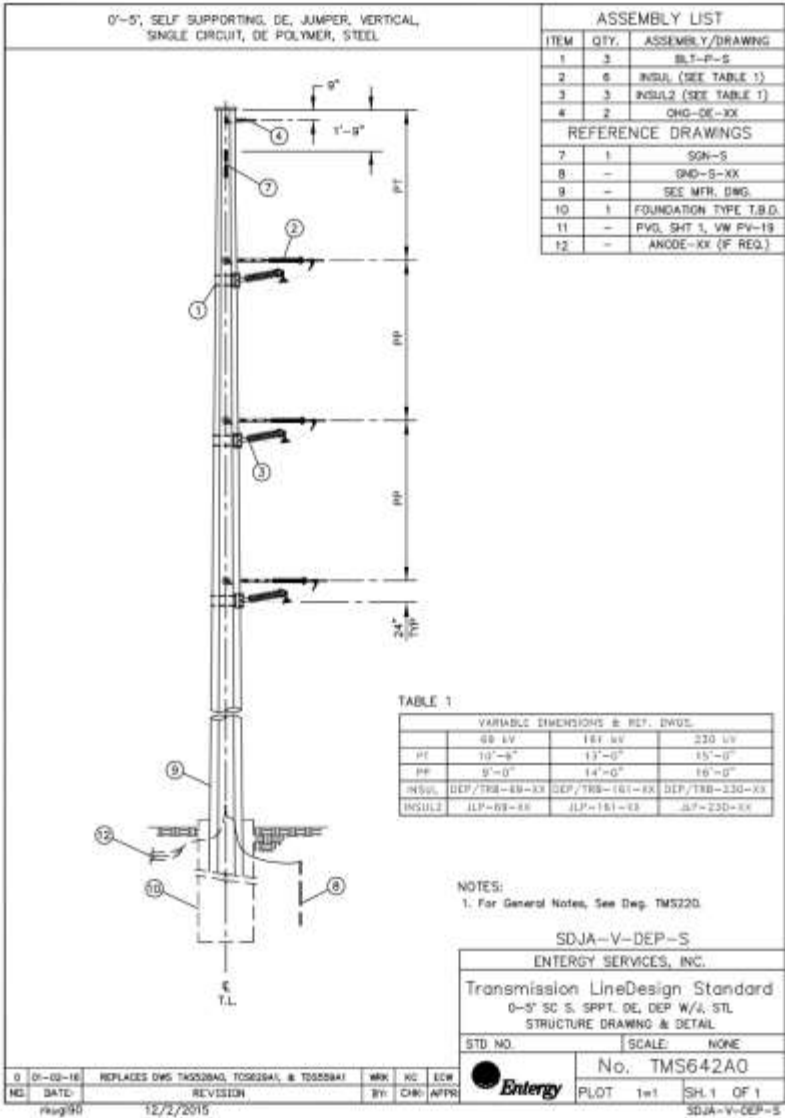
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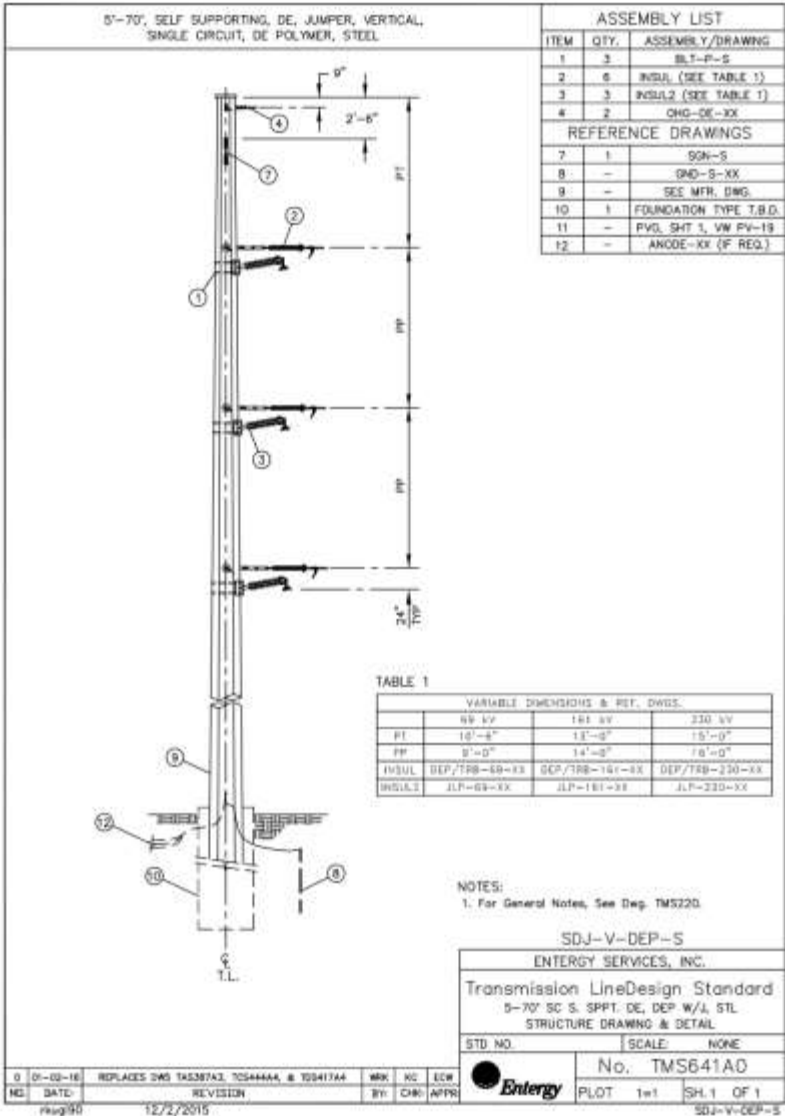
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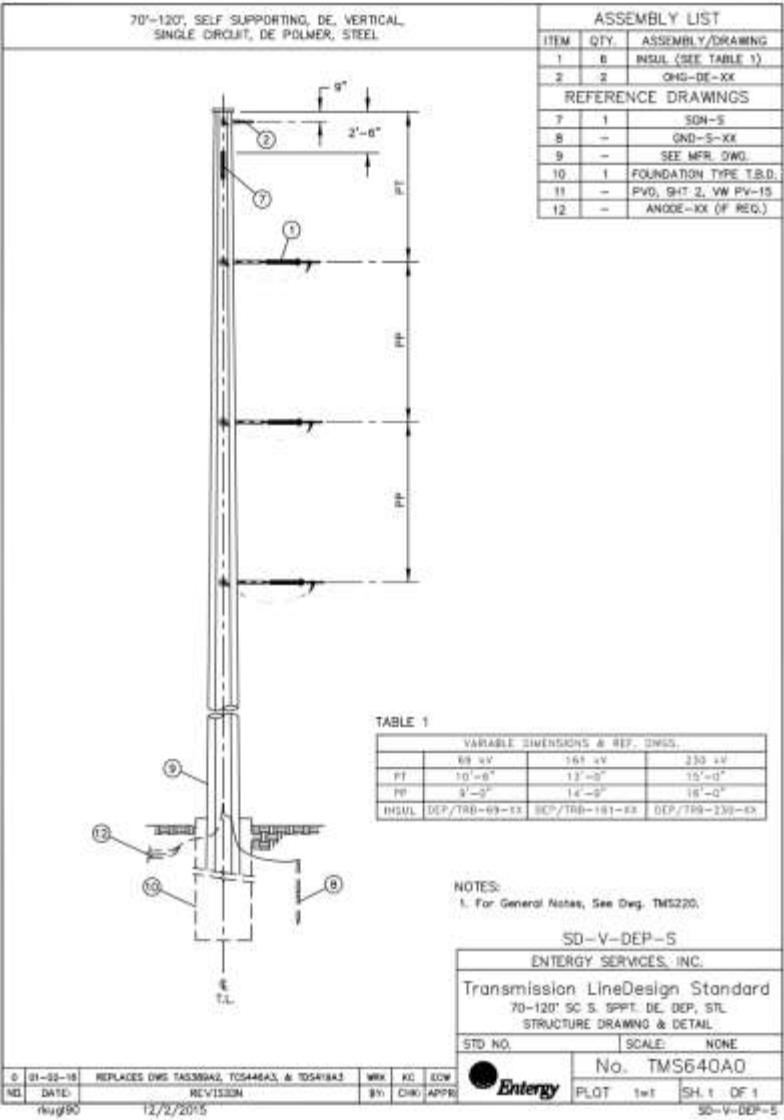
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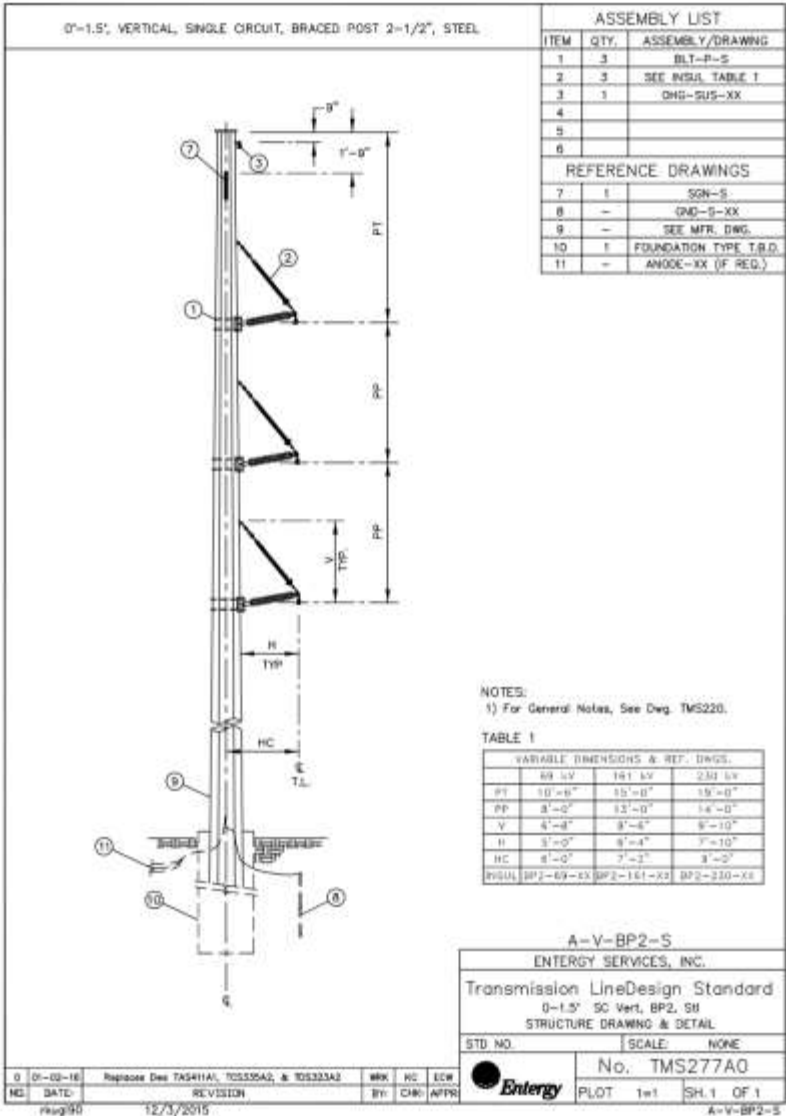
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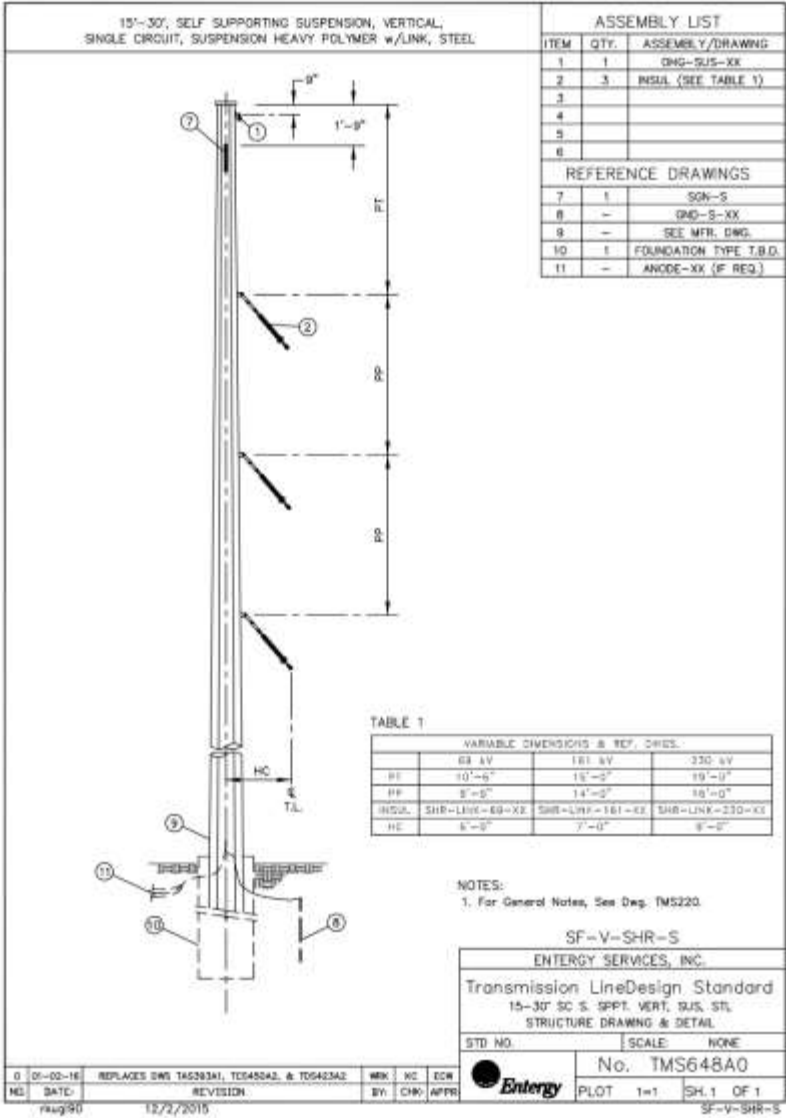


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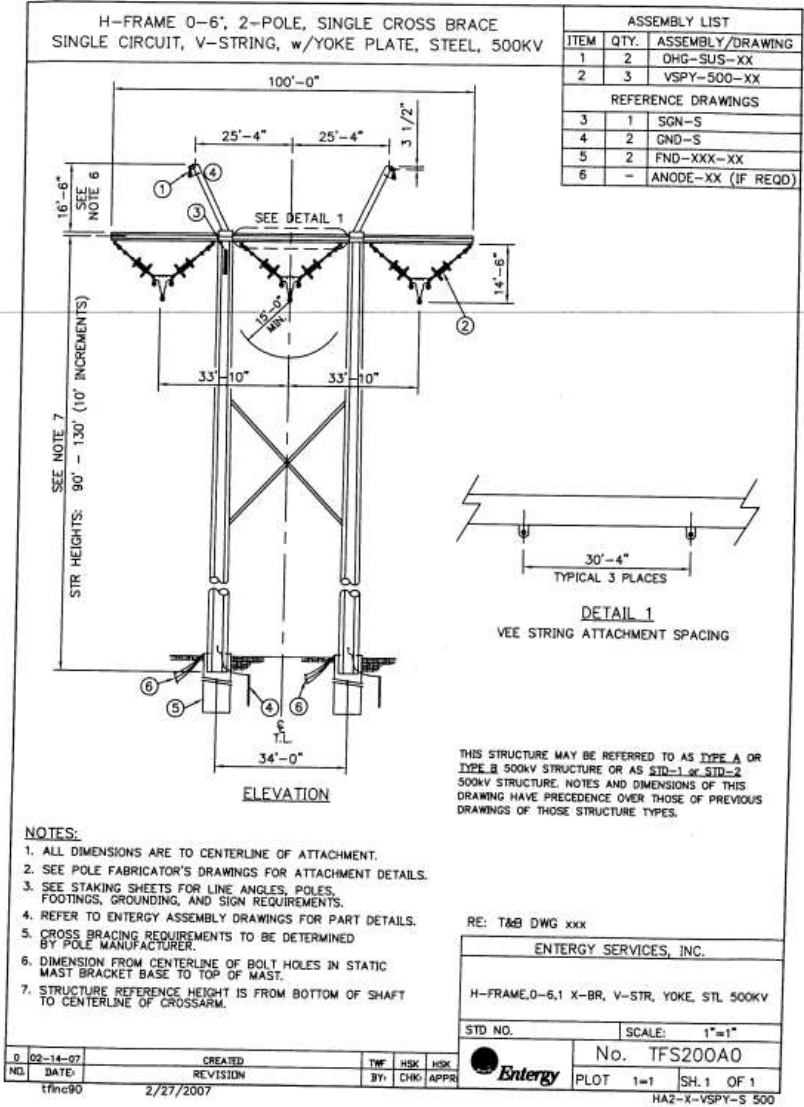
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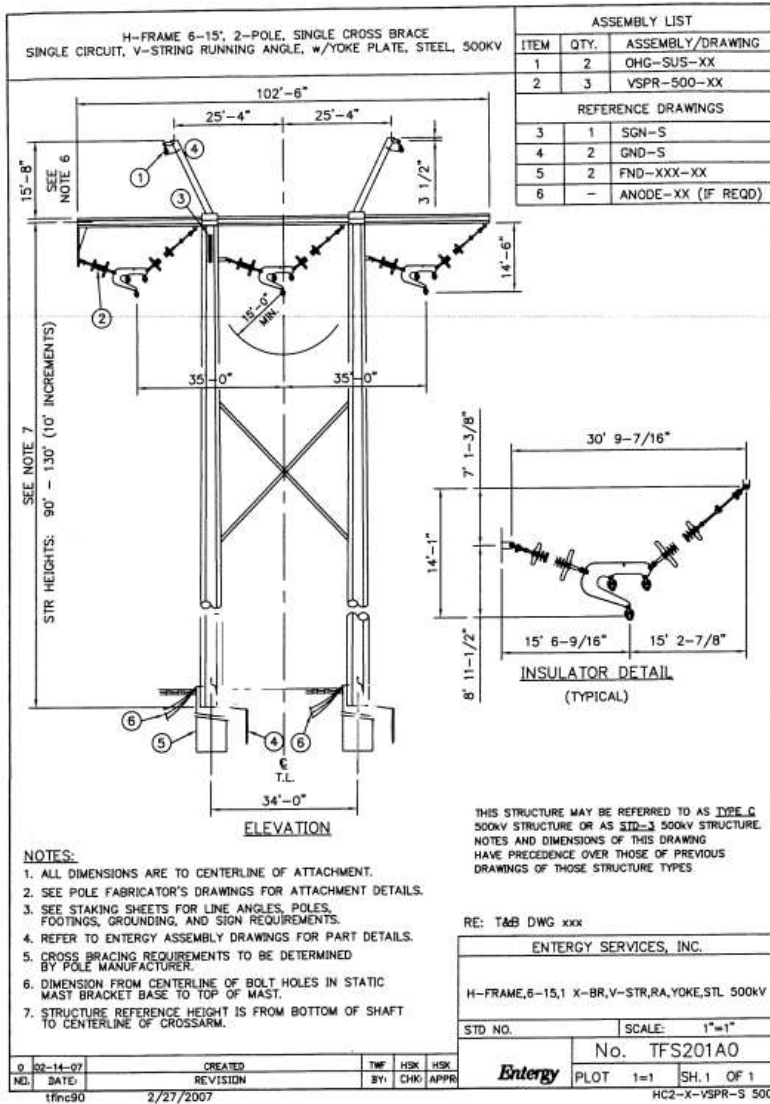
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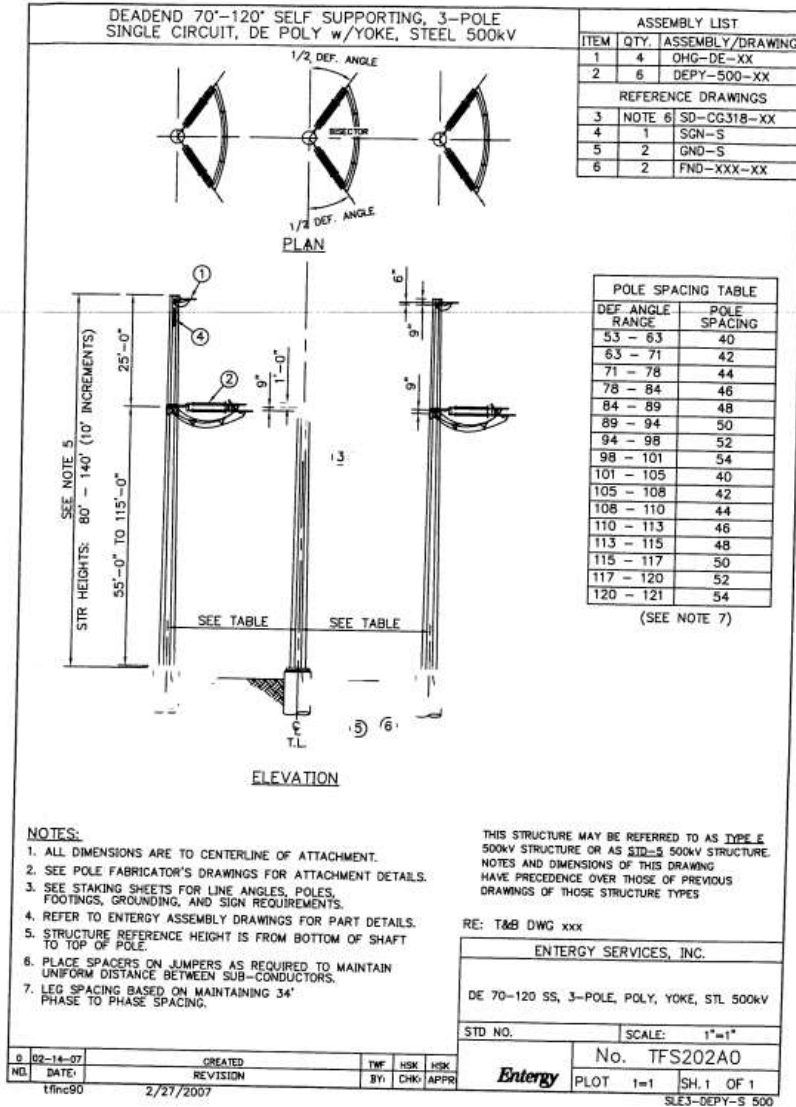
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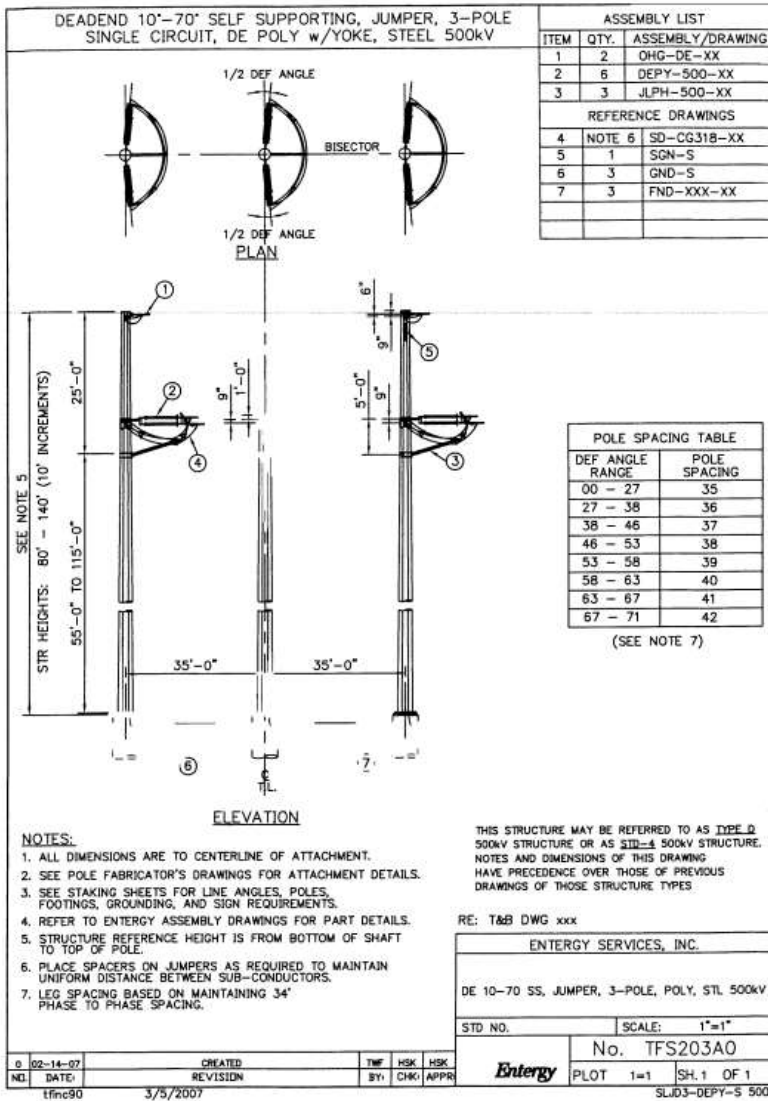
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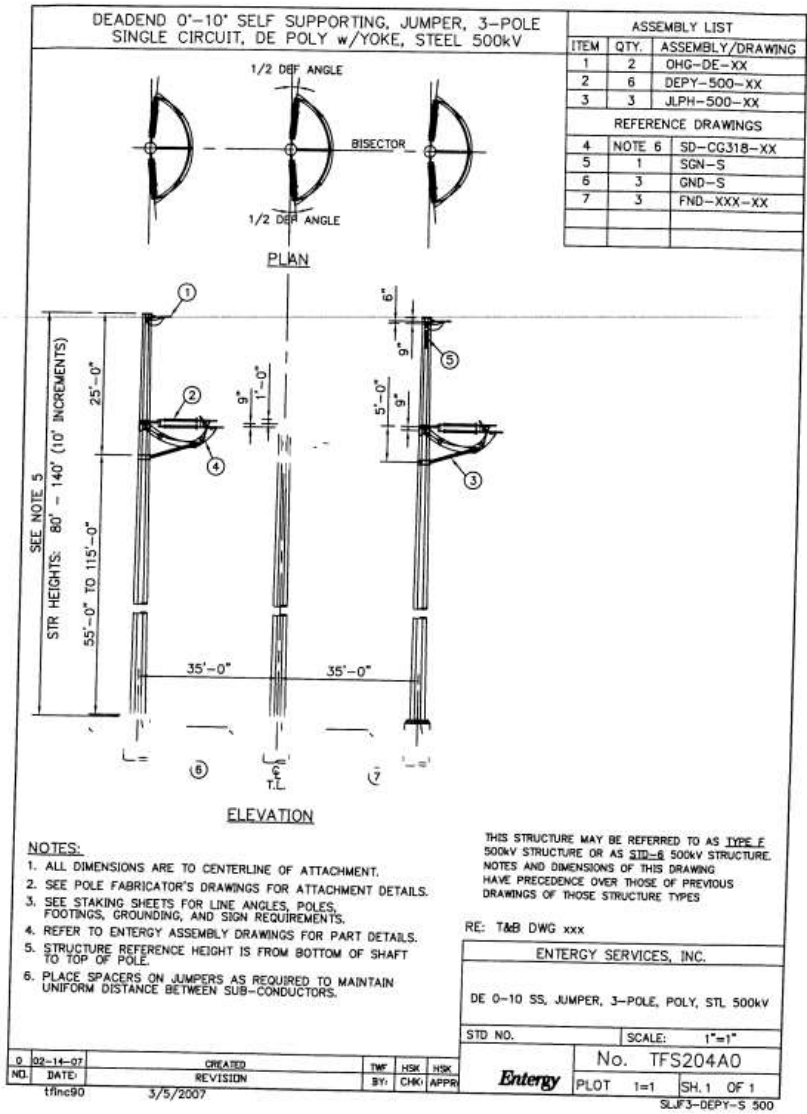
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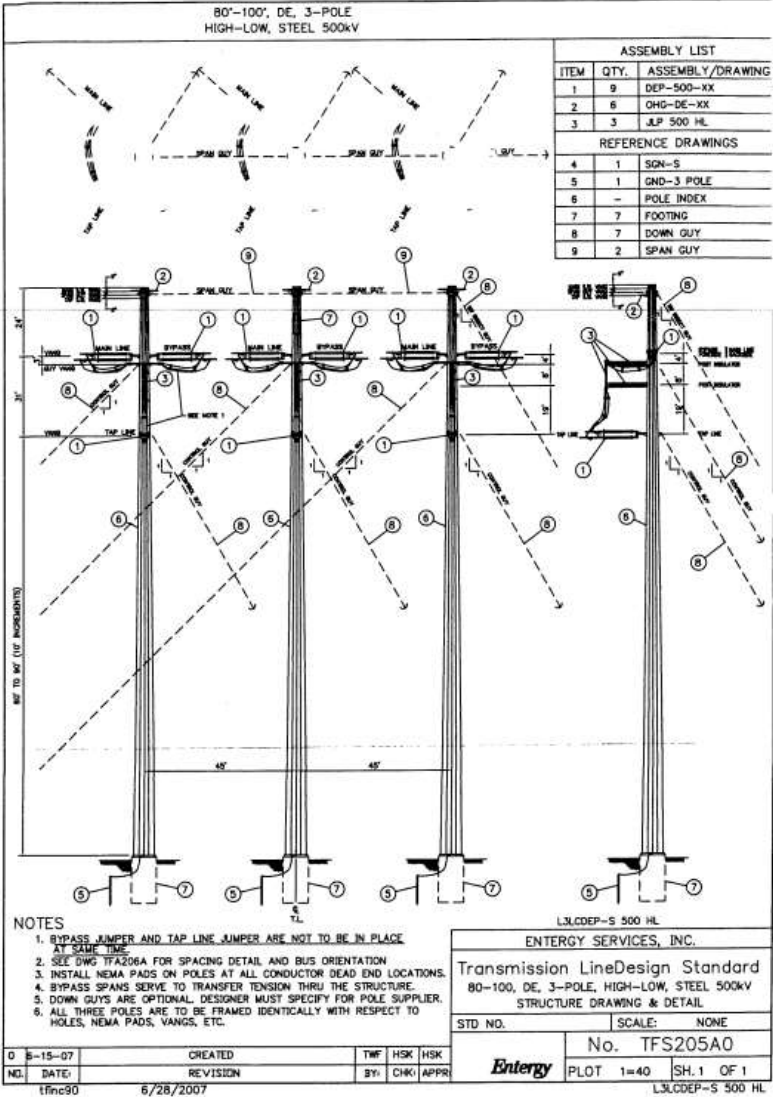
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Attachment 1: Applicable Standard Framing and Assembly Drawings

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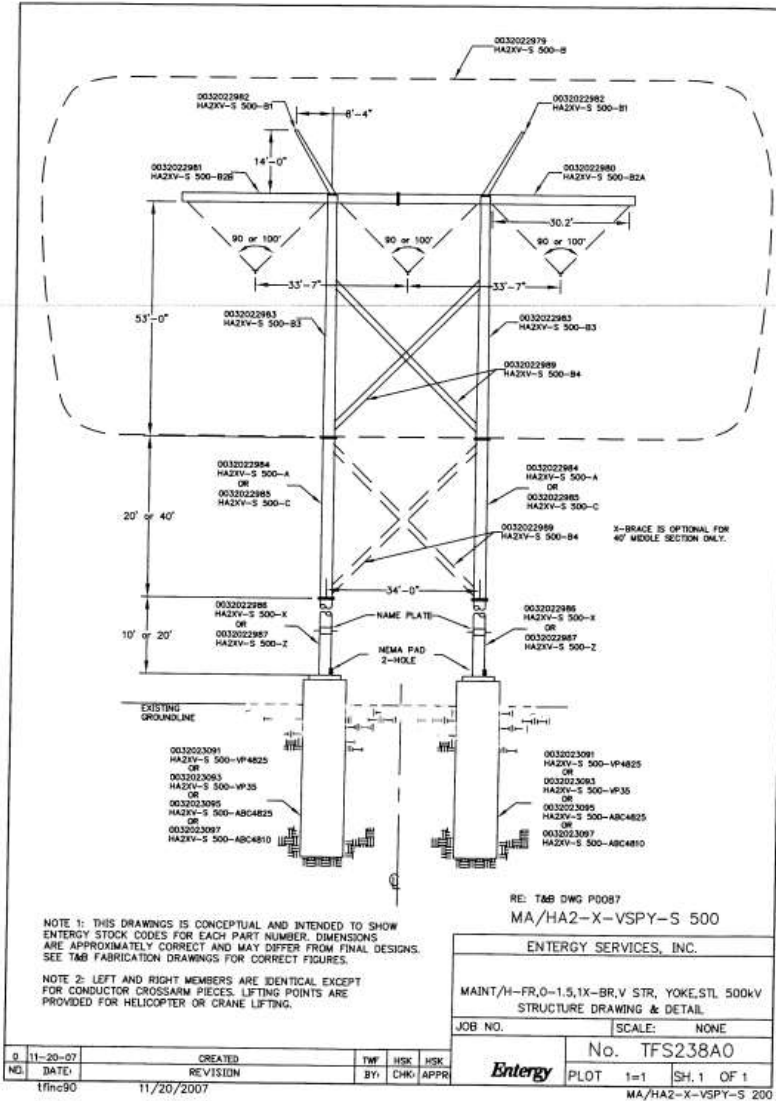
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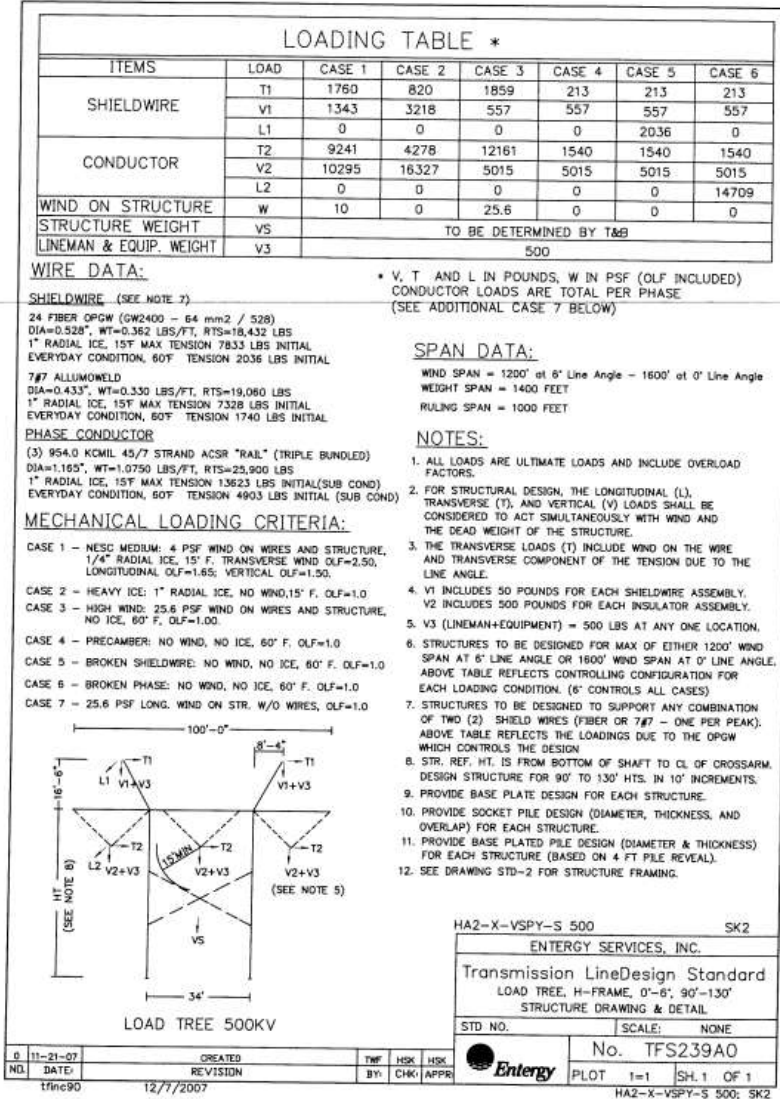
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LOADING TABLE *						
ITEMS	LOAD	CASE 1	CASE 2	CASE 3	CASE 4	CASE 5
SHIELDWIRE	T1	2682	2045	2392	532	532
	V1	1343	3218	557	557	557
	L1	0	0	0	0	5000
CONDUCTOR	T2	14752	10669	15472	3840	3840
	V2	10295	16327	5015	5015	5015
	L2	0	0	0	0	8000
WIND ON STRUCTURE	W	10	0	25.6	0	0
STRUCTURE WEIGHT	V5	TO BE DETERMINED BY T&B				
LINEMAN & EQUIP. WEIGHT	V3	500				

WIRE DATA:

SHIELDWIRE (SEE NOTE 7)
24 FIBER OPGW (DW2400 - 64 mm² / 528)
DIA=0.528", WT=0.362 LBS/FT, RTS=18,432 LBS
1" RADIAL ICE, 15' MAX TENSION 7833 LBS INITIAL
EVERYDAY CONDITION, 60' TENSION 2036 LBS INITIAL
7/7 ALLUMOWELD
DIA=0.433", WT=0.330 LBS/FT, RTS=19,060 LBS
1" RADIAL ICE, 15' MAX TENSION 7328 LBS INITIAL
EVERYDAY CONDITION, 60' TENSION 1740 LBS INITIAL

PHASE CONDUCTOR
(3) 954.0 KCMIL 45/7 STRAND ACSR "RAIL" (TRIPLE BUNDLED)
DIA=1.165", WT=1.0750 LBS/FT, RTS=25,900 LBS
1" RADIAL ICE, 15' MAX TENSION 13623 LBS INITIAL (SUB COND)
EVERYDAY CONDITION, 60' TENSION 4903 LBS INITIAL (SUB COND)

MECHANICAL LOADING CRITERIA:

CASE 1 - NESC MEDIUM: 4 PSF WIND ON WIRES AND STRUCTURE, 1/4" RADIAL ICE, 15' F. TRANSVERSE WIND OLF=2.50, LONGITUDINAL OLF=1.65; VERTICAL OLF=1.50.
CASE 2 - HEAVY ICE: 1" RADIAL ICE, NO WIND, 15' F. OLF=1.0
CASE 3 - HIGH WIND: 25.6 PSF WIND ON WIRES AND STRUCTURE, NO ICE, 60' F. OLF=1.00.
CASE 4 - PRECAMBER: NO WIND, NO ICE, 60' F. OLF=1.0
CASE 5 - BROKEN SHIELDWIRE: NO WIND, NO ICE, 60' F. OLF=1.0
CASE 6 - UNBALANCED PHASE: NO WIND, NO ICE, 60' F. OLF=1.0
CASE 7 - 25.6 PSF LONG. WIND ON STR. W/O WIRES, OLF=1.0

SPAN DATA:
WIND SPAN = 1000' at 15' Line Angle
WEIGHT SPAN = 1400 FEET
RULING SPAN = 1000 FEET

NOTES:

- ALL LOADS ARE ULTIMATE LOADS AND INCLUDE OVERLOAD FACTORS.
- FOR STRUCTURAL DESIGN, THE LONGITUDINAL (L), TRANSVERSE (T), AND VERTICAL (V) LOADS SHALL BE CONSIDERED TO ACT SIMULTANEOUSLY WITH WIND AND THE DEAD WEIGHT OF THE STRUCTURE.
- THE TRANSVERSE LOADS (T) INCLUDE WIND ON THE WIRE AND TRANSVERSE COMPONENT OF THE TENSION DUE TO THE LINE ANGLE.
- V1 INCLUDES 50 POUNDS FOR EACH SHIELDWIRE ASSEMBLY. V2 INCLUDES 500 POUNDS FOR EACH INSULATOR ASSEMBLY.
- V3 (LINEMAN-EQUIPMENT) = 500 LBS AT ANY ONE LOCATION.
- STRUCTURES TO BE DESIGNED FOR 1000' WIND SPAN AT 15' LINE ANGLE. PROVIDE SPAN AND ANGLE CHART FOR 5' TO 14' LINE ANGLE.
- STRUCTURES TO BE DESIGNED TO SUPPORT ANY COMBINATION OF TWO (2) SHIELD WIRES (FIBER OR 7/7 - ONE PER PEAK). ABOVE TABLE REFLECTS THE LOADINGS DUE TO THE OPGW WHICH CONTROLS THE DESIGN.
- STR. REF. HT. IS FROM BOTTOM OF SHAFT TO CL. OF CROSSARM. DESIGN STRUCTURE FOR 90' TO 130' HTS. IN 10' INCREMENTS.
- PROVIDE BASE PLATE DESIGN FOR EACH STRUCTURE.
- PROVIDE SOCKET PILE DESIGN (DIAMETER, THICKNESS, AND OVERLAP) FOR EACH STRUCTURE.
- PROVIDE BASE PLATED PILE DESIGN (DIAMETER & THICKNESS) FOR EACH STRUCTURE (BASED ON 4 FT PILE REVEAL).
- SEE DRAWING STD-3 FOR STRUCTURE FRAMING.

HC2-X-VSPR-S 500 SK3

ENTERGY SERVICES, INC.

Transmission Line Design Standard
LOAD TREE, H-FRAME, 6'-15', 90'-130'
STRUCTURE DRAWING & DETAIL

STD NO. SCALE: NONE

No. TFS240A0

Entergy

PLOT 1=1 SH. 1 OF 1

HC2-X-VSPR-S 500; SK3

0 11-21-07 CREATED TWF HSK HSK
NO. DATE REVISION BY: CHK: APPR:
tmc90 12/7/2007

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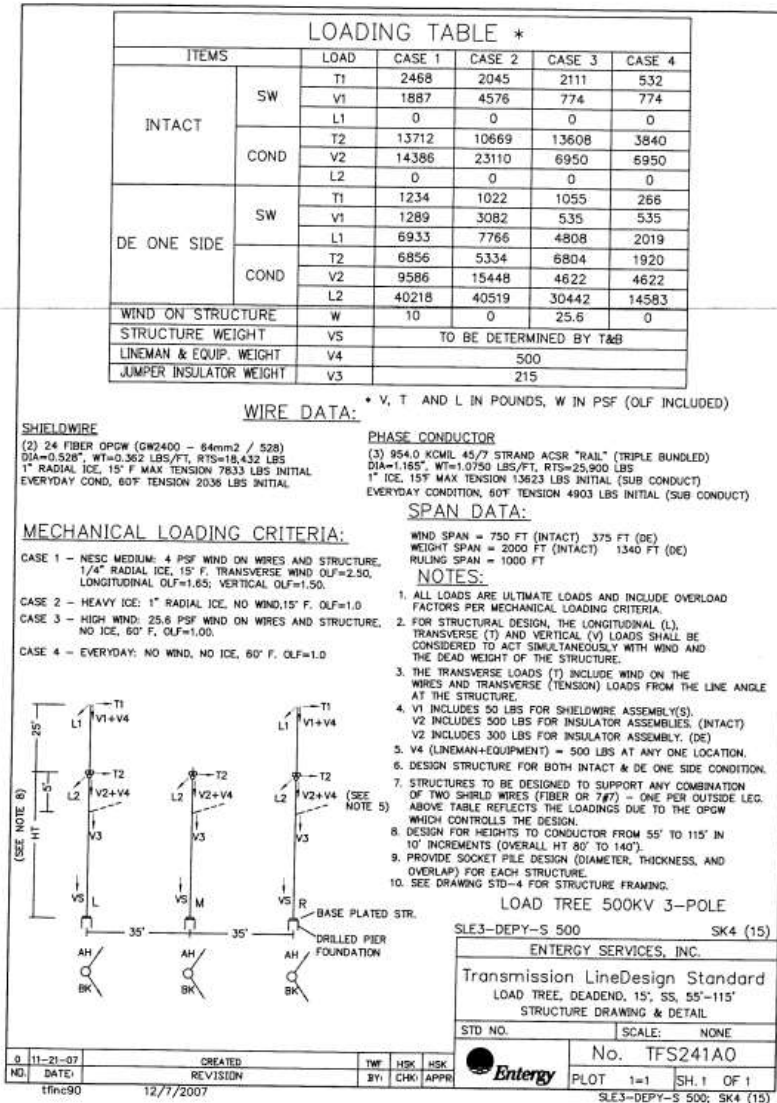
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Attachment 1: Applicable Standard Framing and Assembly Drawings

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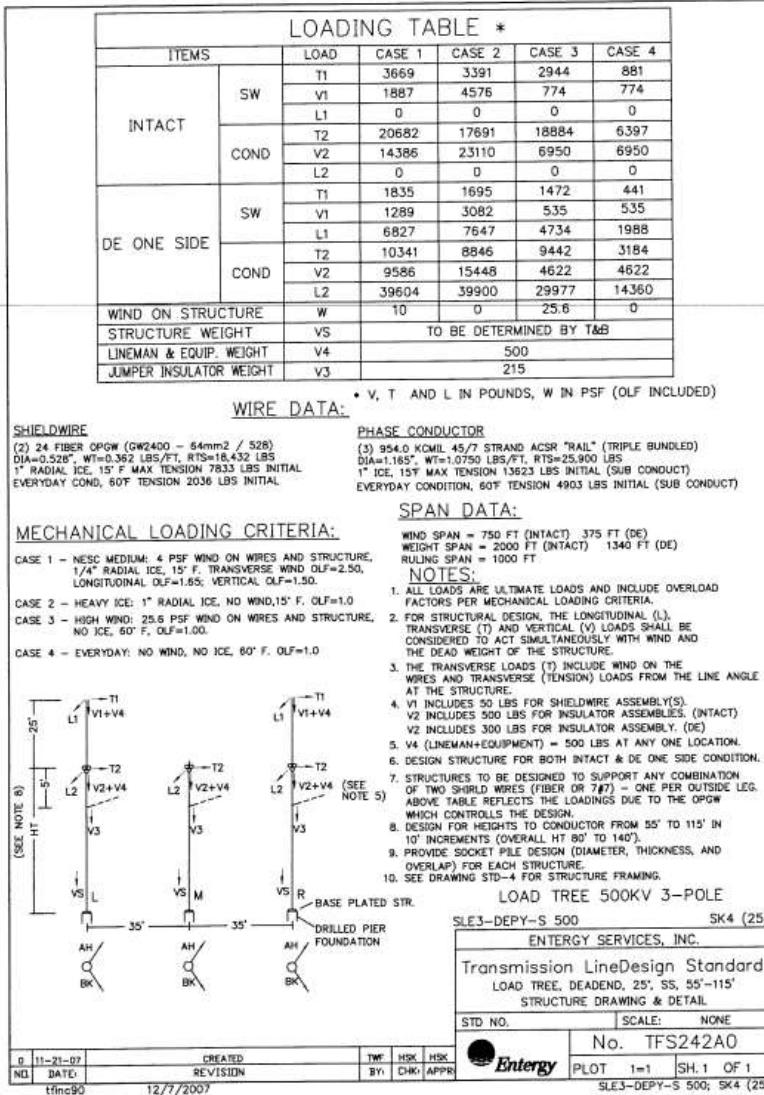
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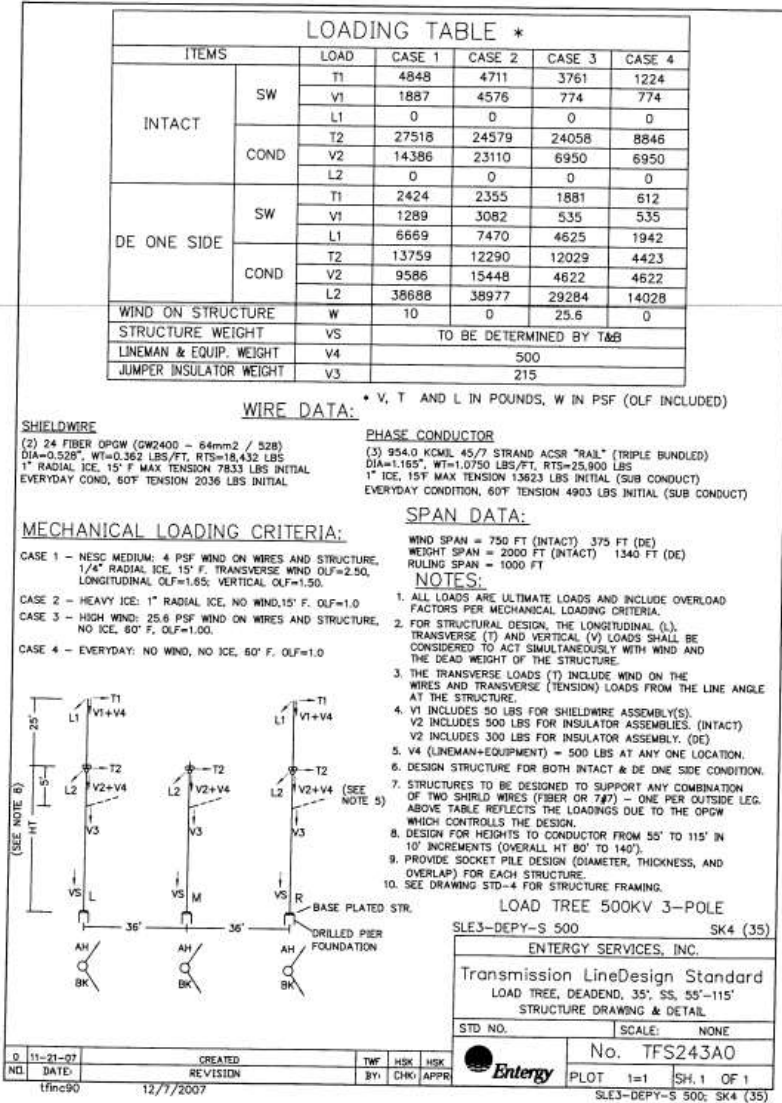
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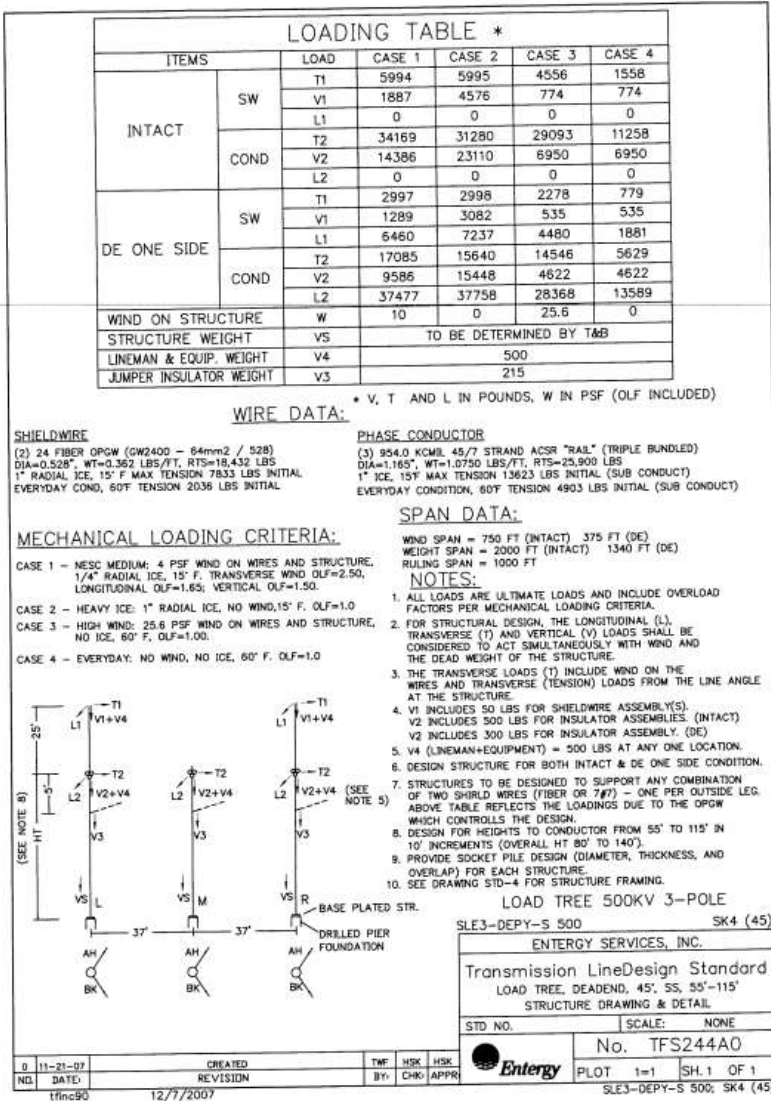
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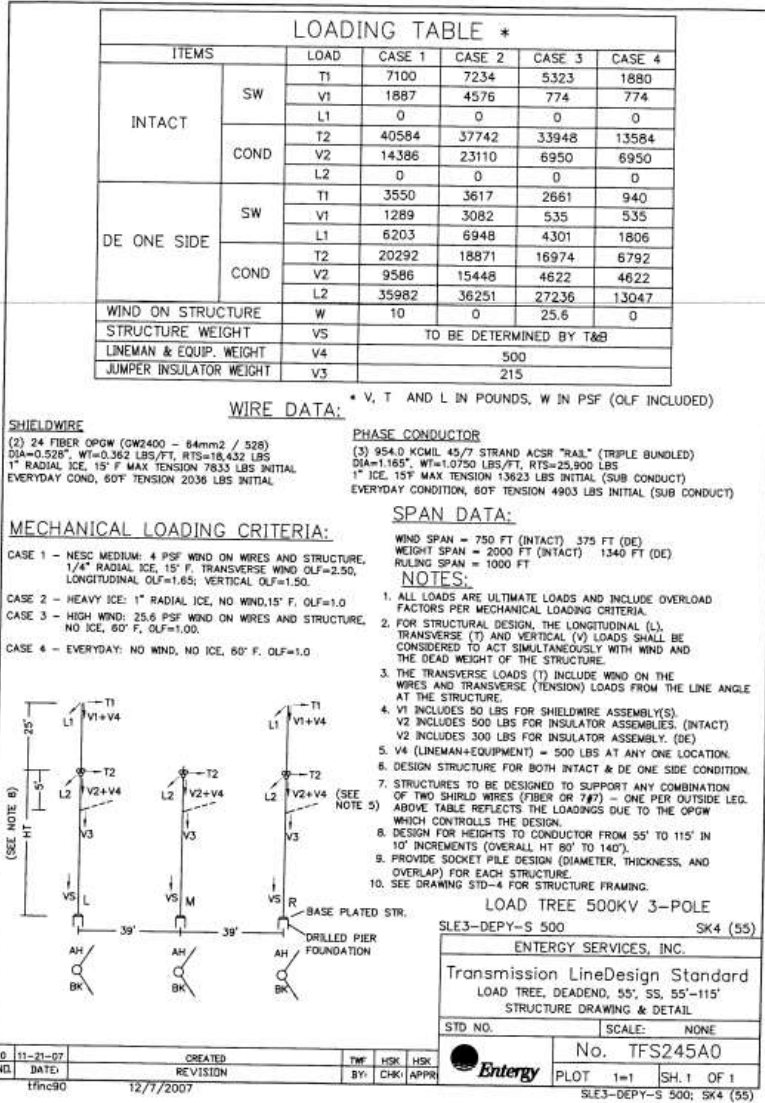
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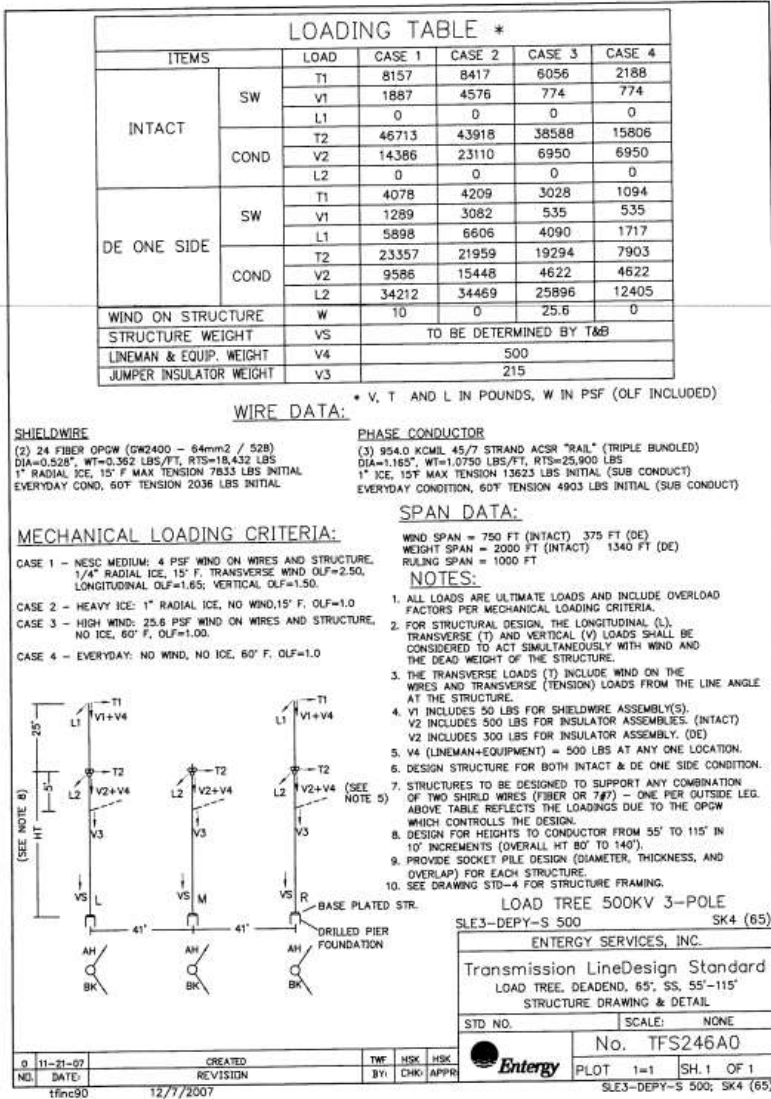
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LOADING TABLE *						
ITEMS		LOAD	CASE 1	CASE 2	CASE 3	CASE 4
INTACT	SW	T1	8664	8986	6407	2336
		V1	1887	4576	774	774
		L1	0	0	0	0
	COND	T2	49656	46883	40815	16873
		V2	14386	23110	6950	6950
		L2	0	0	0	0
DE ONE SIDE	SW	T1	4332	4493	3204	1168
		V1	1289	3082	535	535
		L1	5728	6416	3972	1668
	COND	T2	24828	23441	20408	8437
		V2	9586	15448	4622	4622
		L2	33229	33478	25152	12049
WIND ON STRUCTURE		W	10	0	25.6	0
STRUCTURE WEIGHT		VS	TO BE DETERMINED BY TAB			
LINEMAN & EQUIP. WEIGHT		V3	500			

* V, T AND L IN POUNDS, W IN PSF (OLF INCLUDED)

WIRE DATA:

SHIELDWIRE

(2) 24 FIBER OPGW (GW2400 - 64mm2 / 528)
 DIA=0.528", WT=0.362 LBS/FT, RTS=18,432 LBS
 1" RADIAL ICE, 15' F MAX TENSION 7833 LBS INITIAL
 EVERYDAY COND, 60' F TENSION 2036 LBS INITIAL

PHASE CONDUCTOR

(3) 954.0 KCMIL 45/7 STRAND ACSR "RAIL" (TRIPLE BUNDLED)
 DIA=1.165", WT=1.0750 LBS/FT, RTS=25,900 LBS
 1" ICE, 15' F MAX TENSION 13623 LBS INITIAL (SUB CONDUCT)
 EVERYDAY CONDITION, 60' F TENSION 4903 LBS INITIAL (SUB CONDUCT)

MECHANICAL LOADING CRITERIA:

CASE 1 - NESC MEDIUM: 4 PSF WIND ON WIRES AND STRUCTURE,
 1/4" RADIAL ICE, 15' F. TRANSVERSE WIND OLF=2.50,
 LONGITUDINAL OLF=1.65; VERTICAL OLF=1.50.

CASE 2 - HEAVY ICE: 1" RADIAL ICE, NO WIND, 15' F, OLF=1.0
 CASE 3 - HIGH WIND: 25.6 PSF WIND ON WIRES AND STRUCTURE,
 NO ICE, 60' F, OLF=1.00.

CASE 4 - EVERYDAY: NO WIND, NO ICE, 60' F, OLF=1.0

SPAN DATA:

WIND SPAN = 750 FT (INTACT) .375 FT (DE)
 WEIGHT SPAN = 2000 FT (INTACT) 1340 FT (DE)
 RULING SPAN = 1000 FT

NOTES:

- ALL LOADS ARE ULTIMATE LOADS AND INCLUDE OVERLOAD FACTORS PER MECHANICAL LOADING CRITERIA.
- FOR STRUCTURAL DESIGN, THE LONGITUDINAL (L), TRANSVERSE (T) AND VERTICAL (V) LOADS SHALL BE CONSIDERED TO ACT SIMULTANEOUSLY WITH WIND AND THE DEAD WEIGHT OF THE STRUCTURE.
- THE TRANSVERSE LOADS (T) INCLUDE WIND ON THE WIRES AND TRANSVERSE (TENSION) LOADS FROM THE LINE ANGLE AT THE STRUCTURE.
- V1 INCLUDES 50 LBS FOR SHIELDWIRE ASSEMBLY(S). V2 INCLUDES 500 LBS FOR INSULATOR ASSEMBLIES. (INTACT) V2 INCLUDES 300 LBS FOR INSULATOR ASSEMBLY. (DE)
- V3 (LINEMAN+EQUIPMENT) = 500 LBS AT ANY ONE LOCATION.
- DESIGN STRUCTURE FOR BOTH INTACT & DE ONE SIDE CONDITION.
- STRUCTURES TO BE DESIGNED TO SUPPORT ANY COMBINATION OF TWO SHIELD WIRES (FIBER OR 7FT) - ONE PER OUTSIDE LEG. ABOVE TABLE REFLECTS THE LOADINGS DUE TO THE OPGW WHICH CONTROLS THE DESIGN.
- DESIGN FOR HEIGHTS TO CONDUCTOR FROM 55' TO 115' IN 10' INCREMENTS (OVERALL HT 80' TO 140').
- PROVIDE SOCKET PILE DESIGN (DIAMETER, THICKNESS, AND OVERLAP) FOR EACH STRUCTURE.
- SEE DRAWING STD-5 FOR STRUCTURE FRAMING.

LOAD TREE 500KV 3-POLE

SLE3-DEPY-S 500 SK5 (70)

ENTERGY SERVICES, INC.

Transmission LineDesign Standard

LOAD TREE, DEADEND, 70', SS, 55'-115'

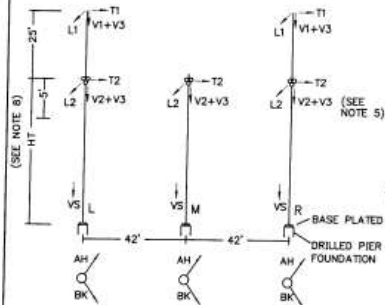
STRUCTURE DRAWING & DETAIL

STD NO. SCALE: NONE

No. TFS247A0

PLOT 1=1 SH. 1 OF 1

SLE3-DEPY-S 500; SK5 (70)



0 11-21-07	CREATED	TSF	HSK	HSK
NO. DATE:	REVISION	BY:	CHK:	APPR:
tfnc90	12/7/2007			

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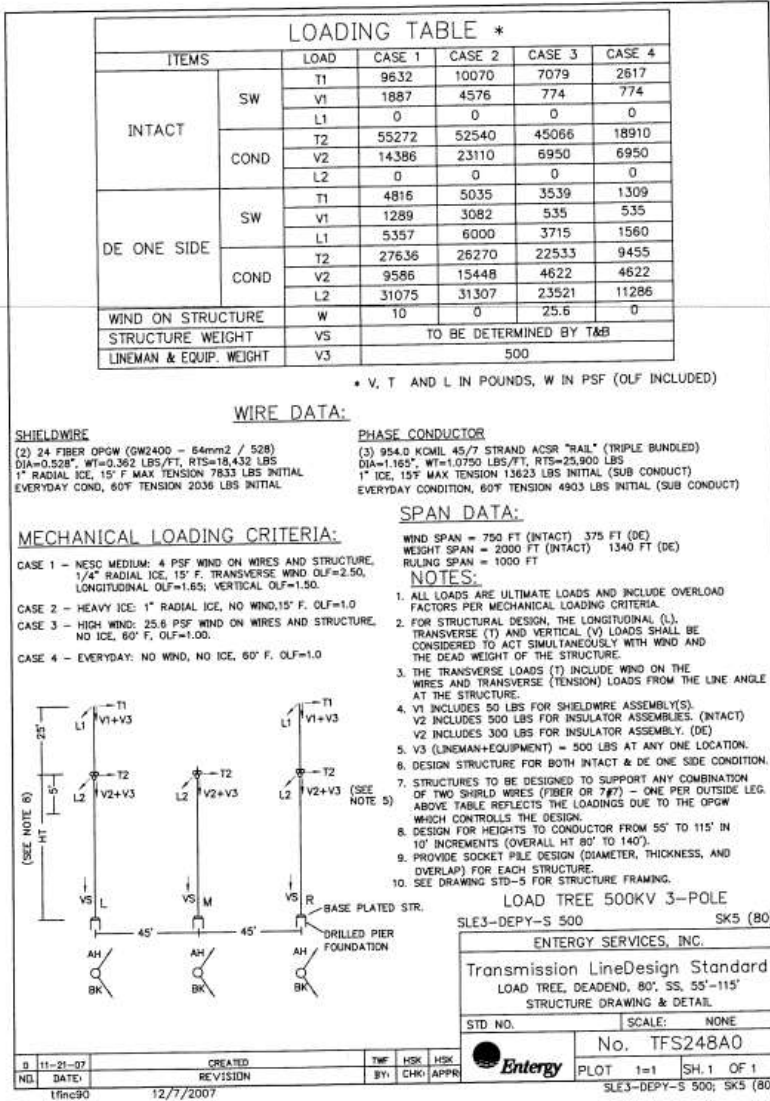
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Attachment 1: Applicable Standard Framing and Assembly Drawings

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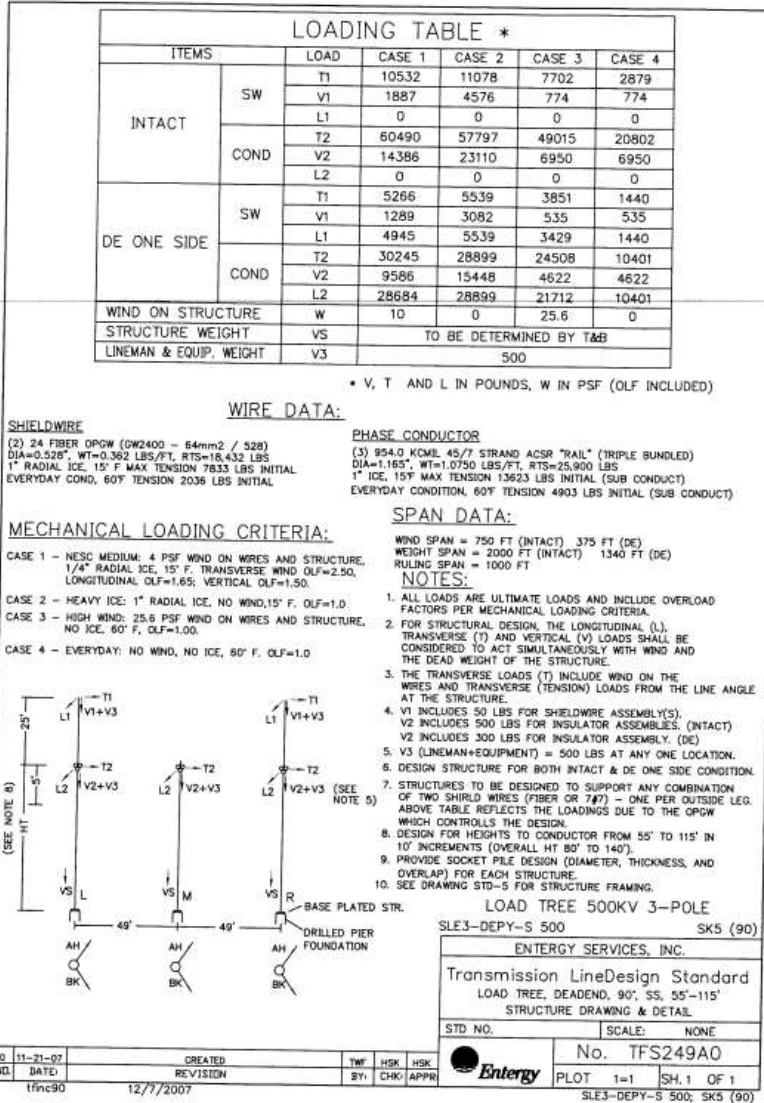
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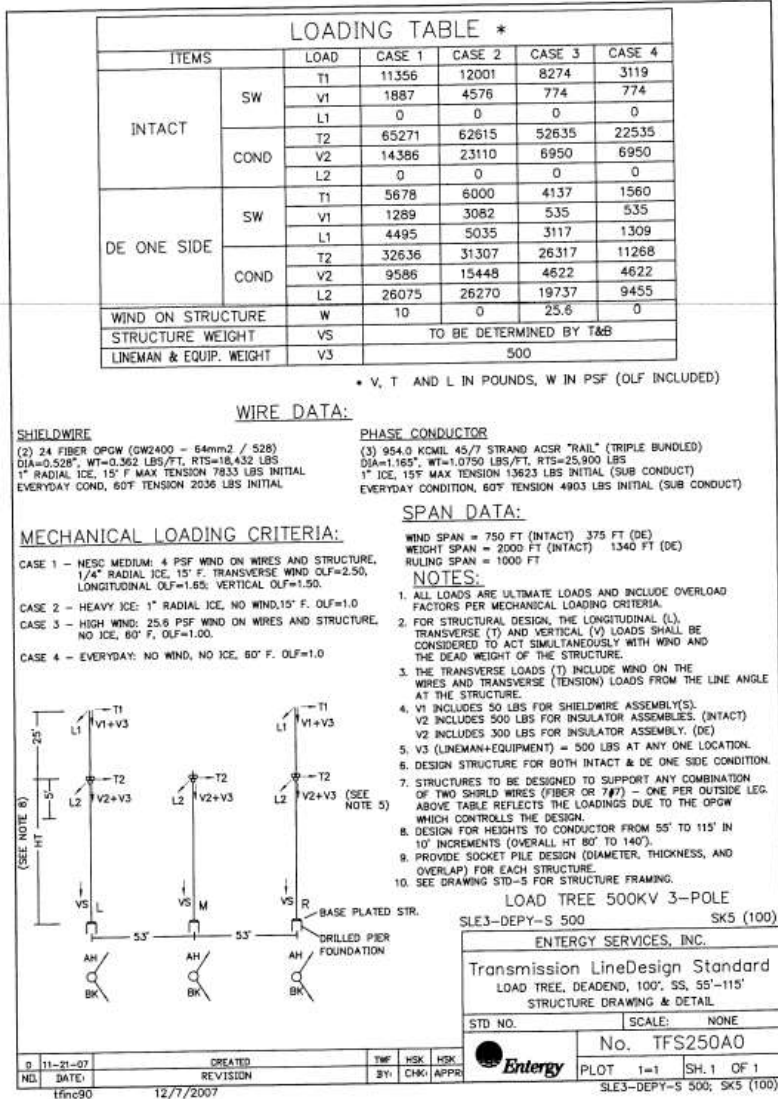
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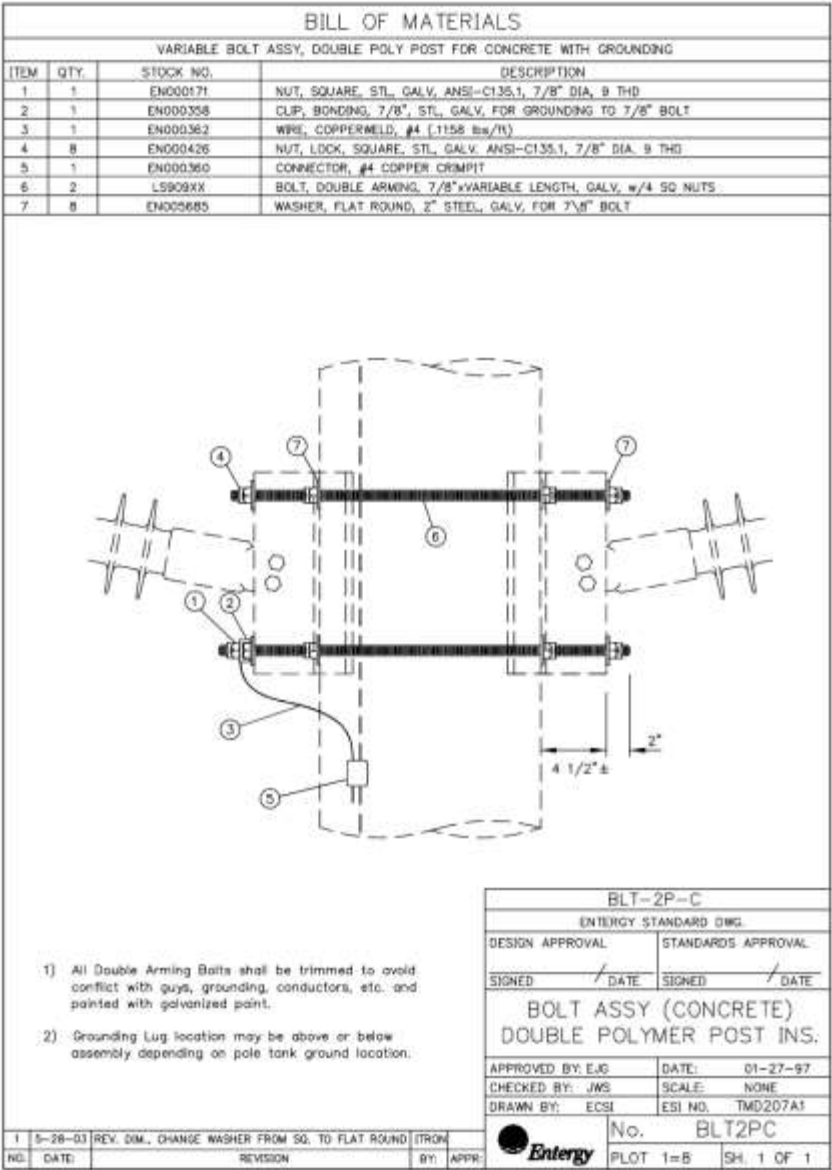
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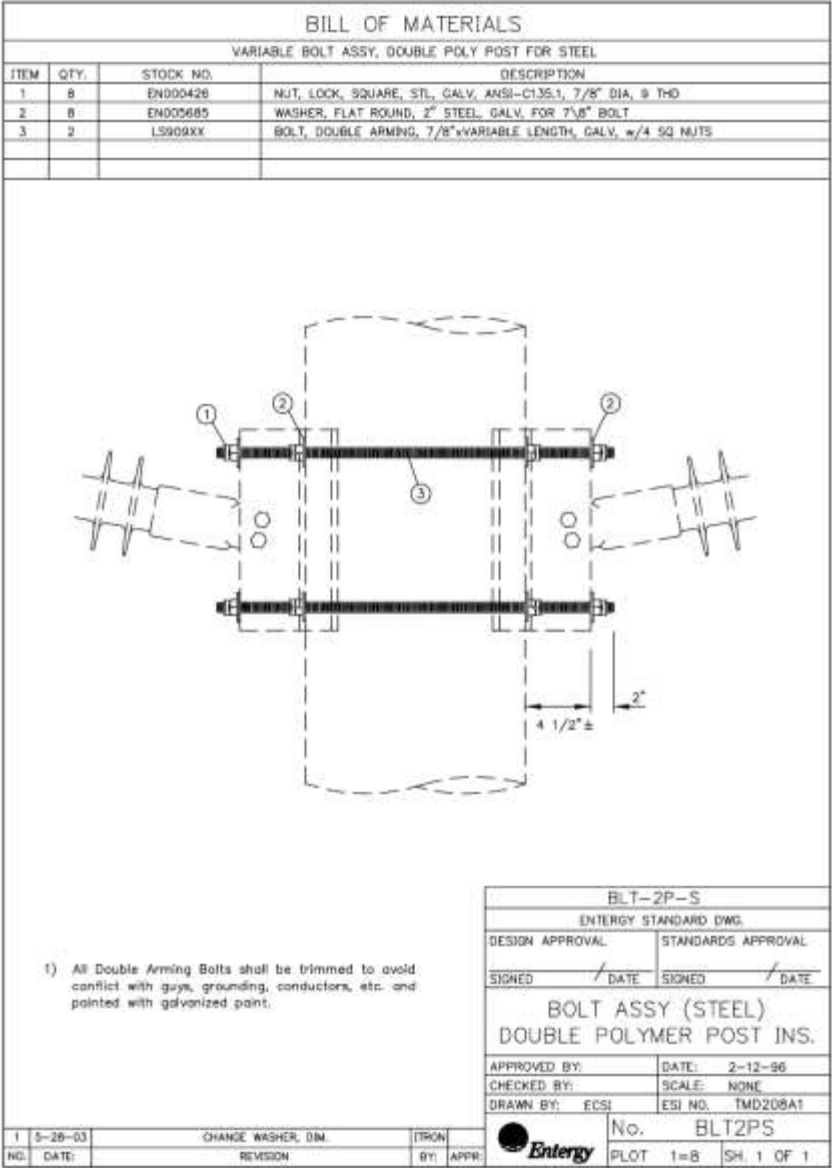
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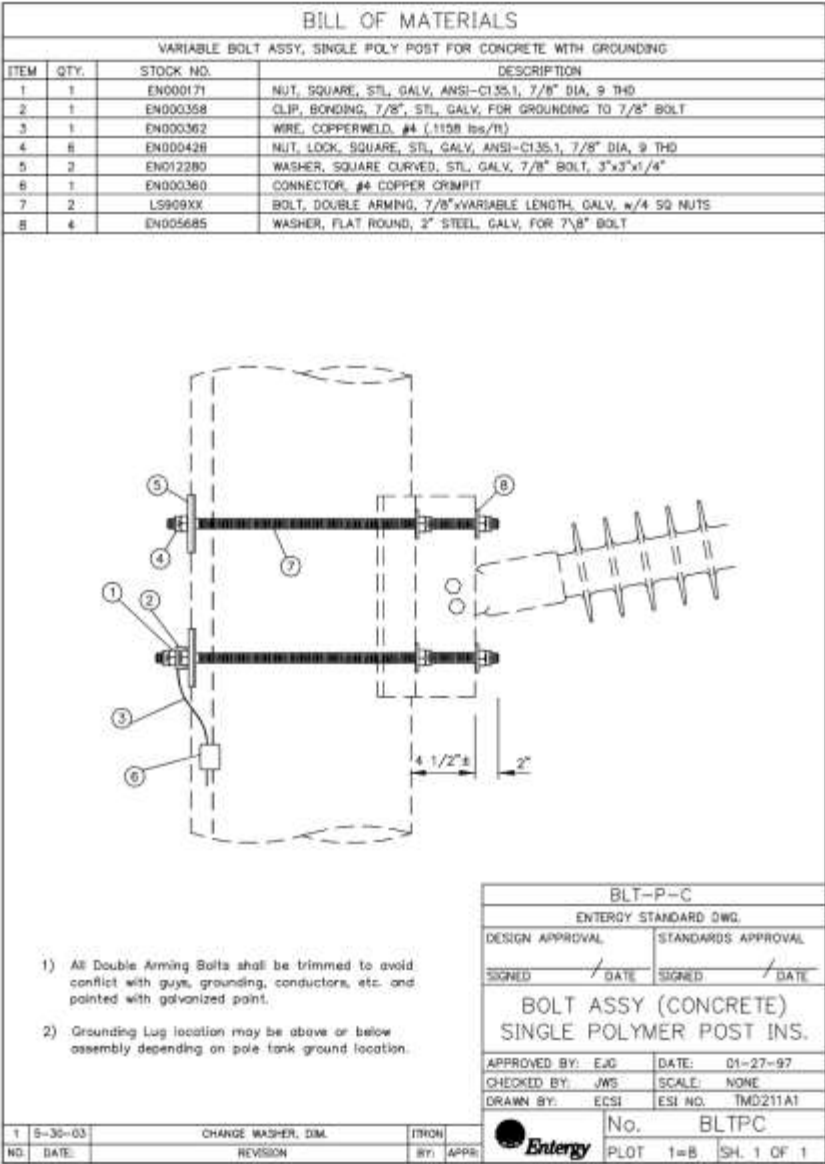
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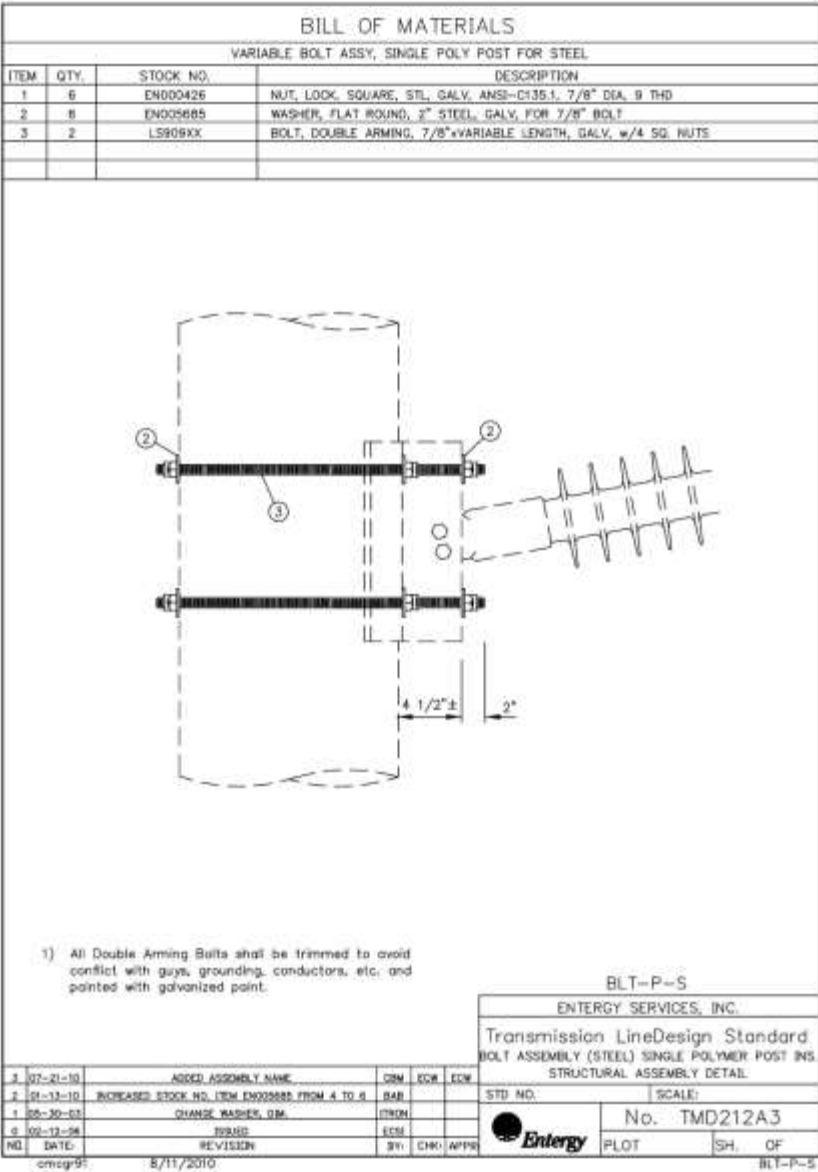
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BILL OF MATERIALS			
OHGW DEADEND			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	2	EN000492	SHACKLE, ANCHOR, 40K U/LT, 3/4" PIN DIA, 2-3/4" LONG
2	1	LS9004XX	TERMINAL CONNECTOR, 15 DEG, FOR VARIABLE SIZE WIRE
3	1	LS9005XX	DEADEND, ALUMINUM COMPRESSION BODY, SINGLE TONGUE, VARIABLE WIRE SIZE
4	-	LS5012XX	CONNECTOR, AMPACT, SEE GND ASSEMBLY DRAWING FOR MATERIAL
ALTERNATE FOR BOLTED ASSEMBLY			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	2	EN000492	SHACKLE, ANCHOR, 40K U/LT, 3/4" PIN DIA, 2-3/4" LONG
4	-	LS5012XX	CONNECTOR, AMPACT, SEE GND ASSEMBLY DRAWING FOR MATERIAL
5	1	LS913XX	DEADEND BOLTED STRAIN ALUMINUM
6	1	LS5012XX	CONNECTOR, AMPACT, VARIABLE CONDUCTOR SIZE TO VARIABLE CONDUCTOR SIZE
7	1	EN000390	LINK, CHAIN, XMSN: CONNECTING, CS, 1/2" PITCH, 2 1/4" LONG

FOR GROUNDING DETAIL AND MATERIALS SEE DWG. GND-XX.

See note 2

ALTERNATE PARTS
No. (LS913XX) deadend clamp
No. (LS5012XX) impact connector

See note 2

1) Item #2, #3 and #6 are conductor dependent.
2) For grounding detail and materials, see applicable Gnd-xx drawing.
3) For horizontal wire orientation, omit one of item 1.

OHG-DE-XX			
ENTERGY SERVICES, INC.			
Transmission LineDesign Standard			
OVERHEAD GROUNDWIRE DEADEND ASSY			
STRUCTURAL ASSEMBLY DETAIL			
STD. NO.	SCALE	NONE	
No. TMD222A6			
PLOT 1=8		SPL. 1 OF 1	
OHG-DE-XX			

REV	DATE	DESCRIPTION	BY	CHK	APPV
6	07-21-10	SHOW ITEM 4 ON ASSEMBLY	CBM	ECW	ECW
5	09-15-08	REVISED ITEM #4	PLA		
4	01-21-01	MODIFIED STOCK NUMBER LS5012XX	LS		
3	01-04-01	MODIFIED CALLOUTS	LS		
2	04-07-00	MODIFIED STOCK NUMBER LS9012XX	RMR		
1	11-16-99	ADDED AMPACT & CARTRIDGE DESCRIPTION	RMR		
0		ISSUED	ECW		
NO.	DATE	REVISION	BY	CHK	APPV
	8/15/2006				

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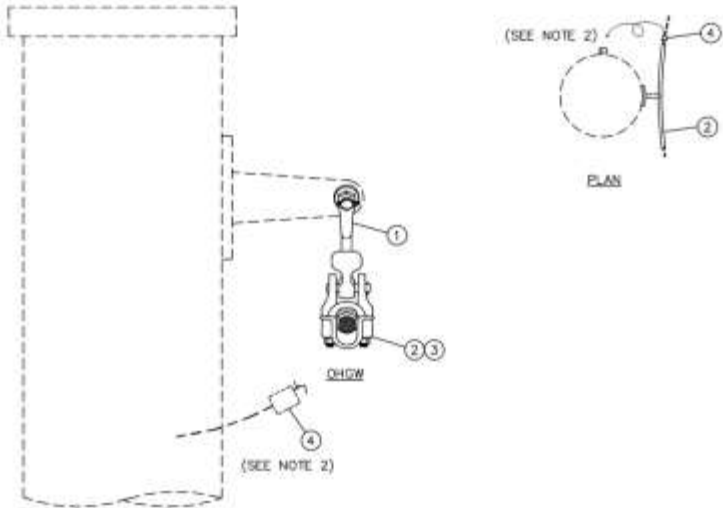
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BILL OF MATERIALS			
OHGW SUSPENSION, 0-30"			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	EN004375	BALL CLEVIS, 45 DEG Y, 30K ULT, 3/4" PIN DIA
2	1	LS9003XX	ROD, ARMOR, PREFORMED, ALUMINUM, VARIABLE CONDUCTOR SIZE
3	1	LS9008XX	CLAMP, SUSPENSION, ALUMINUM, VARIABLE WIRE SIZE, w/SOCKET EYE
4	-	LS5012XX	CONNECTOR, AMPACT



1) Item #2 and #3 are conductor dependent. These items are selected for each project and may be with or without Armor Rod.

2) For grounding detail and materials see applicable GND-XX drawing.

OHG-SUS-XX			
ENTERGY STANDARD OHG.			
DESIGN APPROVAL		STANDARDS APPROVAL	
SIGNED	/ DATE	SIGNED	/ DATE
OVERHEAD GROUNDWIRE SUSPENSION ASSY			
APPROVED BY:		DATE: 2-15-03	
CHECKED BY:		SCALE: NONE	
DRAWN BY: ITRON		ESI NO. TMD22.3A9	
No. OHGSUS			
PLOT 1=8		SH. 1 OF 1	

NO.	DATE	REVISION	BY	APPR.
9	8-15-06	REMOVED OPTOH OPTION, DELETED ITEM #4	RJA	
8	12-8-03	ADDED BACK GROUNDING DETAILS	ITRON	
7	5-30-03	ADDED OPTOH OPTION	ITRON	
6	2-17-03	ADDED POLE CAP AND GROUNDING NOTE 2	ITRON	
5	10-15-02	REMOVE GROUNDING DETAIL	ITRON	
4	1-18-02	MODIFIED ITEMS 1, 2 AND 3.	LSFT	
3	1-29-01	MODIFIED STOCK NUMBER LS9007XX	LSFT	
2	1-29-01	MODIFIED STOCK NUMBER LS5012XX	RMB	

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BILL OF MATERIALS			
OHGW SUSPENSION, 30-50" WITH YOKE PLATE			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	2	EN000482	SHACKLE, ANCHOR, 40K ULT, 3/4" PIN DIA, 2-3/4" LONG
2	2	EN004375	BALL, CLEVIS, 45 DEG Y, 30K ULT, 3/4" PIN DIA
3	1	EN015676	PLATE, YOKE, DUCTILE IRON, 18" WIDTH, 30K ULT, 3/4" GALV
4	1	LS9003XX	ROD, ARMOR, PREFORMED, ALUMINUM, VARIABLE CONDUCTOR SIZE
5	2	LS9007XX	CLAMP, SUSPENSION, ALUMINUM, VARIABLE SIZE WIRE, W/SOCKET EYE
6	-	LS5012XX	CONNECTOR, AMPACT, SEE GROUND ASSEMBLY DRAWING FOR MATERIAL

1) ITEM #4 AND #5 ARE CONDUCTOR DEPENDENT. THESE ITEMS ARE SELECTED FOR EACH PROJECT AND MAY BE WITH OR WITHOUT ARMOR ROD.

2) FOR GROUNDING DETAIL AND MATERIALS SEE APPLICABLE GND-XX DRAWING.

NO.	DATE	REVISION	BY	APPR.
8	8-15-08	REVISED ITEM #6	RL	
5	12-8-03	ADDED BACK GROUNDING DETAILS	ITRON	
4	2-18-03	ADDED POLE CAP AND GROUNDING NOTE	ITRON	
3	1-29-01	MODIFIED STOCK NUMBER LS9007XX	LS	
2	8-7-00	MODIFIED STOCK NUMBER LS5012XX	RMB	
1	11-16-99	ADDED AMPACT & CARTRIDGE DESCRIPTION	RMB	

OHG-SUY-XX	
ENTERGY STANDARD OHG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
OVERHEAD GROUNDWIRE HEAVY ANGLE ASSY	
APPROVED BY:	DATE: 1-29-01
CHECKED BY:	SCALE: NONE
DRAWN BY: ECSE	ESI NO. TMD224A6
No. OHGSUY	
ENTERGY	PLOT: 1=16 SH. 1 OF 1

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BILL OF MATERIALS			
TEE ASSY, BRACE POST FOR STEEL WITH BOLTS			
ITEM	QTY	STOCK NO.	DESCRIPTION
1	1	EN000171	NUT, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
2	4	EN000425	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
3	2	EN003796	WASHER, SQUARE CURVED, STL, GALV, ANSI-C135.1, 7/8" BOLT, 1/4" THK, 4"x4"
4	1	EN011909	PLATE, POLE EYE, GALV STL, DBL EYE, 70K ULT, 8" BOLT SPACING
5	2	LS909XX	BOLT, DOUBLE ARMING, 7/8"xVARIABLE LENGTH, GALV, w/4 SQ NUTS

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

2) Grounding Lug location may be above or below assembly depending on pole tank ground location.

TEE-B-S	
ENTERGY STANDARD DWG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
TEE ASSY (STEEL) BRACE	
APPROVED BY: EJC	DATE: 12-19-00
CHECKED BY: JWS	SCALE: NONE
DRAWN BY: ECS	ESI NO. TMD279AD
No. TBS	
PLOT 1=8 SH. 1 OF 1	

NO.	DATE	REVISION	BY	APPR
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PROPRIETARY, CONFIDENTIAL, OR PRIVILEGED INFORMATION

Attachment 1: Applicable Standard Framing and Assembly Drawings

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BILL OF MATERIALS			
TEE ASSY, BRACE TO BRACE FOR STEEL WITH BOLTS			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	EN000171	NUT, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
2	4	EN000426	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
3	2	EN011909	PLATE, POLE EYE, GALV STL, DBL EYE, 70K ULT, 8" BOLT SPACING
4	2	LSR09KX	BOLT, DBL ARMING, 7/8"xVARIABLE LENGTH, GALV, w/4 SQ NUTS

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

2) Grounding Lug location may be above or below assembly depending on pole tank ground location.

TEE-B-B-S	
ENTERGY STANDARD DWG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
TEE ASSY (STEEL) BRACE - BRACE	
APPROVED BY: EJD	DATE: 12-19-00
CHECKED BY: JWS	SCALE: NONE
DRAWN BY: ECSI	ESI NO. TMD28040
No. TBBS	
PLOT 1=8 SH. 1 OF 1	

NO. DATE: REVISION BY: APPR.

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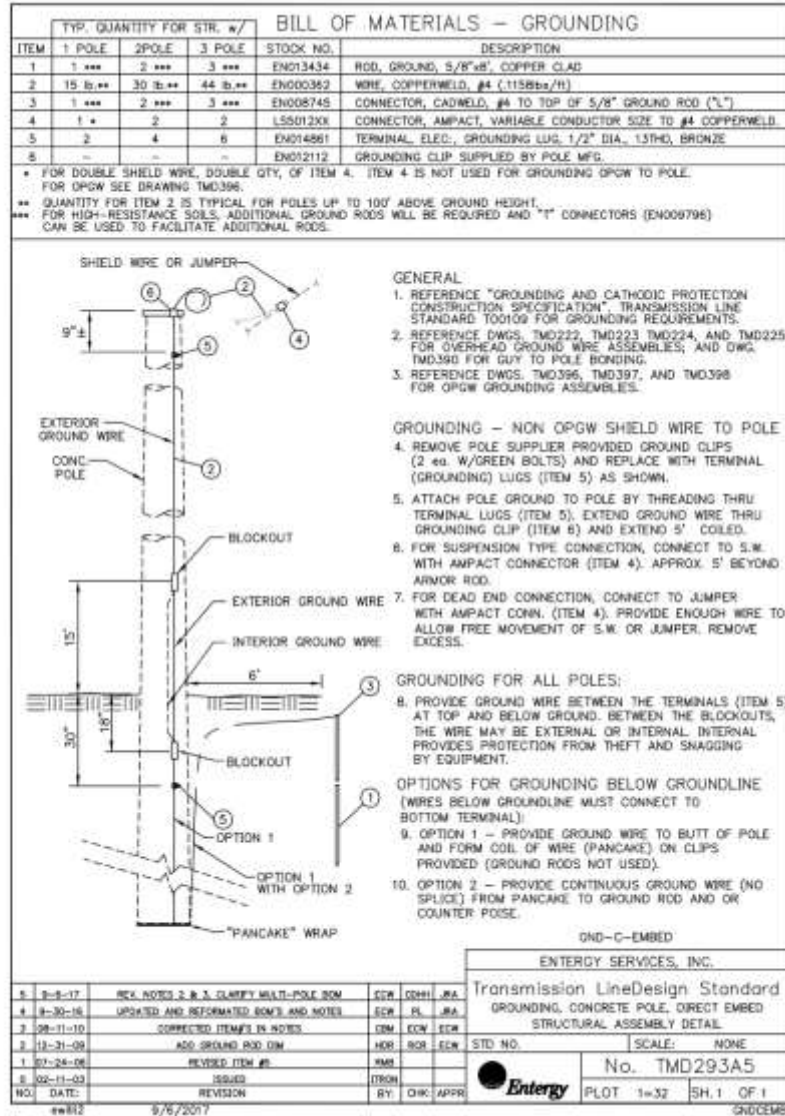
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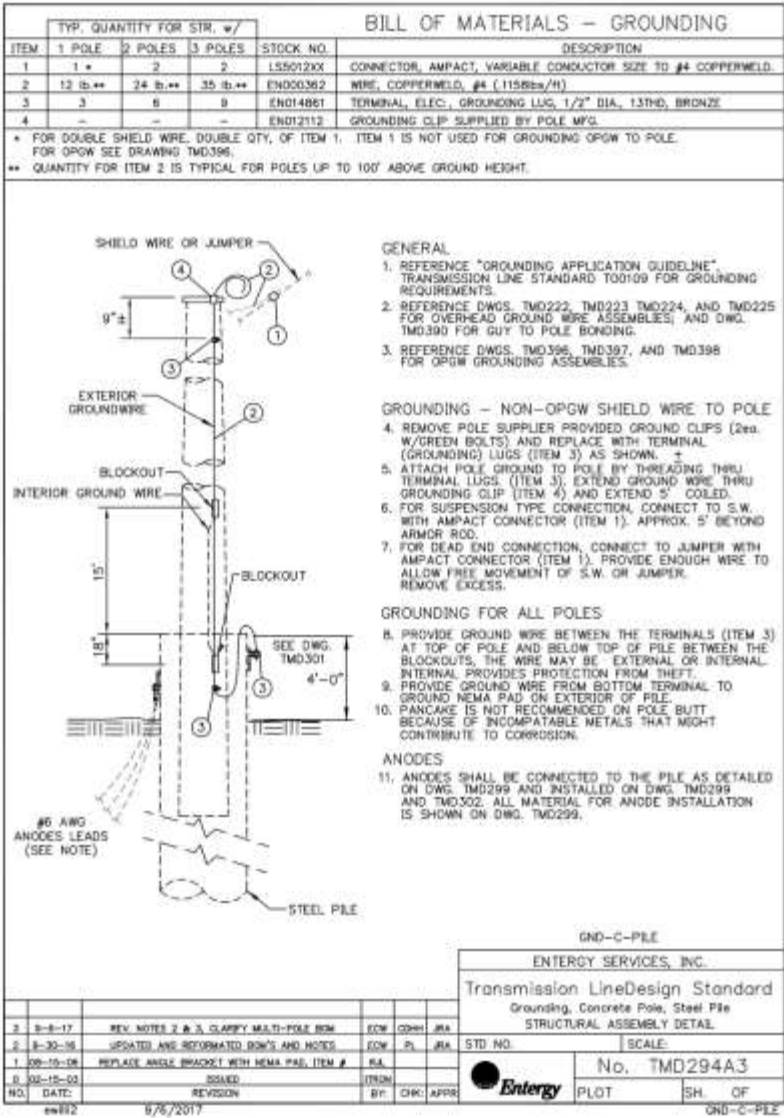
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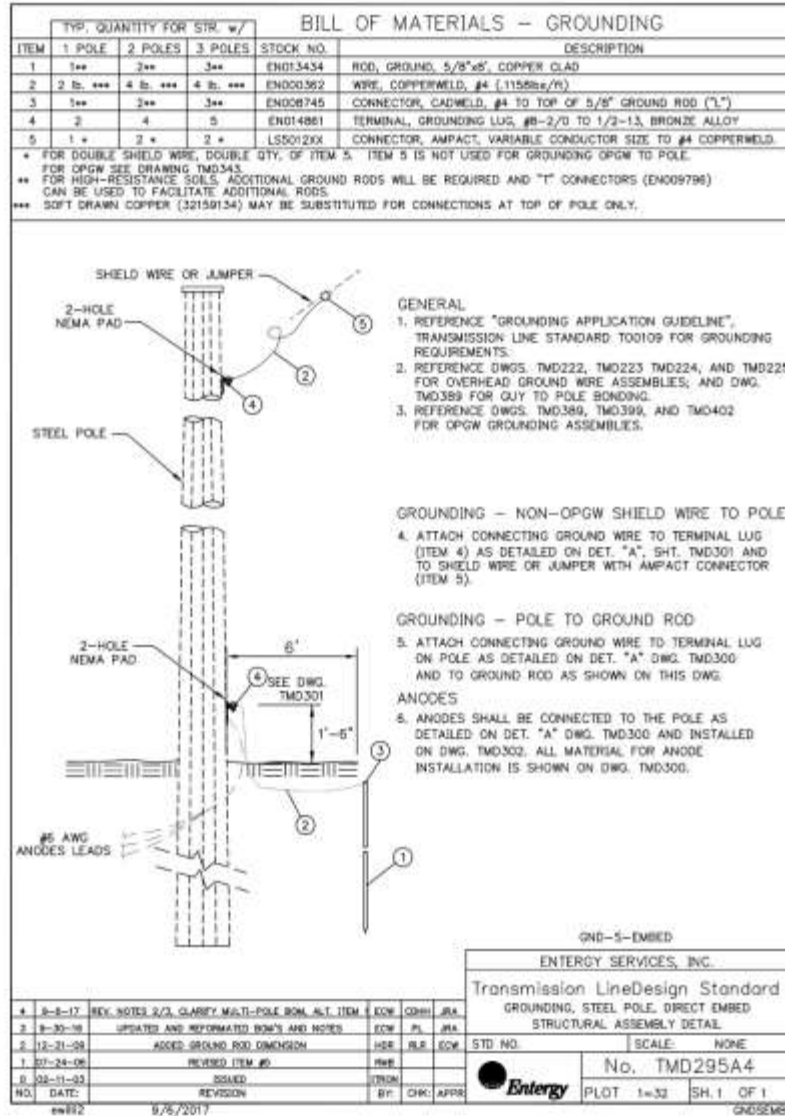
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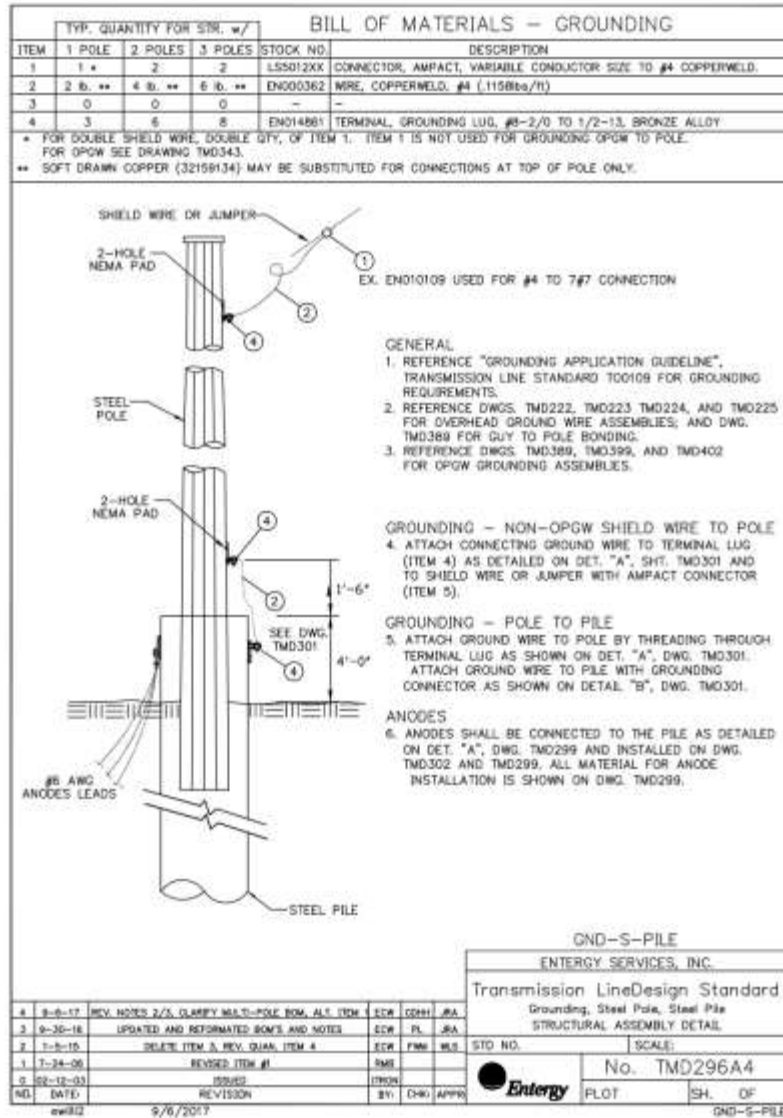
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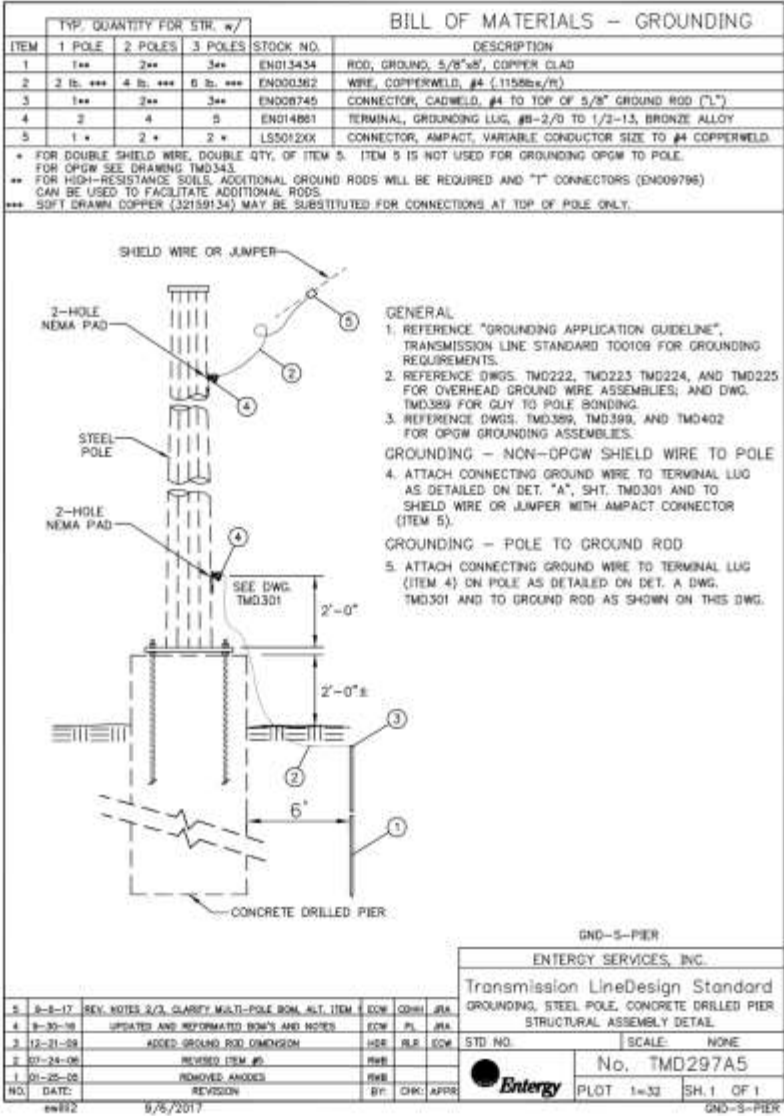
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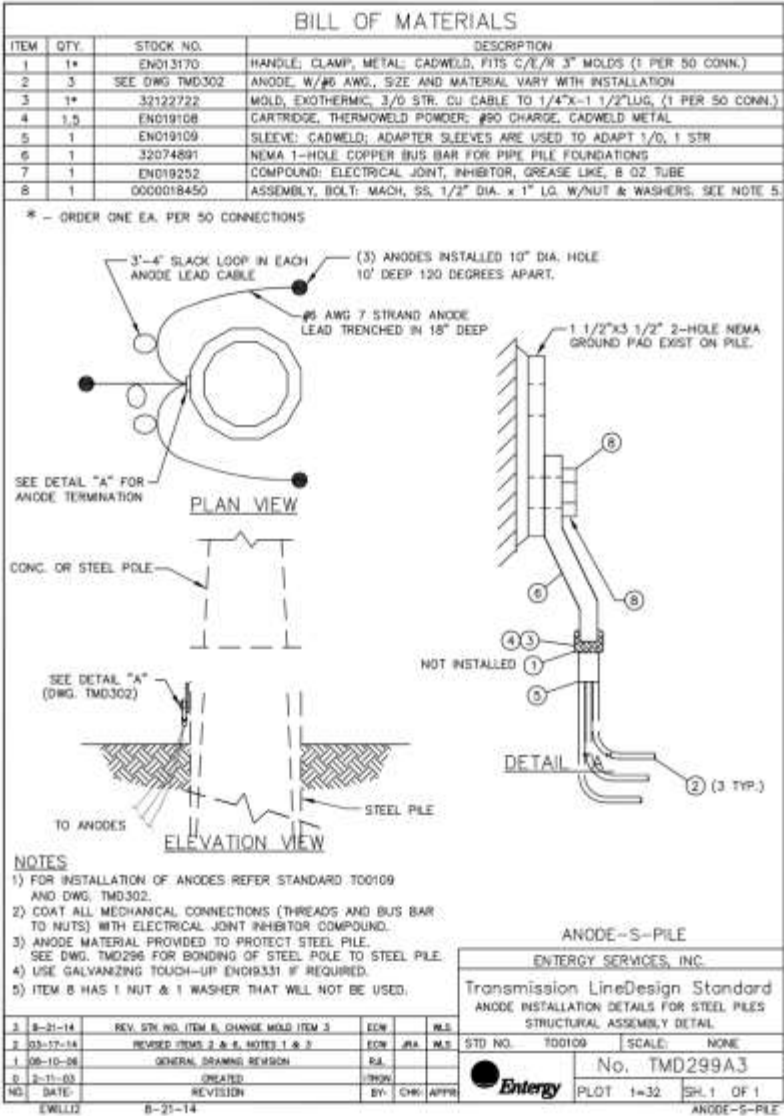
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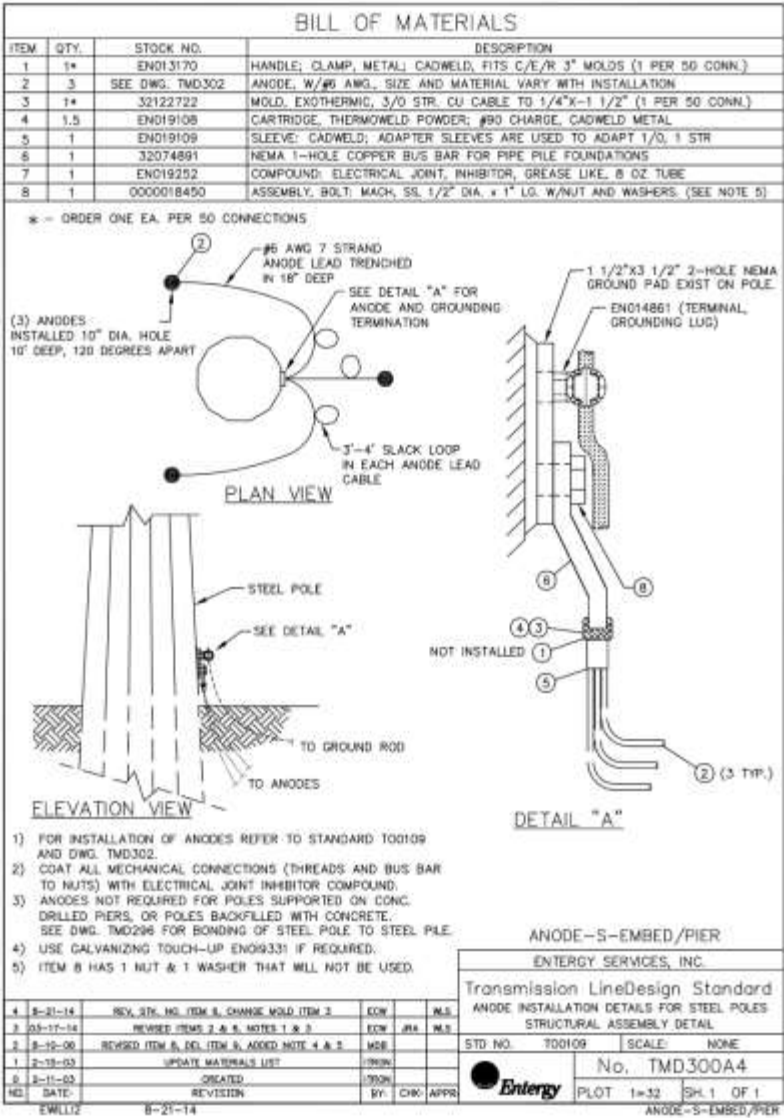
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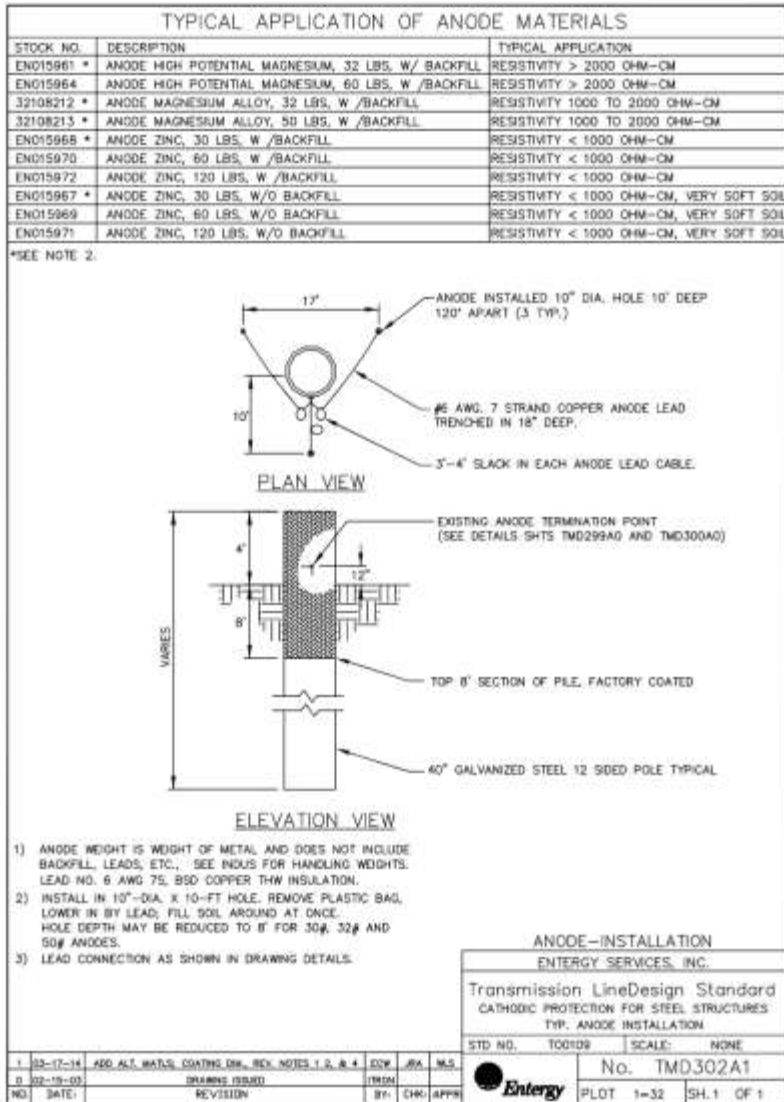
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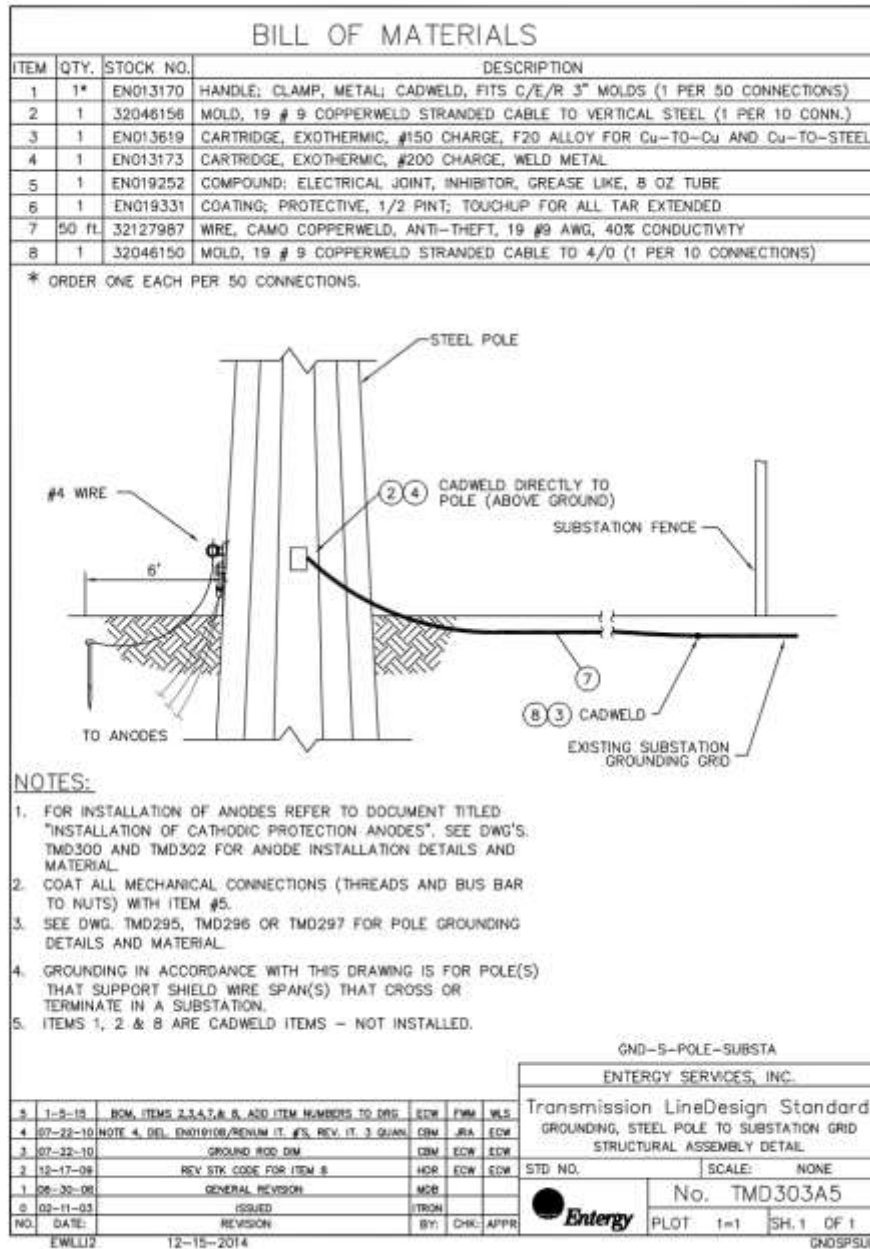
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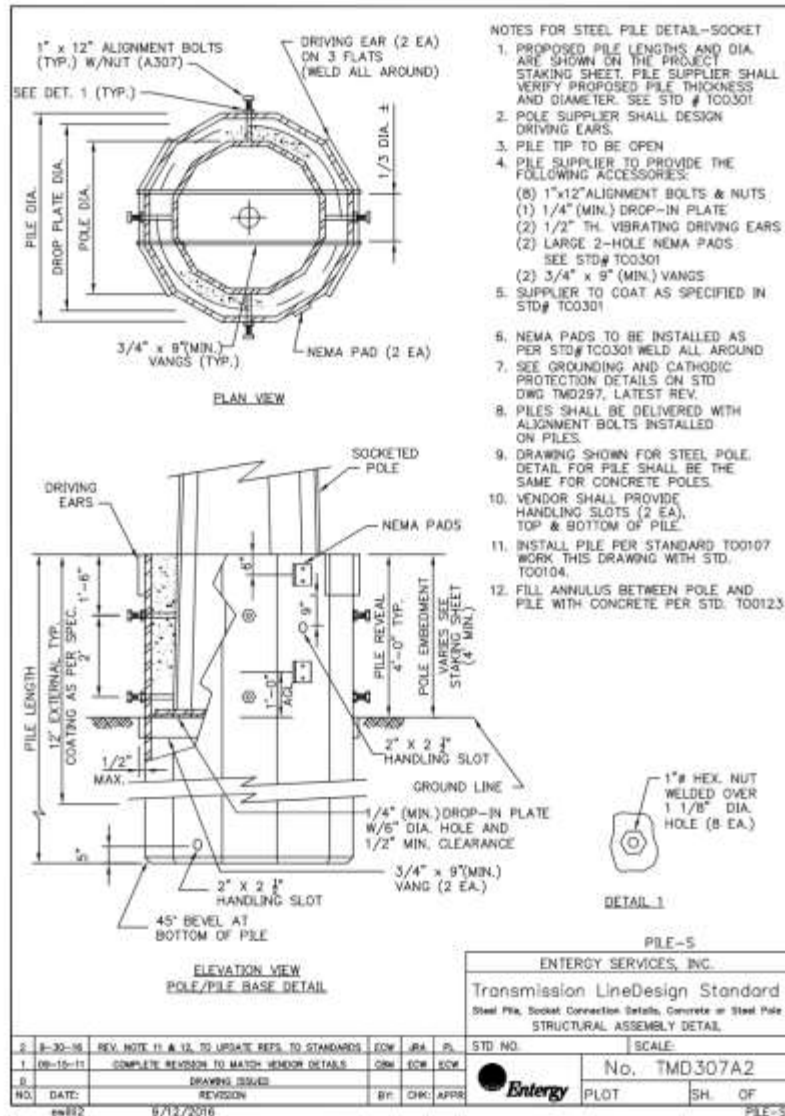
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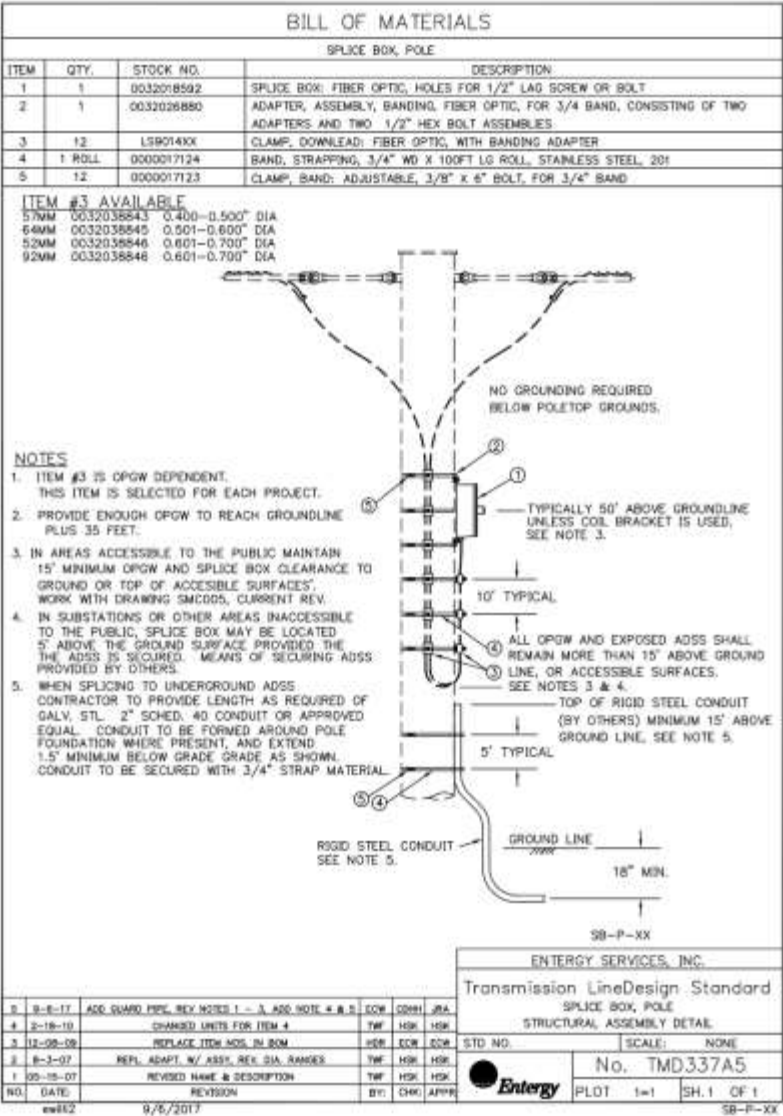
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BILL OF MATERIALS			
OVERHEAD GROUND WIRE, DEADEND, OPGW, POLE			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	LS9011XX	DEADEND-BOLTED STRAIN,OPGW,3/4" PIN DIA.
2	1	0000012506	LINK, CHAIN: 5/8" X 3-1/4", 40K
3	1	0000024787	CLEVIS, CLEVIS: Y-Y, 30K, 3/4" PD, 15" LONG

NOTE: ILLUSTRATED AS TANGENT OR SMALL ANGLE STRUCTURE. LARGER ANGLES WILL HAVE THE PULLOFFS AT DIFFERENT ELEVATIONS BY SEVERAL INCHES.

NOTE: FOR NON-SPLICE BOX LOCATIONS, MAINTAIN CONTINUOUS LOOP AND DO NOT CUT OPGW.

NOTE: FOR SPLICE BOX LOCATIONS, PROVIDE ENOUGH WIRE TO REACH THE GROUNDLINE, PLUS 15 FEET.

ITEM #1 AVAILABLE:

SIZE	STOCK NO.	DIA.
57MM	0000018531	0.465" DIA
64MM	0032018594	0.528" DIA
52MM	0032018595	0.646" DIA
92MM	0032018596	0.671" DIA

1) ITEM #1 IS OPGW DEPENDENT. THIS ITEM IS SELECTED FOR EACH PROJECT.

OHG-DE-OP-P-XX

ENTERGY SERVICES, INC.

Transmission LineDesign Standard

OVERHEAD GROUNDWIRE, DE, OPGW, POLE

STRUCTURAL ASSEMBLY DETAIL

REV	DATE	REVISION	BY	CHK	APP
2	9-15-07	REVISED NOTES, NAME & DESCRIPTION	TWP	HSK	HSK
1	8-23-06	UPDATED BILL OF MATERIAL	R/L	HSK	HSK
0	X	CREATED		HSK	HSK

11/11/2007 6/25/2007

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STD NO. No. TMD339A2

SCALE: NONE

PLOT 1=1 SH. 1 OF 1

OHG-DE-OP-P-XX

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PROPRIETARY, CONFIDENTIAL, OR PRIVILEGED INFORMATION

Attachment 1: Applicable Standard Framing and Assembly Drawings

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BILL OF MATERIALS			
OVERHEAD GROUND WIRE, SUSP. 30-50' W/YOKE, OPGW			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	LS9010XX	CLAMP, SUSP. DOUBLE (2 CLAMPS), ALUM AL 15K, W/48" ARM RODS, 30'-60' MAX. ANGLE
2	2	0032020410	CLEVIS EYE: STRAIGHT, 30K, 2-7/8" LG, 1-5/8" EYE WD, 3/4" EYE RAD, 5/8" PIN DIA
3	1	0032020414	PLATE, YOKE-DELTA, DUCTILE IRON, 18" LONG, 30K
4	1	0000004375	BALL CLEVIS: 45 DEG Y, 30K, 3/4" PD, CLASS 52-3/5
5	1	0000000486	SOCKET CLEVIS: STRAIGHT, 30K, 5/8" PD, CLASS 52-3/5

AS ON LATTICE TOWER

AS ON POLE

ARMOR RODS COME WITH CLAMPS

ITEM #1 AVAILABLE

ITEM #1 AVAILABLE	ITEM #1 AVAILABLE	ITEM #1 AVAILABLE
57MM	0032018593	0.450-0.475" DIA
64MM	0000017195	0.528-0.555" DIA
52MM	0000017196	0.615-0.646" DIA
92MM	0000017198	0.647-0.679" DIA

1) ITEM #1 OPGW DEPENDENT.
THIS ITEM IS SELECTED FOR EACH PROJECT.

OHG-SUY-OP-XX			
ENTERGY SERVICES, INC.			
Transmission LineDesign Standard			
OVERHEAD GROUNDWIRE, SUSP 30-50 W/YOKE, OPGW			
STRUCTURAL ASSEMBLY DETAIL			
REV	DATE	DESCRIPTION	BY
2	5-15-07	REVISED NAME & DESCRIPTION COMBINED DWGS TMD340 & TMD341	TWF HSK HSK
1	8-01-08	EXPANDED DESCRIPTIONS OF ITEMS 1 & 2	CDR HSK HSK
0	5-24-04	CREATED	HSK HSK
NO.	DATE	REVISION	BY: CHK: APPR:

116c90 6/25/2007

OHG-SUY-OP-XX

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PLT 1=1 SH. 1 OF 1

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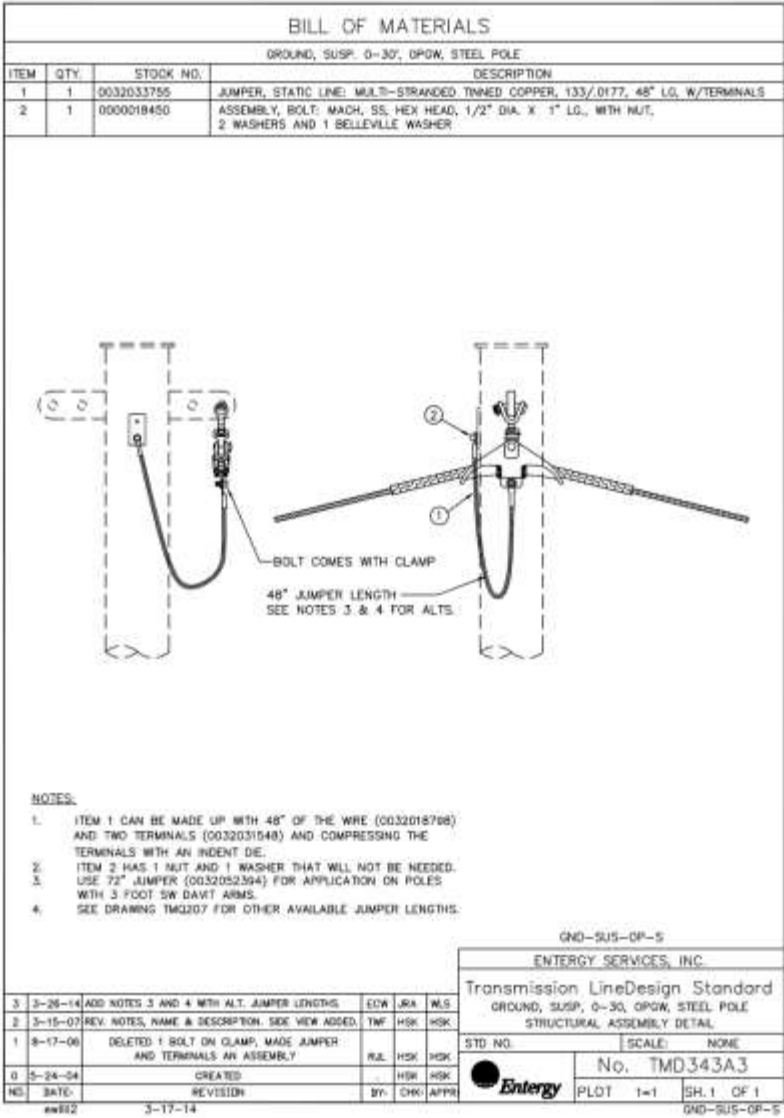
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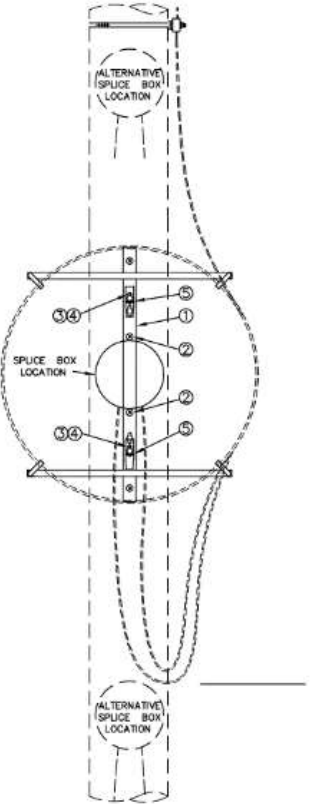
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BILL OF MATERIALS					
COIL BRACKET, OPGW, STEEL POLE					
ITEM	QTY.	STOCK NO.	DESCRIPTION		
1	1	0032031230	BRACKET, COIL: 60 INCH, GALV. STEEL, PER ENTERGY DWG TMM060A		
2	2	—	BOLT, MACHINE, 1/2"-13 X 1", ALL THREAD, GALV. STEEL, NO NUT, NO WASHER (ANY SUPPLIER)		
3	0	000000139	BOLT ASSEMBLY, MACHINE: HEX HEAD, GALV. STEEL, 5/8"-11 X 1-1/2", WITH HEX NUT		
4	0	000000532	WASHER, ROUND, FLAT, 11/16" ID, 1-1/2" OD, 1/8" THICK, ASTM A153, GALV. STEEL		
5	0	0032031232	PLATE, BENT, GALV. STEEL, PER ENTERGY DWG. TMM061A		



NOTE #1: ASSEMBLY WILL TYPICALLY BE Banded TO POLE USING 3/4" SS BAND MATERIAL AND ADAPTERS SUPPLIED WITH THE SPLICE BOX. ALTERNATELY, THE COIL BRACKET ASSEMBLY MAY BE SECURED WITH TWO 1/2" BOLTS (ITEM 2) USING ANY TWO OF THE FOUR THREADED RECEIVER PROVIDED.

NOTE #2: TWO EACH OF ITEMS 3 AND 5, AND FOUR OF ITEM 4 MAY ALSO BE USED TO SECURE THE COIL BRACKET ASSEMBLY TO POLES ALREADY IN SERVICE THAT WERE MANUFACTURED WITH STEP CLIPS. THE STEP CLIP DETAIL IS COMMON ON OLDER POLES MANUFACTURED BY THOMAS & BETTS.

NOTE #3: COIL BRACKET ASSEMBLY CAN BE INSTALLED WITH EITHER END UP. BEFORE TIGHTENING BOLTS, BE SURE THAT WEIGHT OF COMPONENTS PULLS THEM FIRMLY INTO SLOTTED HOLES IN THE CHANNEL.

NOTE #4: THE LOWEST PART OF THE INSTALLATION MUST BE A MINIMUM OF 15 FEET ABOVE GROUNDLINE AND THE CABLE MUST COME INTO THE BOTTOM OF THE SPLICE BOX WITH NO STRAIN ON THE CONNECTORS. ADDITIONAL BANDING MAY BE NECESSARY TO GATHER AND STABILIZE THE EXCESS CABLE LENGTH TO THE BRACKET AND POLE. HOLES ARE PROVIDED IN THE END OF EACH ARM TO ACCOMMODATE CABLE TIES OR WIRE TIES.

15' MINIMUM ABOVE GL. IF ALTERNATE SPLICE BOX LOCATION IS USED, NO PART OF INSTALLATION CAN BE LOWER THAN 15' ABOVE THE GROUND LINE.

CB-OP-S

ENTERGY SERVICES, INC.					
Transmission LineDesign Standard					
COIL BRACKET, OPGW, STEEL POLE					
STRUCTURAL ASSEMBLY DETAIL					
3	9-24-15	ADD REF. LINE FOR 15' MIN. DIMENSION	ECW		ECW
2	8-21-14	QTY. ITEMS 3-5, REV. NOTES 1 & 2	ECW		WLS
1	5-15-07	REVISED NAME & DESCRIPTION	TWF	HSK	HSK
0	3-30-06	CREATED	RMB	HSK	HSK
NO.	DATE	REVISION	BY	CHK	APPR

EWILLJ2 08-24-15

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No. TMD386A3

PLOT 1=1 SH.1 OF 1

CB-OP-S

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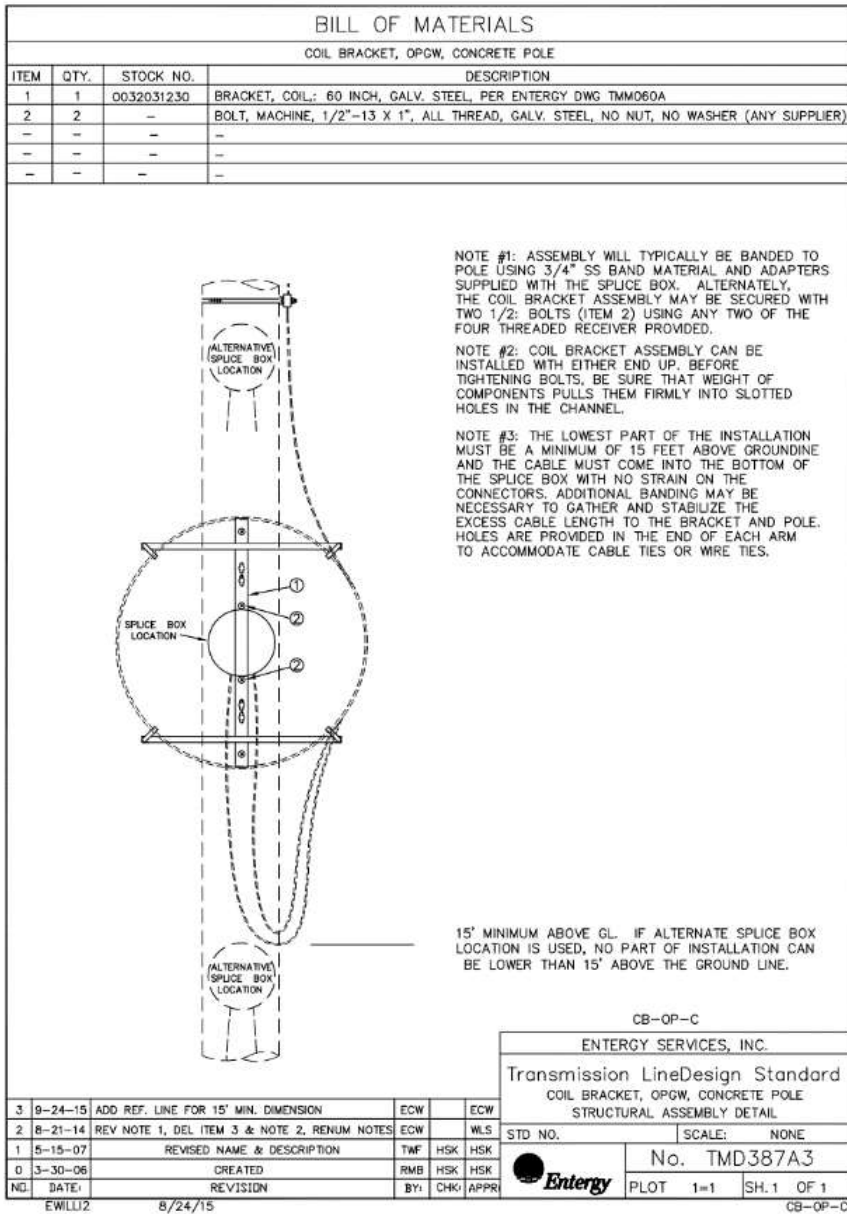
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Attachment 1: Applicable Standard Framing and Assembly Drawings

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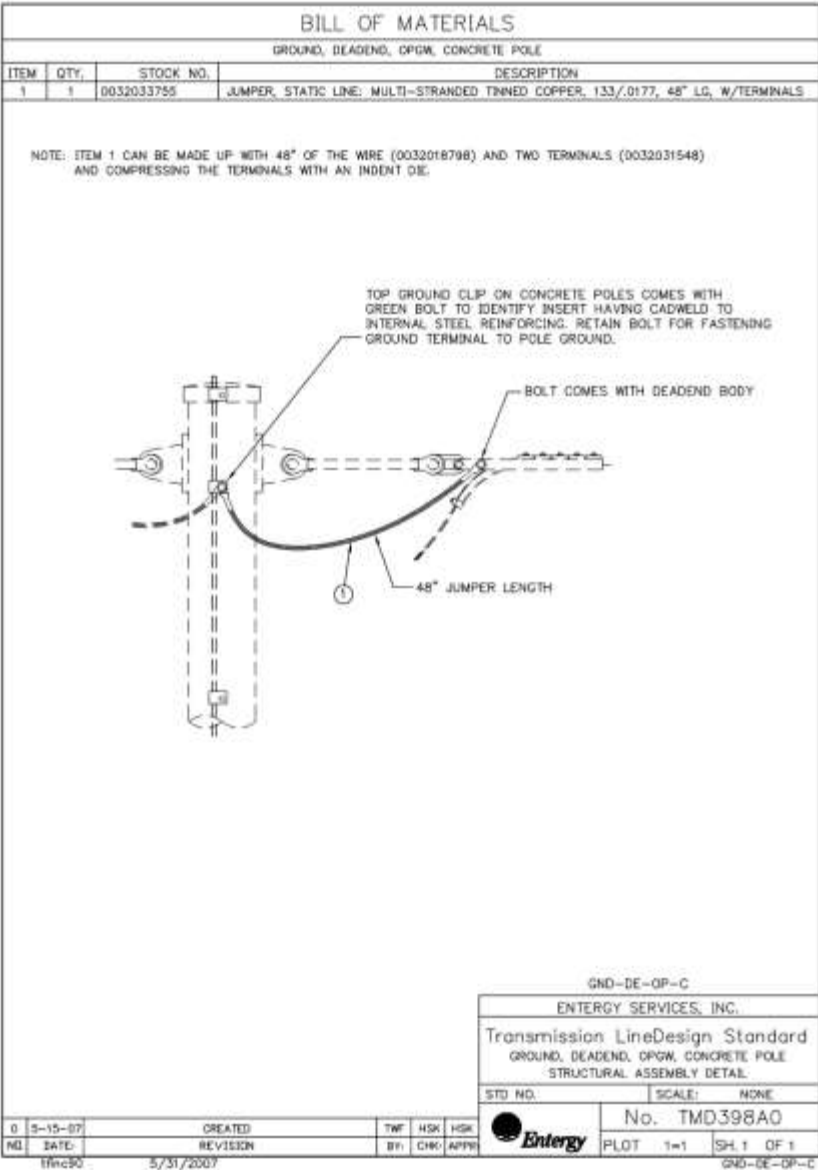
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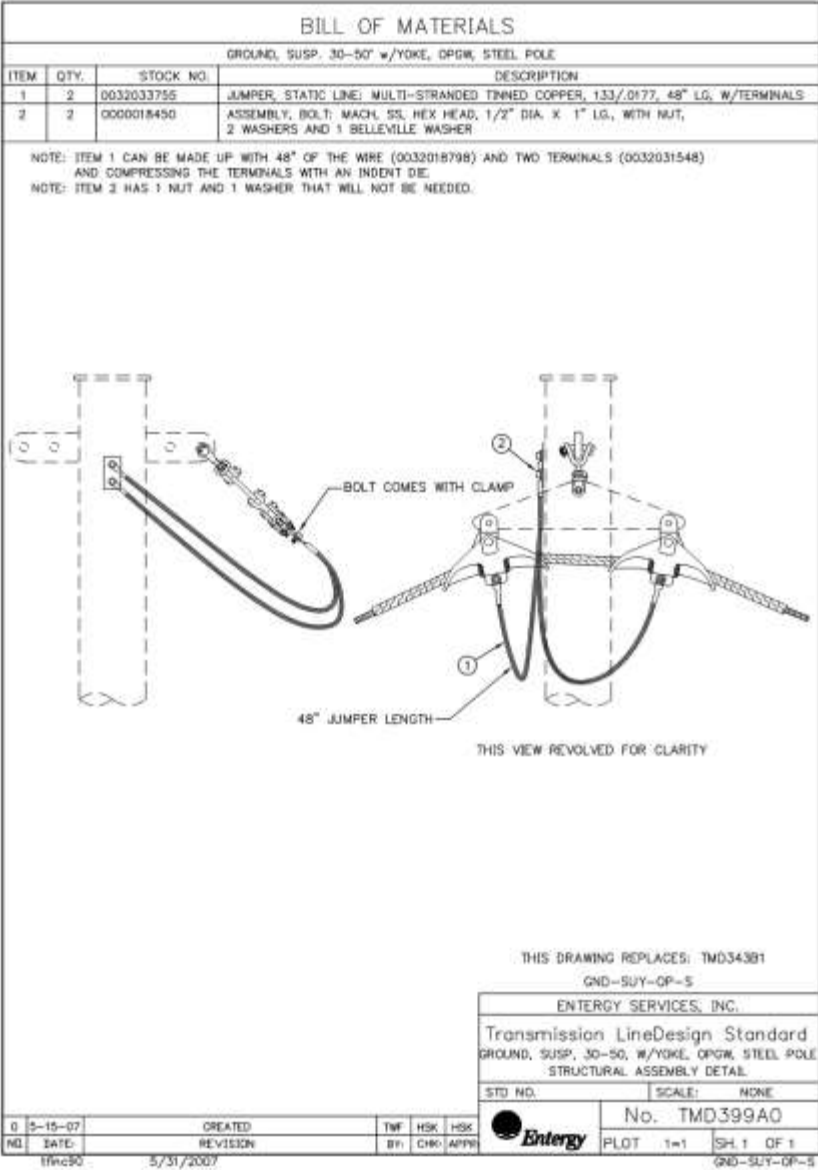
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BILL OF MATERIALS			
GROUND, DEADEND, OPGW, STEEL POLE			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	0032033755	JUMPER, STATIC LINE; MULTI-STRANDED TINNED COPPER, 133/.0177, 48" LG, W/TERMINALS
2	1	0000018450	ASSEMBLY, BOLT; MACH. SS, HEX HEAD, 1/2" DIA. X 1" LG., WITH NUT, 2 WASHERS AND 1 BELLEVILLE WASHER

NOTE: ITEM 1 CAN BE MADE UP WITH 48" OF THE WIRE (0032018798) AND TWO TERMINALS (0032031548) AND COMPRESSING THE TERMINALS WITH AN INDENT DIE.
NOTE: ITEM 2 HAS 1 NUT AND 1 WASHER THAT WILL NOT BE NEEDED.

THIS DRAWING REPLACES: TMD343C1
GND-DE-OP-S

ENTERGY SERVICES, INC.			
Transmission LineDesign Standard			
GROUND, DEADEND, OPGW, STEEL POLE			
STRUCTURAL ASSEMBLY DETAIL			
STD. NO.	SCALE:	NONE	
No. TMD402A0			
0	5-15-07	CREATED	FWF HSK HSK
01	5-31-2007	REVISION	BF1 CHG APPR

ENTERGY

PLOT 1=1 SH. 1 OF 1
GND-DE-OP-S

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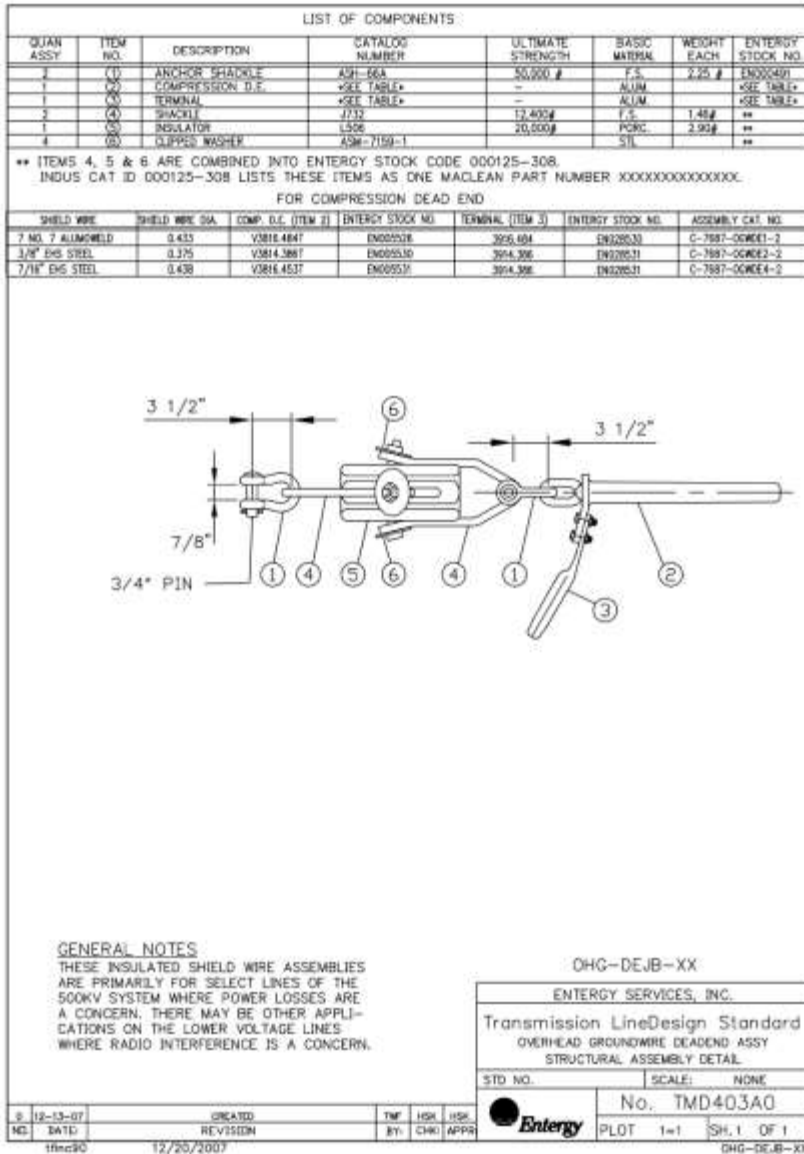
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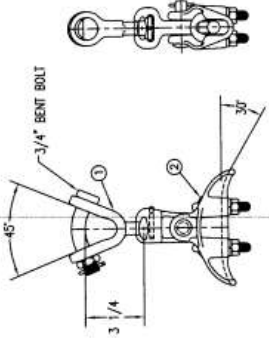
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REVISIONS				EXTENT APPROVAL			
NO.	DATE	DESCRIPTION	BY	CHKD	BY	CHKD	
1	12/22/01	REV. REVISIONS					
2	12/22/01	REV. REVISIONS					
3	12/22/01	REV. REVISIONS					
4	12/22/01	REV. REVISIONS					
5	12/22/01	REV. REVISIONS					
6	12/22/01	REV. REVISIONS					
7	12/22/01	REV. REVISIONS					
8	12/22/01	REV. REVISIONS					
9	12/22/01	REV. REVISIONS					

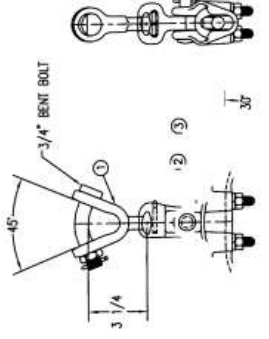
LIST OF COMPONENTS						
QTY/ASST	ITEM	DESCRIPTION	CATALOG NUMBER	BASIC MATERIAL	WEIGHT EACH	ENERGY STOCK NO.
1	1	CLAMP	YOS-65A	F.S.	2.15	EN004375
1	2	SUSPENSION CLAMP	SEE TABLE*	F.S.	2.15	EN004375
1	3	POWER ROD	JAWAT-1050	ALUM.		EN003360

* LS-1 MATERIAL IS AL. & ULT. STR. 18,000 LBS. WT. 4.11 LBS.
FSC-60 MATERIAL IS D.I. & ULT. STR. 17,000 LBS. WT. 4.00 LBS.

SHIELD WIRE	SHIELD WIRE DIA.	CLAMP (ITEM 2)	ENERGY STOCK NO.	ASSEMBLY CAL. NO.
7 NO. 7 ALUMINUM	0.433	FSC-60-S	EN003927	C-7687-00631
3/8 DWS	0.375	FSC-60-S	EN003277	C-7687-00631A



ASSEMBLY C-7687-00631



ASSEMBLY C-7687-00631A

REF. DWG. NO. BC7687-0 FOR MATERIAL NOTES
ALL DIMENSIONS IN INCHES

DESIGN APPROVAL		STANDARD APPROVAL		BETHEA POWER PRODUCTS	
SIGNED	DATE	SIGNED	DATE	DESIGNED	DATE
ESI NO. TMD22344		ENTERGY NO. OHGSUS		BC-687	

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• **FOR CAPITAL CONSTRUCTION PROJECTS**



ON-ROAD LANE - 3000 LBS. AND ROUTE TEST LANE - 10000 LBS.
ALL NEW BUNKER 250 PITCHER SET TO BE SENT (LAW 10-1)
COURT OF THE NEW JERSEY SUPREMACY COURT IN NEWARK, N.J.
ALL NEW BUNKER 250 PITCHER SET TO BE SENT (LAW 10-1)
ALL NEW BUNKER 250 PITCHER SET TO BE SENT (LAW 10-1)

[illegible][illegible]

SCHEIDT, LINDA ANN, 3600 LANE, AND RICHARD SCOT LANE - 3600 LANE, FALLS CHURCH, VIRGINIA 22044, ARE THE FIRST COUPLE TO BE ARRESTED FOR THE SAME REASON SINCE 1971.



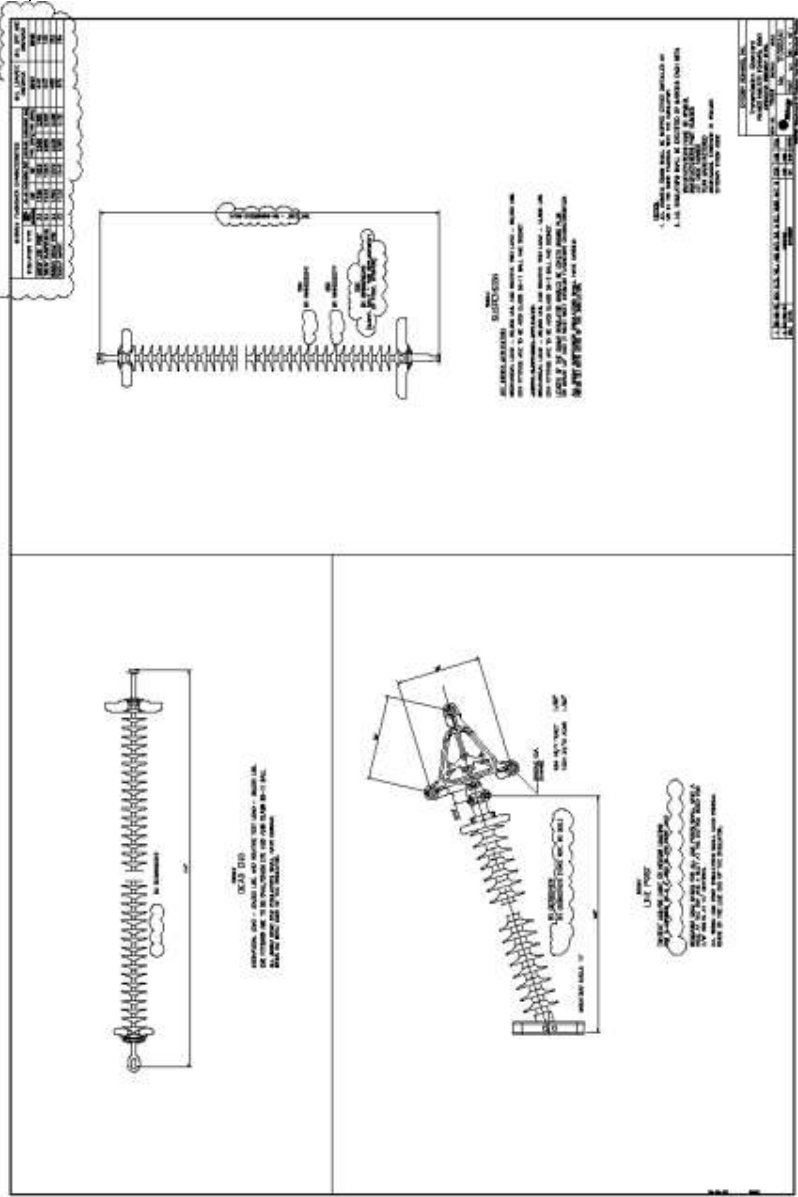
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BILL OF MATERIALS				
DEADEND, POLYMER, WITH BUNDLING YOKE, 500KV				
ITEM	COMP. QTY.	BOLTED QTY.	STOCK NO.	DESCRIPTION
1	2	2	0032009672	SHACKLE, CHAIN, 150k ULT. STR.
2	1	1	0032009669	YOKE PLATE, TRIPLE BUNDLE, DEADEND, 18" SEPARATION, 110k ULT. STR.
3	14	11	0000000689	SHACKLE, ANCHOR, 60k ULT. STR.
4	1	1	0032009670	YOKE PLATE, TRIPLE BUNDLED, DEADEND, 18" SEPARATION, 110k ULT. STR.
5	1	1	0032009665	LINK EXTENSION, EYE-EYE, 40k ULT. STR.
6	3	3	0032009668	PLATE, ADJUSTMENT, 40k ULT. STR.
7	3	3	0032000342	INSULATOR, LINE, EYE-BALL, POLYMER, 500KV, 50k ULT. STR.
8	3		LS9012XX	DEADEND, COMPRESSION, ALUMINUM, SINGLE TONGUE, 33k, FOR VARIABLE
9	3	3	0000028529	SOCKET, Y-CLEVIS, 50k
10	1	1	0032000136	LINK, CHAIN, 132k ULT., 7" LONG
11		3	0032021867	CLEVIS BALL, 35k, BALL CLASS 52-3/5
12		3	LS9013XX	DEADEND, BOLTED, STRAIN, ALUM., 30k, FOR VARIABLE WIRE SIZE
13	1	1	0032009685	CORONA RING, 500KV DEADEND, ALUM.
14	3		LS9014XX	TERMINAL CONNECTOR, 15 DEG., FOR VARIABLE WIRE SIZE
15*	3		LS5029XX	JUMPER, SPLICE, FOR VARIABLE WIRE SIZE

CONDUCTOR		CONDUCTOR DIA.	COMP. D.E. (ITEMS 8 & 14)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR		1.165	VES-130-EHV**	0032000078	C-7686-DE1	NA
954.0 45/7 "RAIL"		1.165	VES-133-EHV**	0032021873	C-7686-DE2	NA
954 54/7 "CARDINAL"		1.196	VES-135-EHV**	0032021874	C-7686-DE4	NA

CONDUCTOR RANGE: BOLTED STRAIN CLAMP (ITEM 12)		ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
.710" - 1.318"	ADE-2526-S-SPH4	0000028892	C-7686-DE3	NA

* ITEMS 15 ARE NOT FURNISHED WITH THE MACLEAN ASSEMBLIES.
** COMPRESSION DEADEND BODIES COME WITH JUMPER TERMINALS, ITEM 14. EITHER OF
OF ITEMS 8 AND 14 CAN BE RETURNED TO STORES WITH THEIR SEPARATE STOCK CODES.

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Attachment 1: Applicable Standard Framing and Assembly Drawings

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BILL OF MATERIALS						
JUMPER LINE POST, POLYMER, w/BUNDLING YOKE, HORIZONTAL, 500kV						
ITEM	QTY.	STOCK NO.	DESCRIPTION			
1	1	LS9015XX	JUMPER YOKE, 10k ULT. STR. 18" SEPARATION, ALUMINUM ALLOY			
2	1	0032021878	INSULATOR, LINE POST, 3", POLYMER, 500kV, 10k ULT. STR.			

CONDUCTOR	CONDUCTOR DIA.	JMPR. YOKE (ITEM 1)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR	1.155	C-7686-4	0032021850	C-7686-J2	NA
954.0 45/7 "BAL"	1.155	C-7686-4	0032021850	C-7686-J2	NA
954 54/7 "CARDINAL"	1.196	C-7686-4A	0032021860	C-7686-J2A	NA

HOLES TO FIT 7/8" DIAMETER BOLTS

SECTION A-A
BASE PLATE

14"

160"

1"

1) ITEM #1 IS CONDUCTOR DEPENDENT. THIS ITEM IS SELECTED FOR EACH PROJECT (WITHOUT ARMOR RODS).

RE: MACLEAN DWG. BC-7686-4

ENTERGY SERVICES, INC.

JUMPER LINE POST, POLYMER, W/YOKE, HOR, 500kV

STD. NO. SCALE: NONE

No. TFA201A0

Entergy

PLOT 1=1 SH. 1 OF 1

JLPB-HJ-500-XX; BC-7686-4

NO.	DATE	CREATED	REVISION	TWF	HSK	BY	CHK	APPR
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tflnc90 3/19/2007

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Attachment 1: Applicable Standard Framing and Assembly Drawings

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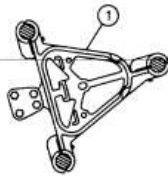
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BILL OF MATERIALS

JUMPER LINE POST, POLYMER, w/BUNDLING YOKE, VERTICAL, 500kV

ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	LS9015XX	JUMPER YOKE, 10k ULT. STR. 18" SEPARATION, ALUMINUM ALLOY
2	1	0032021879	INSULATOR, LINE POST, 3", POLYMER, 500kV, 10k ULT. STR.

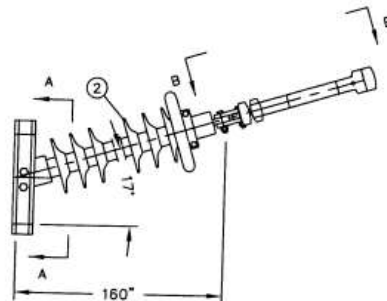
CONDUCTOR	CONDUCTOR DIA.	JMPR. YOKE (ITEM 1)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR	1.165	C-7686-4	0032021850	C-7686-J3	NA
954.0 45/7 "RAIL"	1.165	C-7686-4	0032021850	C-7686-J3	NA
954 54/7 "CARDINAL"	1.196	C-7686-4A	0032021860	C-7686-J3A	NA



SECTION B-B
YOKE PLATE

HOLES TO FIT
7/8" DIAMETER
BOLTS

SECTION A-A
BASE PLATE



- 1) ITEM #1 IS CONDUCTOR DEPENDENT. THIS ITEM IS
SELECTED FOR EACH PROJECT (WITHOUT ARMOR RODS).

RE: MACLEAN DWG. BC-7686-5

ENTERGY SERVICES, INC.

JUMPER LINE POST, POLYMER, W/YOKE, VER, 500kV

STD NO.

SCALE: NONE

No. TFA202A0

PLOT

1=1

SH. 1 OF 1

JLPB-VJ-500-XX; BC-7686-5

NO.	DATE	CREATED	REVISION	TWF	HSK	BY	CHK	APPR
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1	03-05-07							

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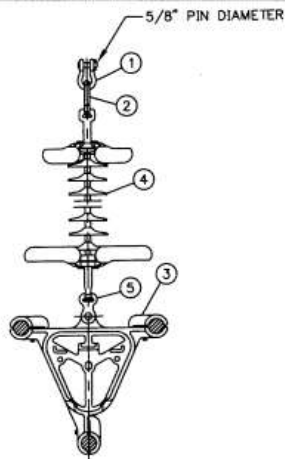
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BILL OF MATERIALS						
JUMPER SUSPENSION, POLYMER, w/ BUNDLING YOKE 500kV						
ITEM	QTY.	STOCK NO.	DESCRIPTION			
1	1	0000004466	SHACKLE, ANCHOR, 30k ULT. STR., 5/8" PIN DIA. 2-13/16"			
2	1	0000028889	BALL EYE, OVAL, 35k ULT. STR., BALL CLASS 52-3/5			
3	1	LS9016XX	YOKE, JUMPER, 10k ULT. STR. 18" SEPARATION, ALUM. ALLOY			
4	1	0032000277	INSULATOR, SUSPENSION, BAS, POLYMER, 500kV, 25k ULT. STR.			
5	1	0032021870	CLEVIS, SOCKET, 30k ULT. STR., CLASS 52-3/5			

CONDUCTOR	CONDUCTOR DIA.	JUMPR. YOKE (ITEM 3)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR	1.165	C-6549-3	0032021827	C-7686-JI	NA
954.0 45/77 "RAIL"	1.165	C-6549-3	0032021827	C-7686-JI	NA
954 54/77 "CARDINAL"	1.196	C-7686-5	0032021863	C-7686-JIA	NA



- 1) ITEM #3 IS CONDUCTOR DEPENDENT.
THIS ITEM IS SELECTED FOR EACH
PROJECT WITHOUT ARMOR RODS.

RE: MACLEAN DWG. BC-7686-2

ENTERGY SERVICES, INC.

JUMPER SUSPENSION, POLYMER, W/YOKE, 500kV

STD NO. SCALE: NONE

No. TFA203A0

Entergy

PLOT 1=1 SH. 1 OF 1
JSPB-500-XX; BC-7686-2

-05-07	CREATED	TWF	HSK
DATE:	REVISION	BY:	CHK:
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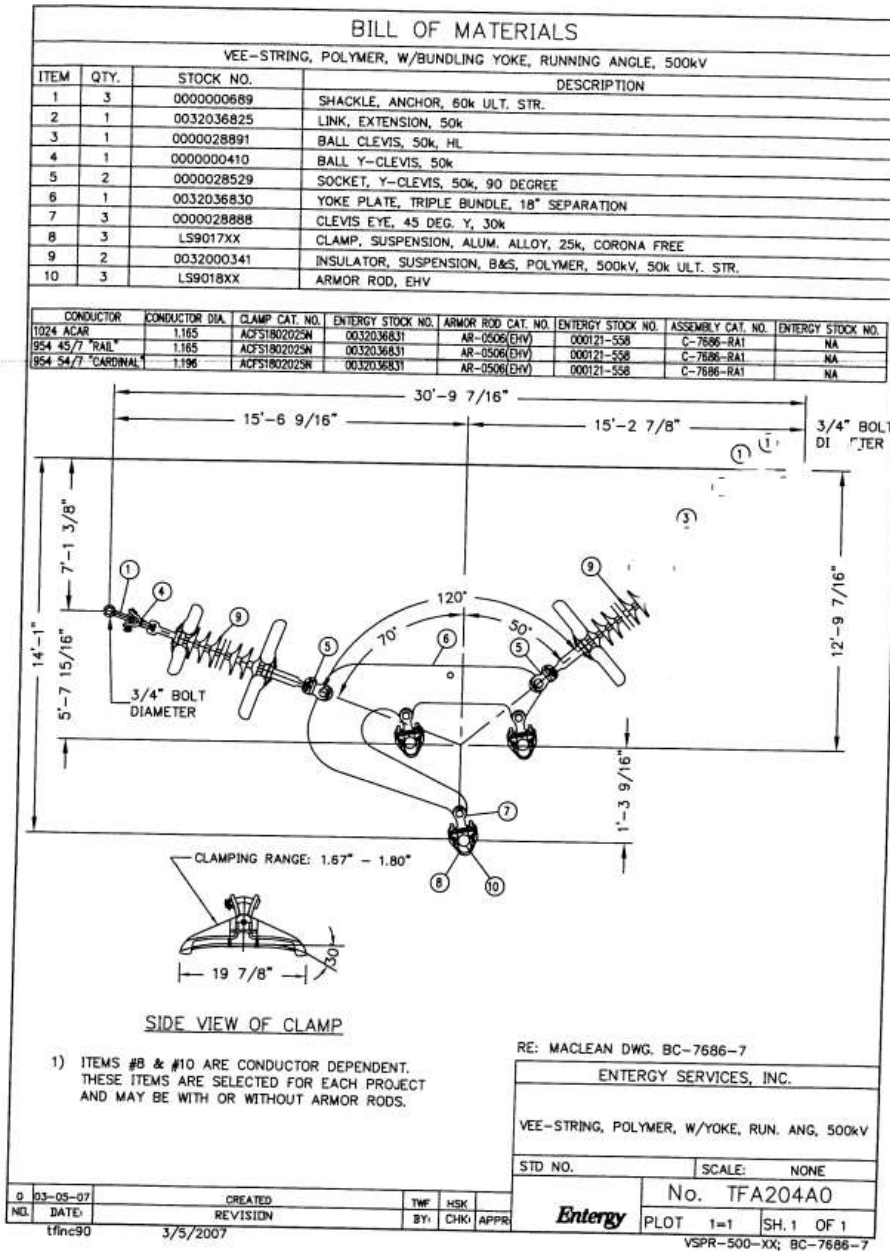
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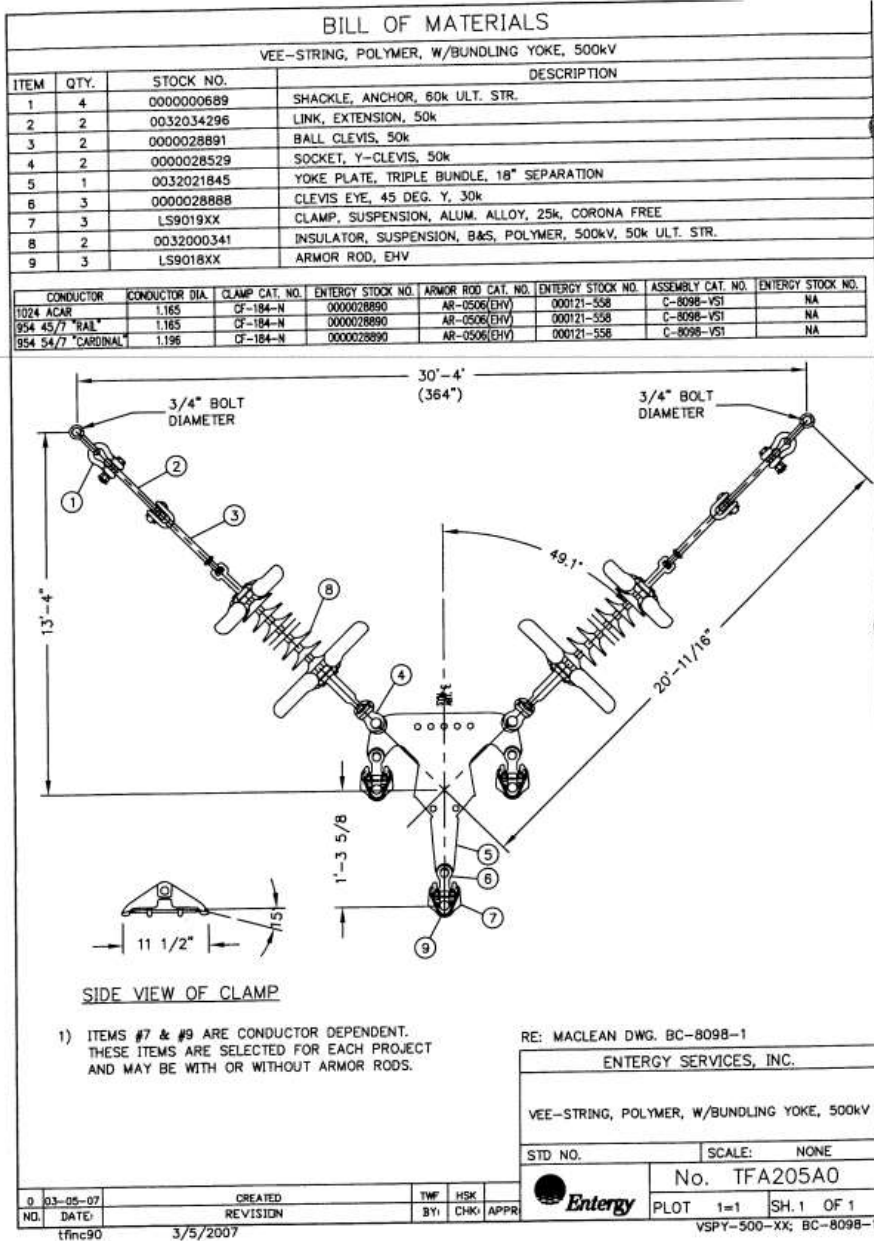
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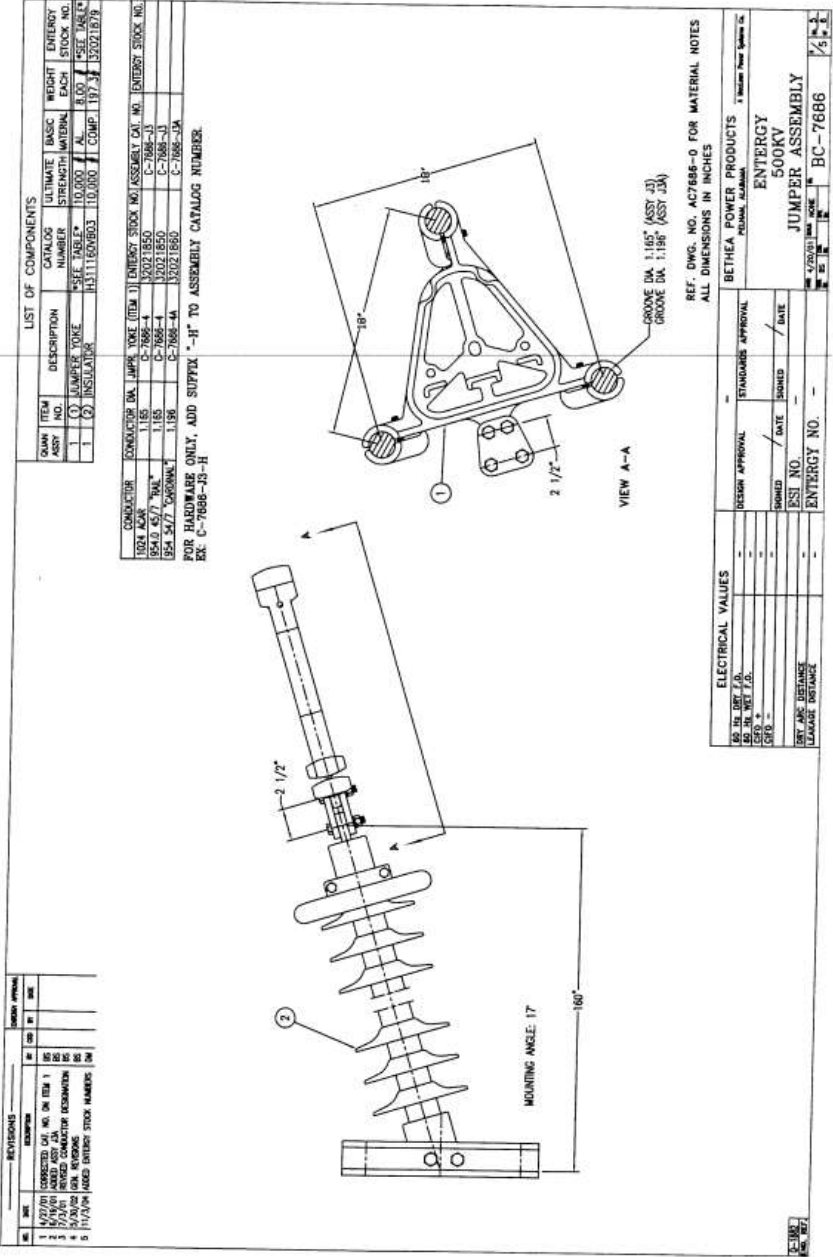


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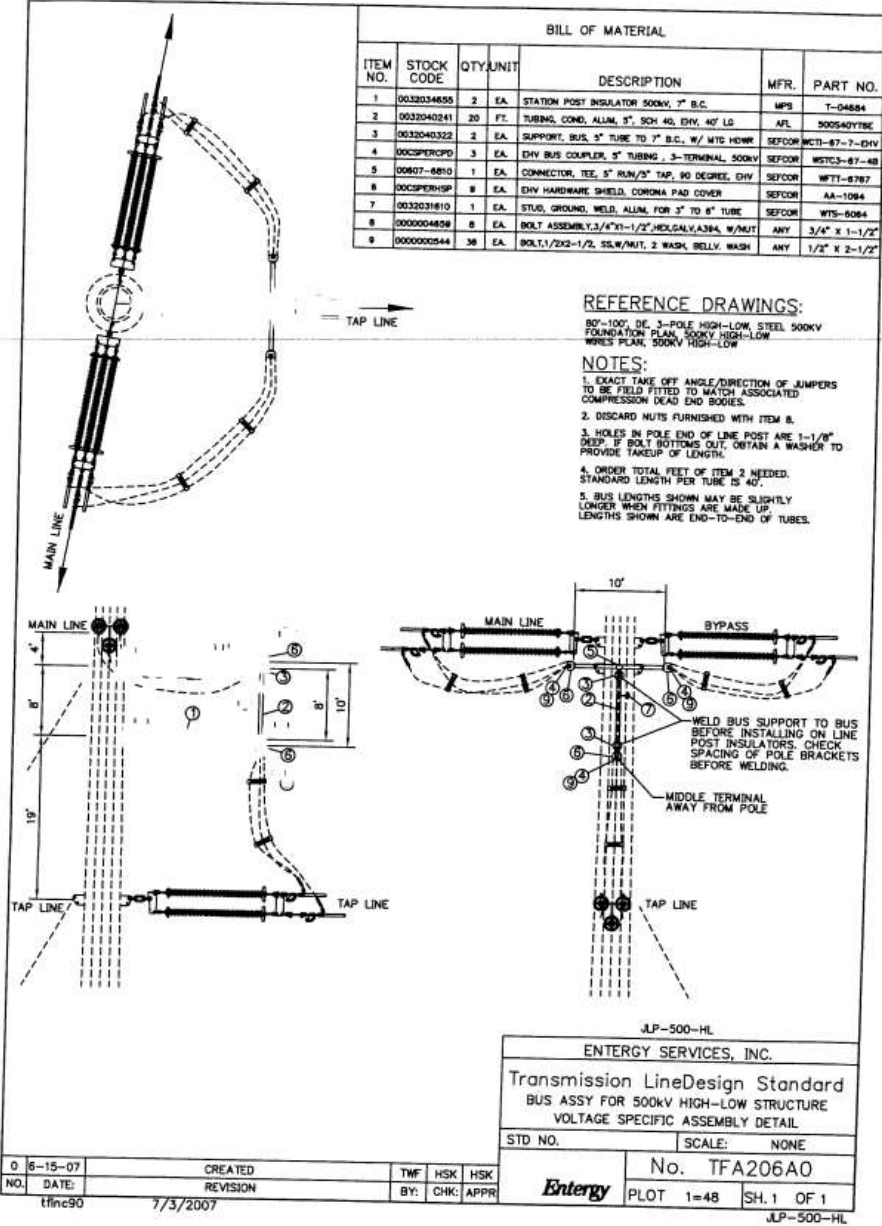


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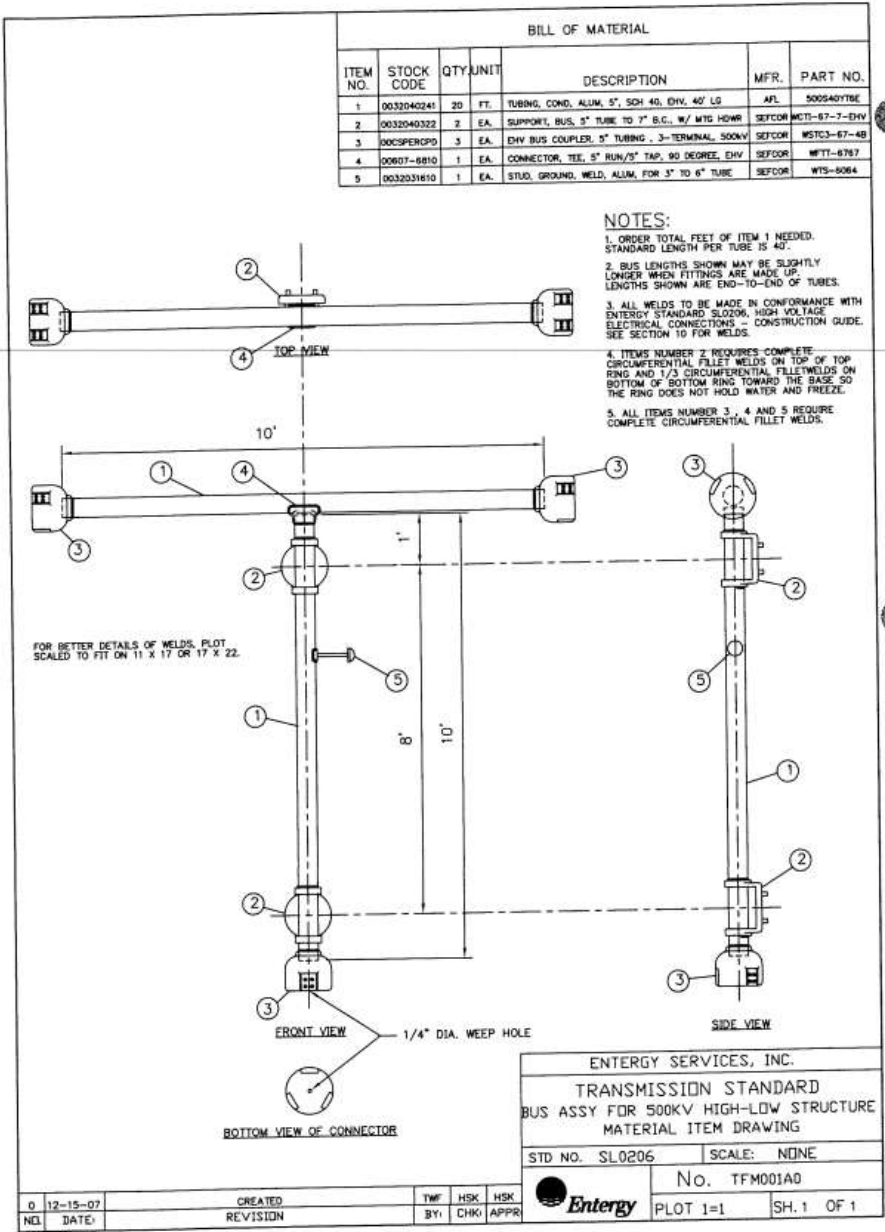
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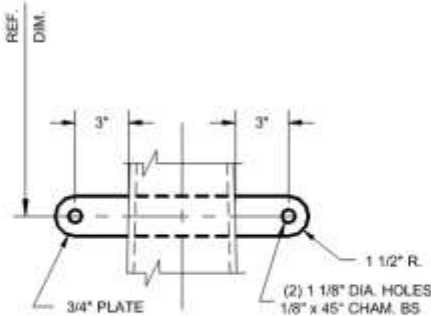
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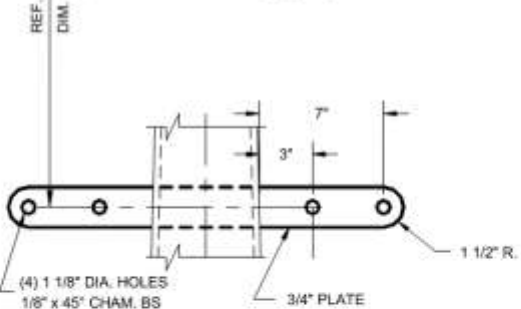
Vang Details for Steel Poles



LIGHT-DUTY 2-HOLE VANG

Primary uses:

- Support shield wire span guys
- Support top of braced-post insulator assemblies
- Support conductor swinging angle assemblies



LIGHT-DUTY 4-HOLE VANG

Primary use:

- Support shield wire suspension

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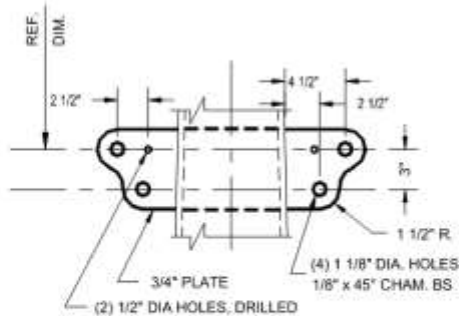
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Attachment 1: Applicable Standard Framing and Assembly Drawings

Vang Details for Steel Poles



HEAVY-DUTY 4-HOLE VANG

Primary use:

Support shield wire deadend assemblies
Support conductor deadend assemblies
Support conductor deadend down guys
Support conductor bisector down guys
Support shield wire deadend down guys
Support shield wire bisector down guys
All conductor and shield wire vangs on structures with running
angle insulators (E, F and G)

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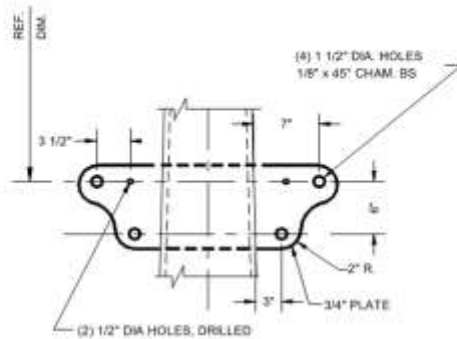
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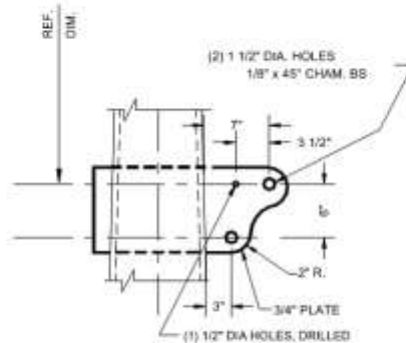
Vang Details for Steel Poles



HEAVY-DUTY 4-HOLE VANG FOR TRIPLE BUNDLE SINGLE POINT DEAD ENDS

Primary use:

Support 500kv conductor dead end assemblies where guys will be at the same elevation as the conductors and when guys are not specified.



HEAVY-DUTY 2-HOLE VANG FOR TRIPLE BUNDLE SINGLE POINT DEAD ENDS

Primary use:

Support 500kv conductor dead end assemblies and guys where guys are specified and will attach at locations below the conductors. Do not install guy vangs on unguyed structures with this type of vang unless specified by Entergy.

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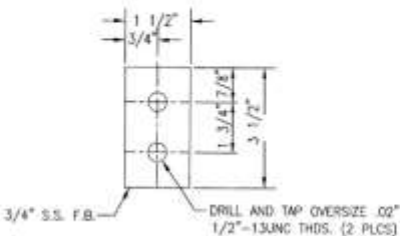
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Attachment 1: Applicable Standard Framing and Assembly Drawings

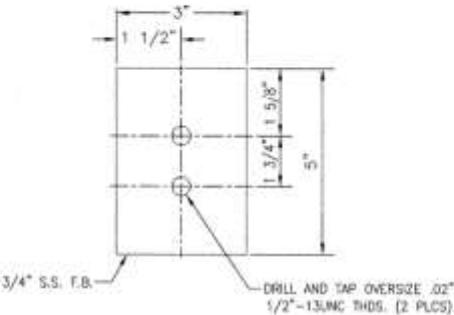
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NEMA Pad Details for Steel Poles or Caissons



SMALL NEMA 2-HOLE PAD



LARGE NEMA 2-HOLE PAD

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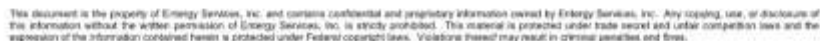
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TDS021A1, Step and Bracket Details, represents the Entergy specifications for drop-in steps.



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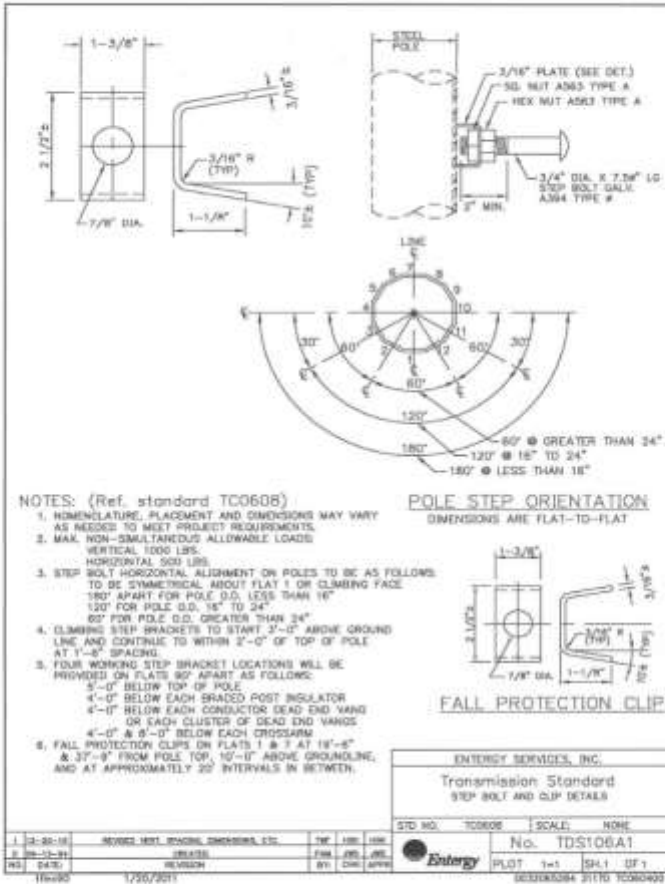
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Climbing Details

TDS106A1, Step Bolt Details, represents the Entergy specifications for pole steps.



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Attachment 1: Applicable Standard Framing and Assembly Drawings

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BILL OF MATERIAL			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	NONE	SIGN, SLOW-VEHICLE, ACQUIRED BY LOCAL PURCHASE
2	8 FT.	0000017124	BAND, STRAPPING, 3/4" WD X 100FT LG ROLL, STAINLESS STEEL, 201
3	2	0032047234	BRACKET, BANDING, FLARED LEG, SS, WITH ONE 5/16"-18 X 3/4" HEX HEAD SS BOLT AND FIBER WASHER, 3/4" SLOT, SHIPPED 50/BOX
4	2	0000017123	BOLT, CLAMP ASSEMBLY, CARRIAGE HD, GALVANIZED STEEL, HIGH STRENGTH, ASTM B221 MILITARY QQ-A-200/B, 5 GR, 3/8" DIA, 6" LG HIGH STR CARR BOLT, WASH AND NUT

NOTES:

- 1) This installation is optional with the grids, and represents a standard for uniformity across the system wherever it is used.
- 2) Install one slow-vehicle sign on third & fourth structures on each side of overhead line crossings of lines to be patrolled by helicopter to provide advance warning of aerial hazard ahead. Additional structures may be marked where sight distance or visibility is limited.
- 3) Place the markers near the pole tops and away from the hazard so it will be seen as the helicopter approaches the line crossing.
- 4) Slow-vehicle signs are available for local purchase at farm supply stores and major hardware stores.
- 5) If there are two overhead line crossings in close proximity of each other, install two markers one above the other on each structure. Some structures in between may require single markers on both sides of each structure.
- 6) Fasten markers to poles with 3/4" banding as indicated in the Bill of Material above. Wooden poles may have the markers fastened with galvanized lag screws, 1/4" by 2-1/2" and washers. Additional holes or enlarged holes may be necessary in the marker.
- 7) On wooden poles, do not install hardware cloth over the face of the markers.

SGN-HAZ-XNG
ENTERGY SERVICES, INC.
Transmission LineDesign Standard
LINE CROSSING HAZARD MARKING
STRUCTURAL ASSEMBLY DETAIL

STD. NO.	SCALE: NONE
No. TMD407A0	
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SH. 1 OF 1	

ENTERGY
12/11/2008
SGN-HAZ-XNG

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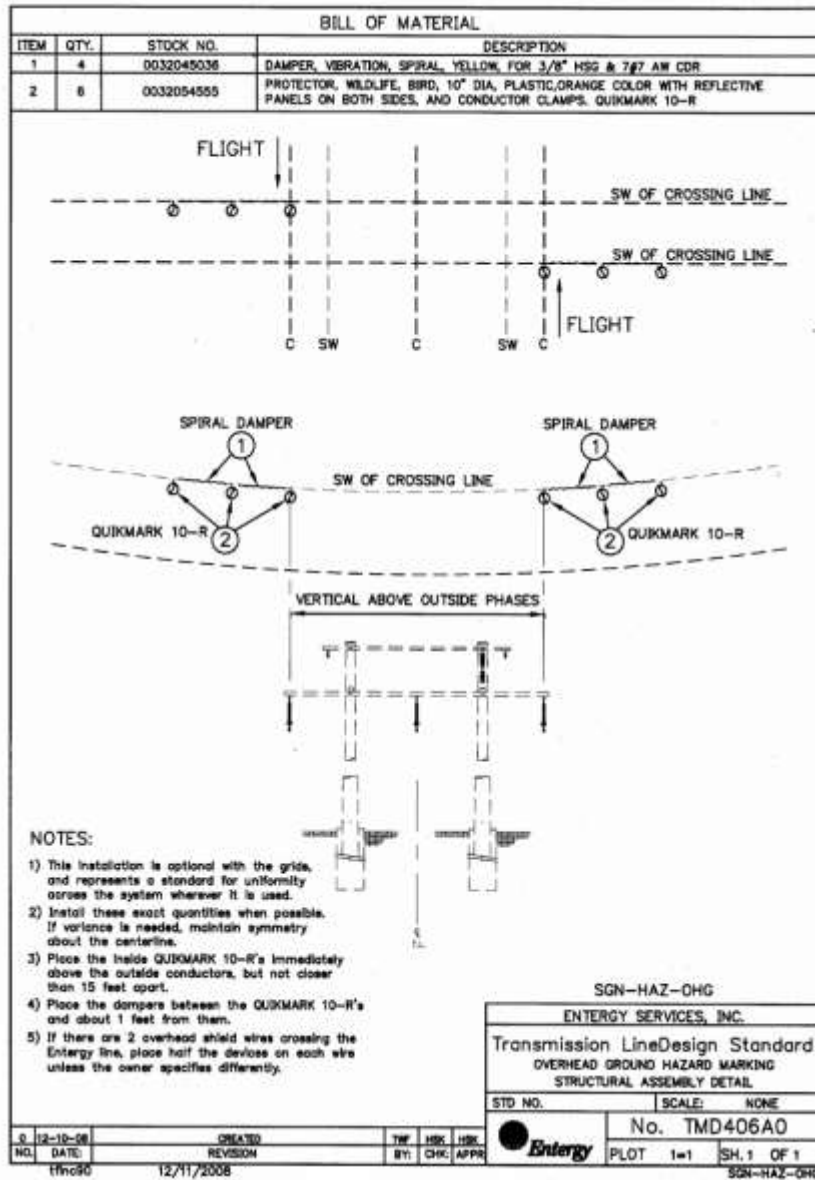
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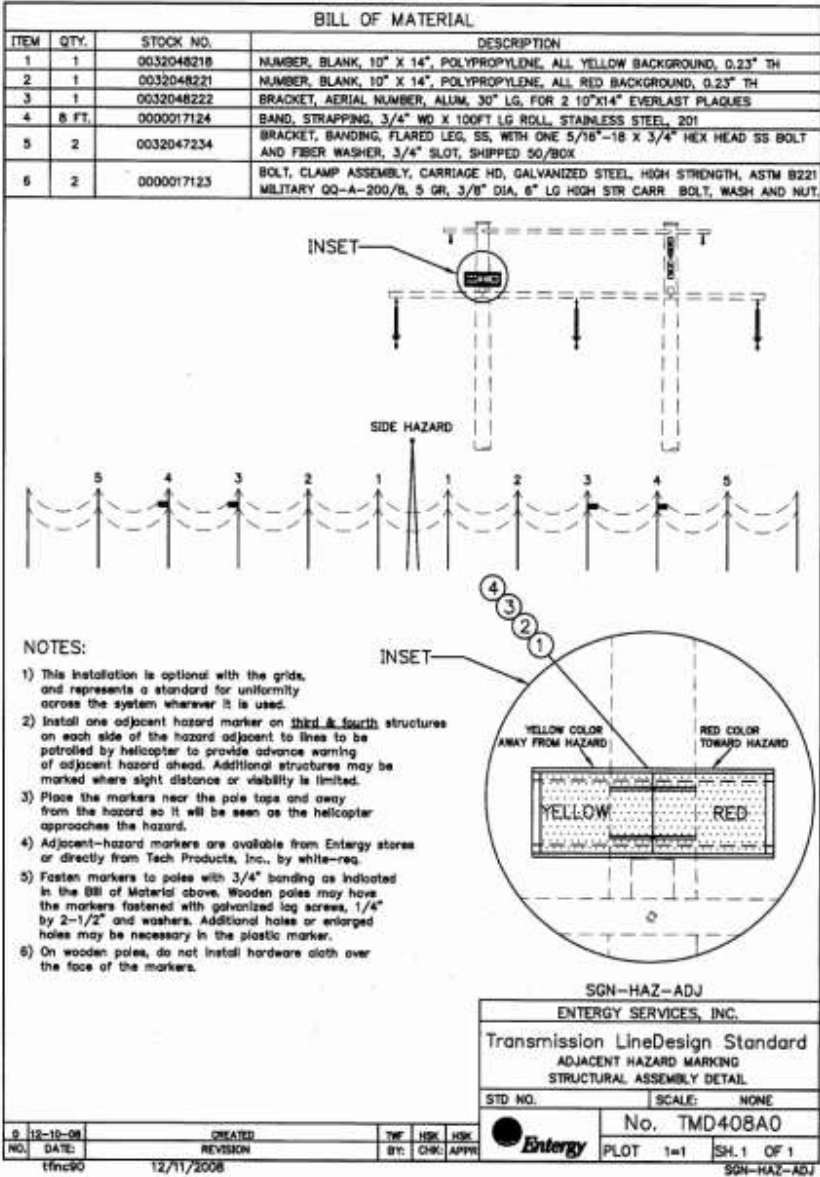
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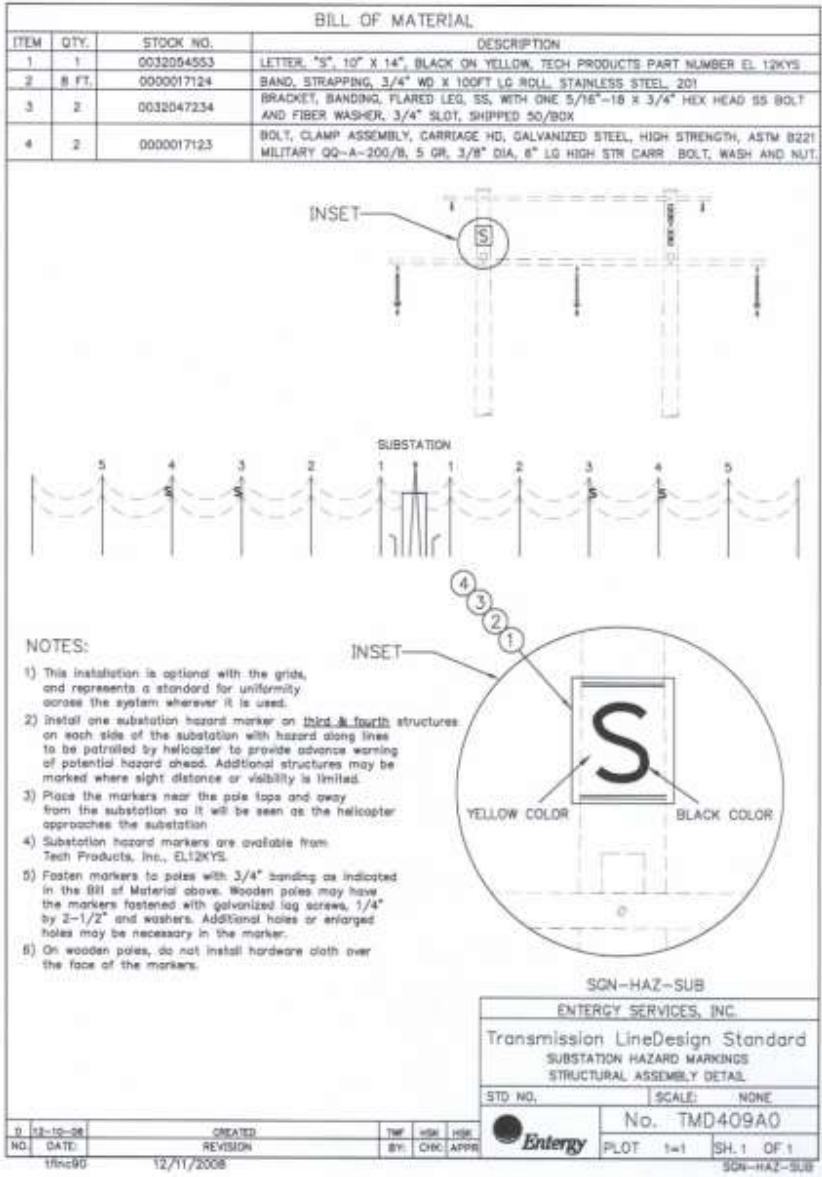
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~~Attachment 1: Applicable Standard Framing and Assembly Drawings~~

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~~**ATTACHMENT 2 – NESC AND ENTERGY CLEARANCE
REQUIREMENTS**~~

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ATTACHMENT 1

APPLICABLE STANDARD FRAMING AND ASSEMBLY DRAWINGS

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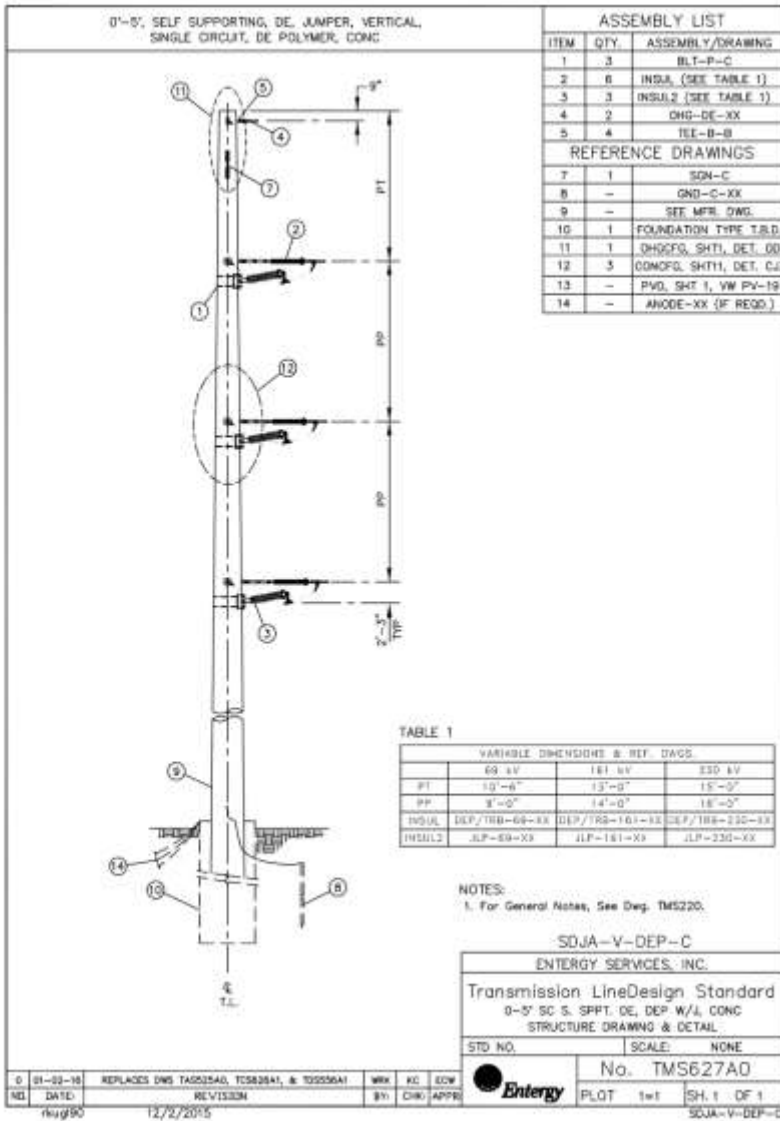
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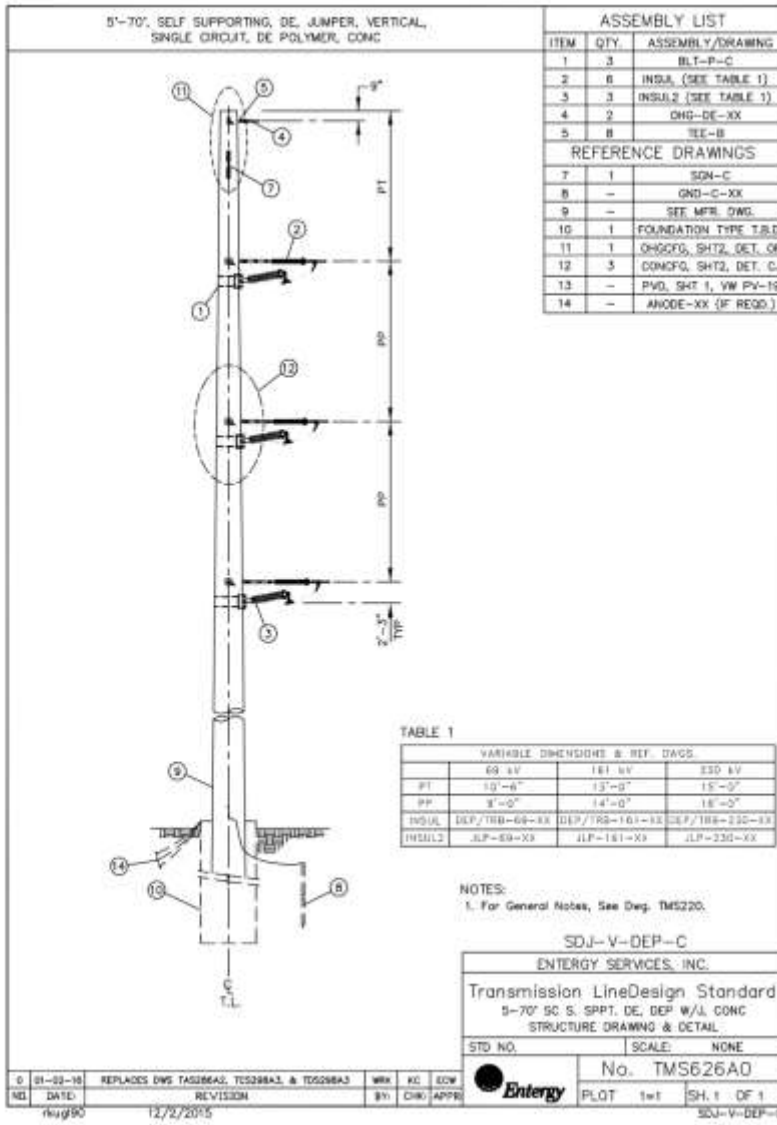
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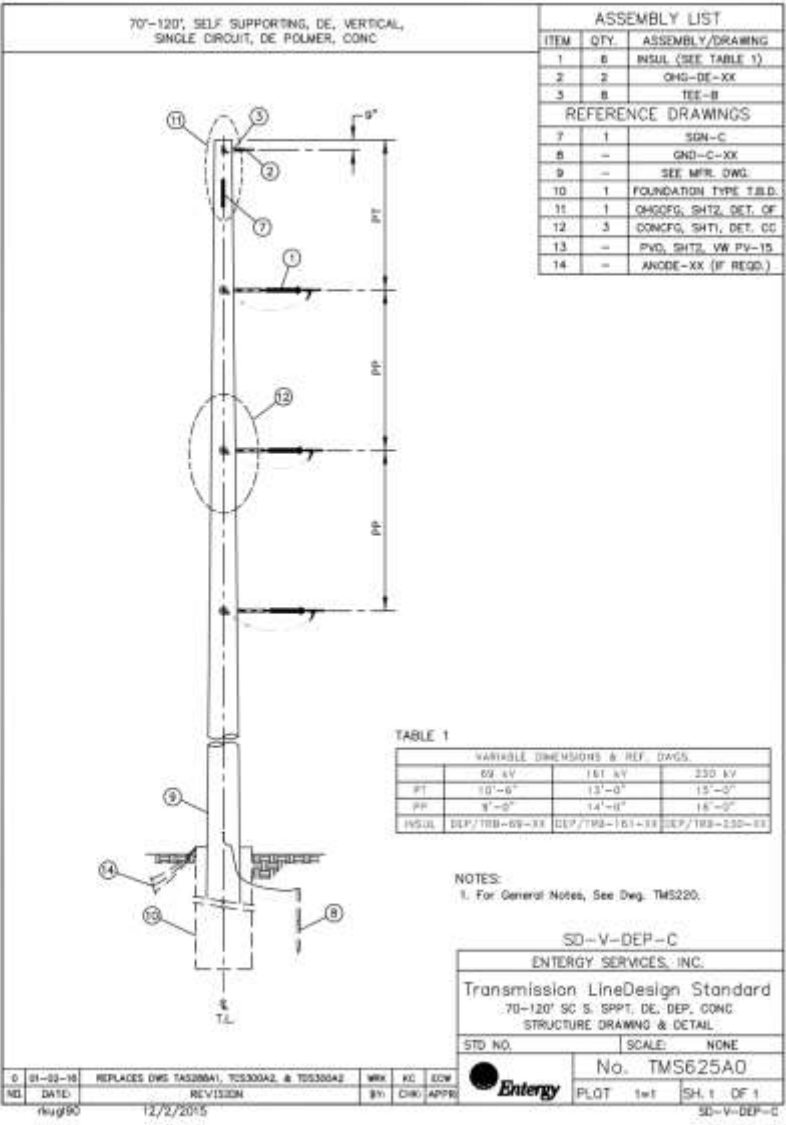
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Attachment 1: Applicable Standard Framing and Assembly Drawings

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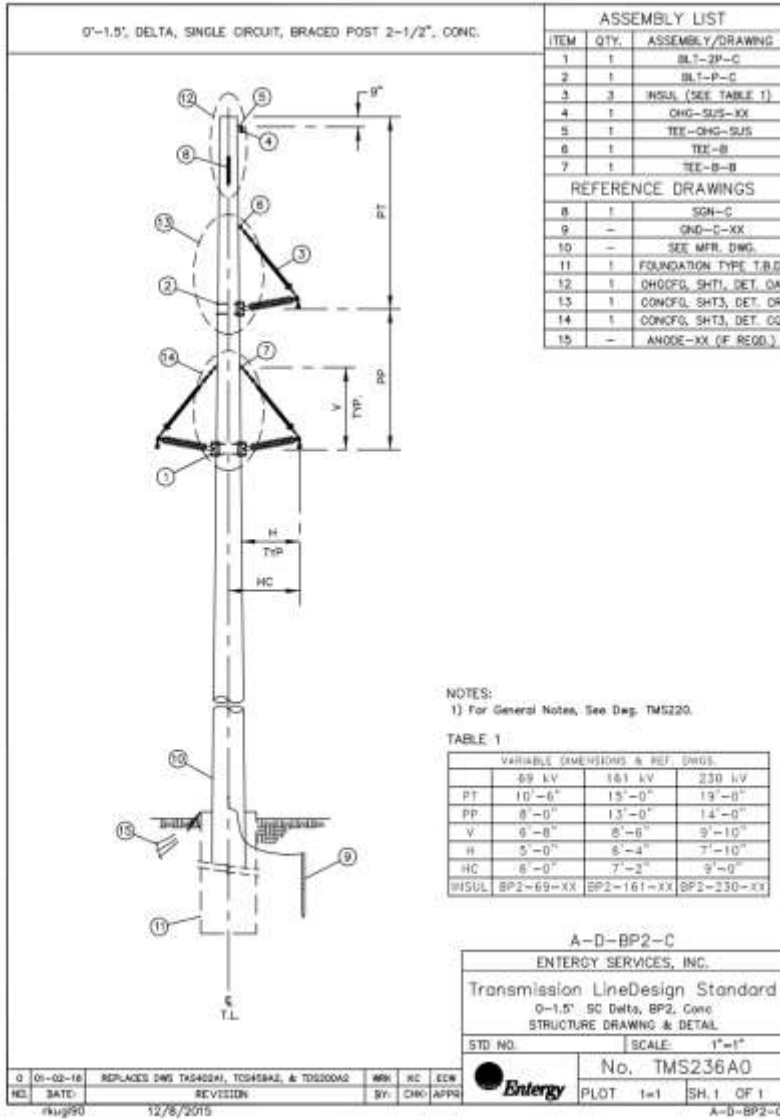
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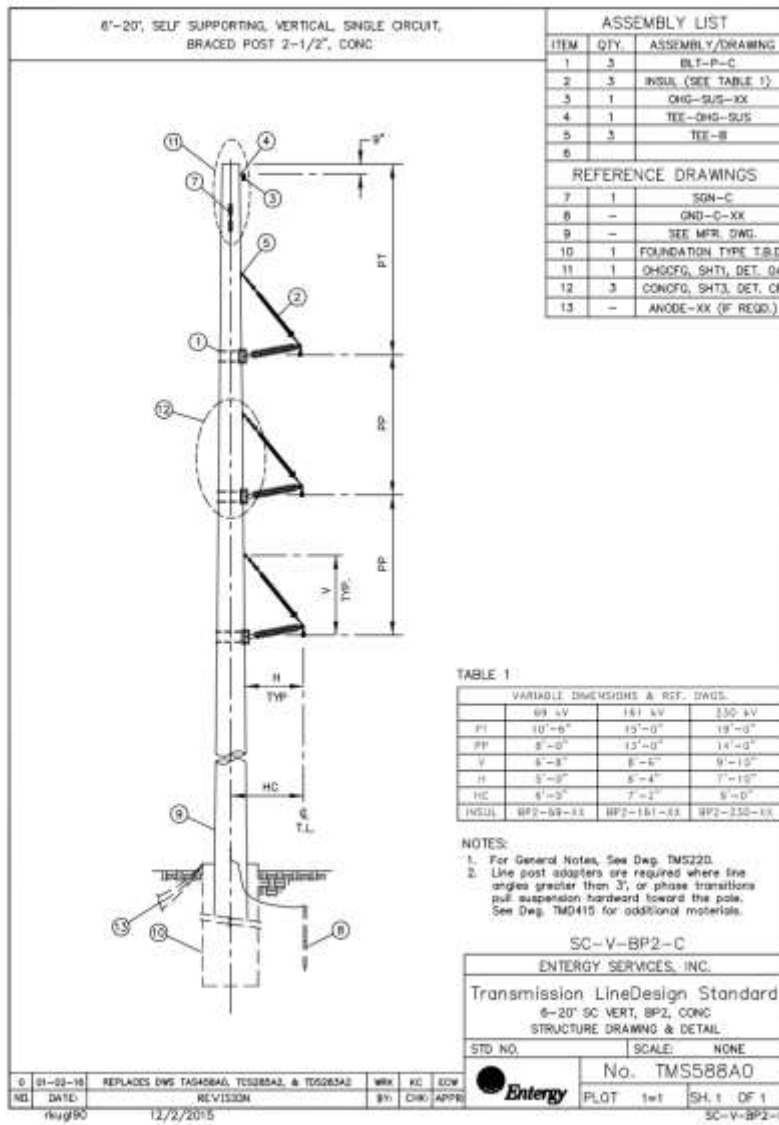
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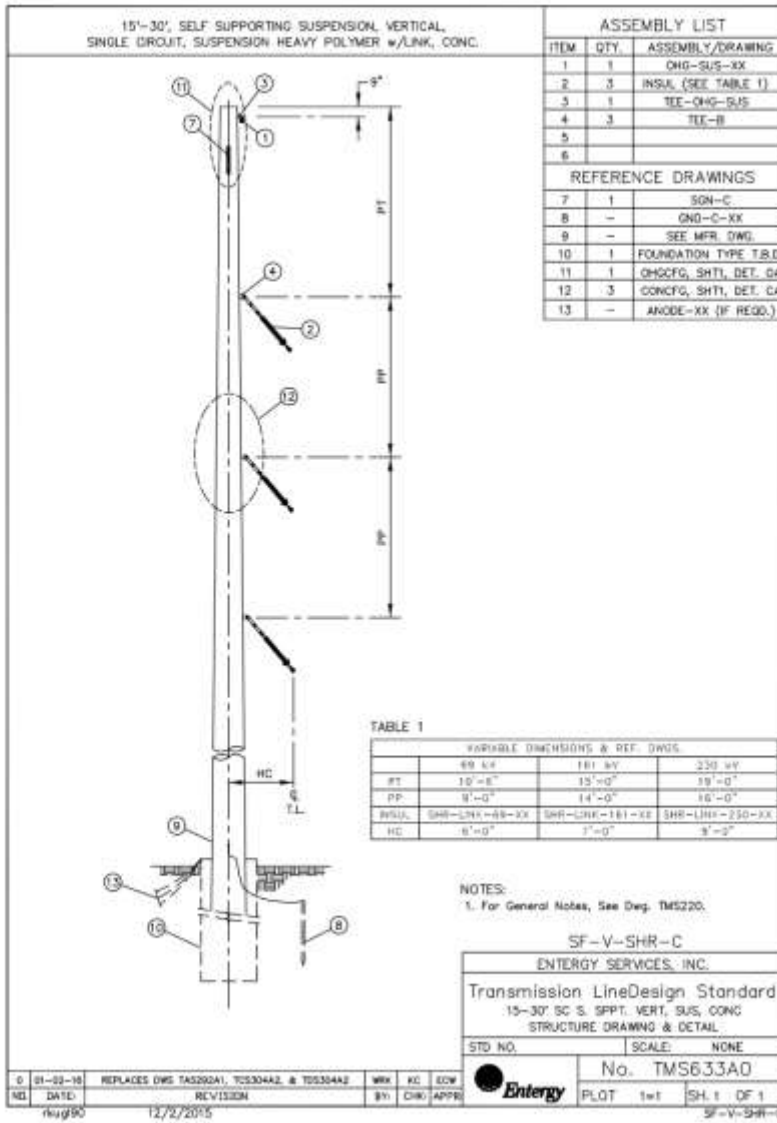
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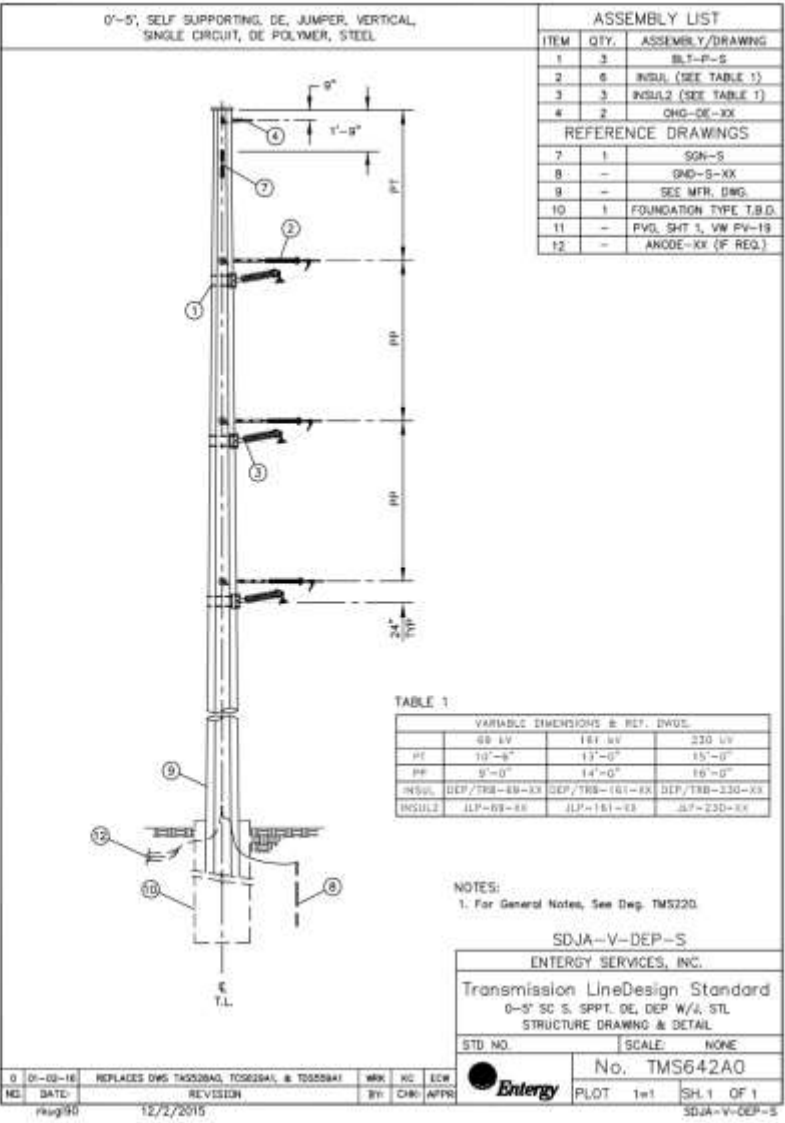
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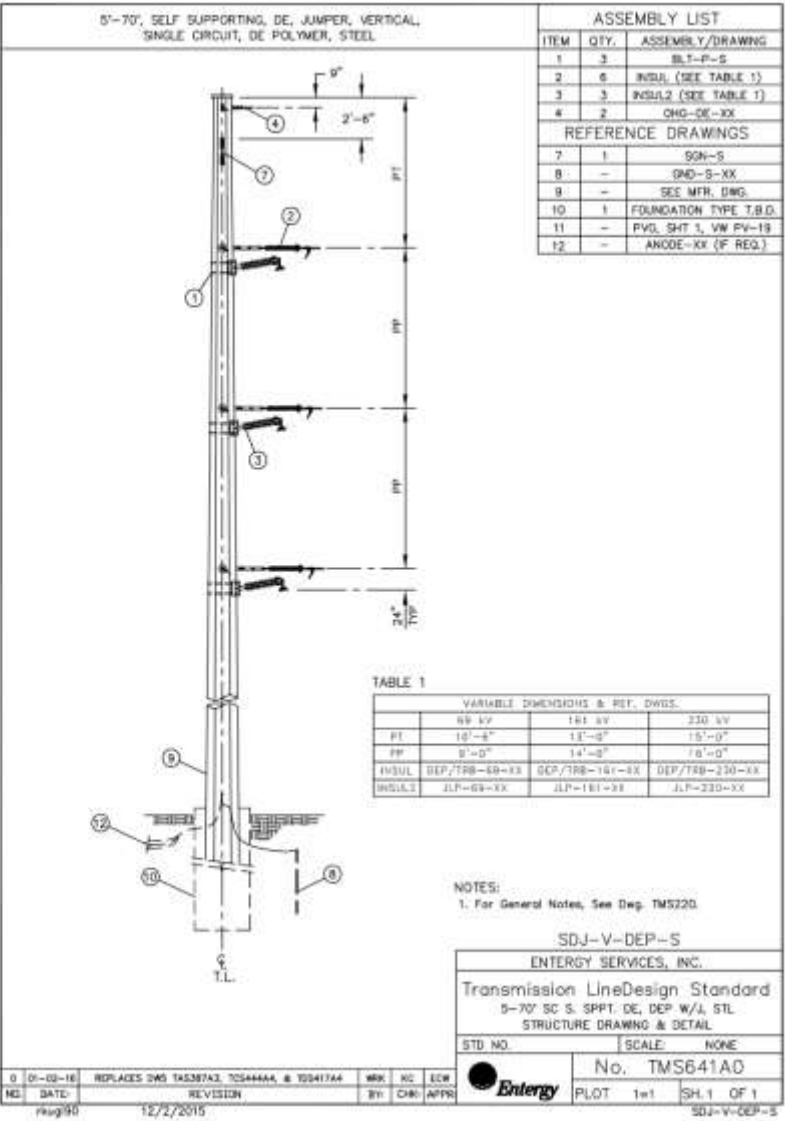
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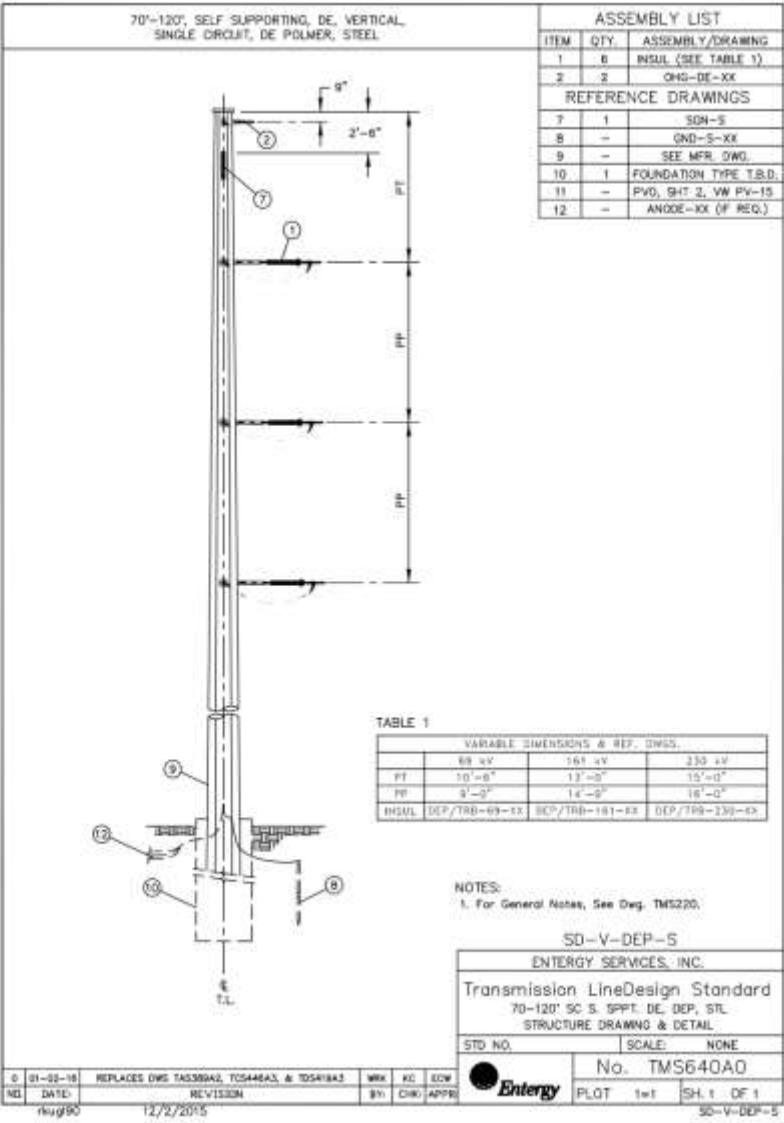
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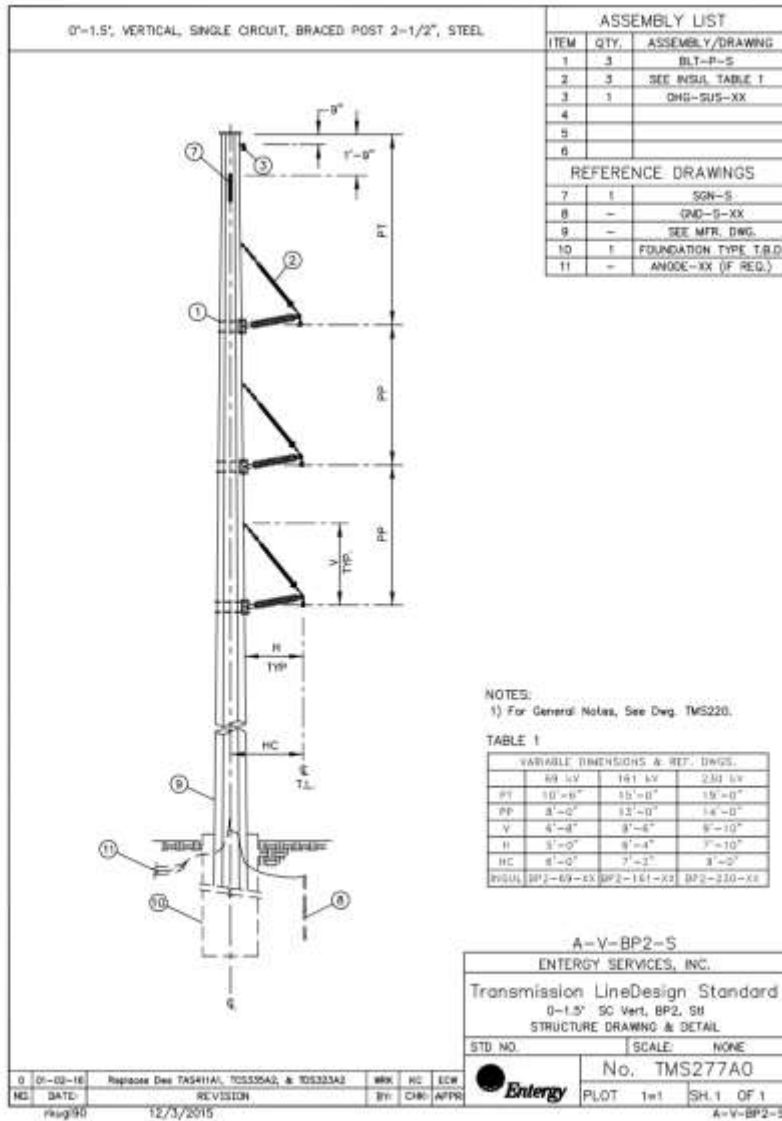
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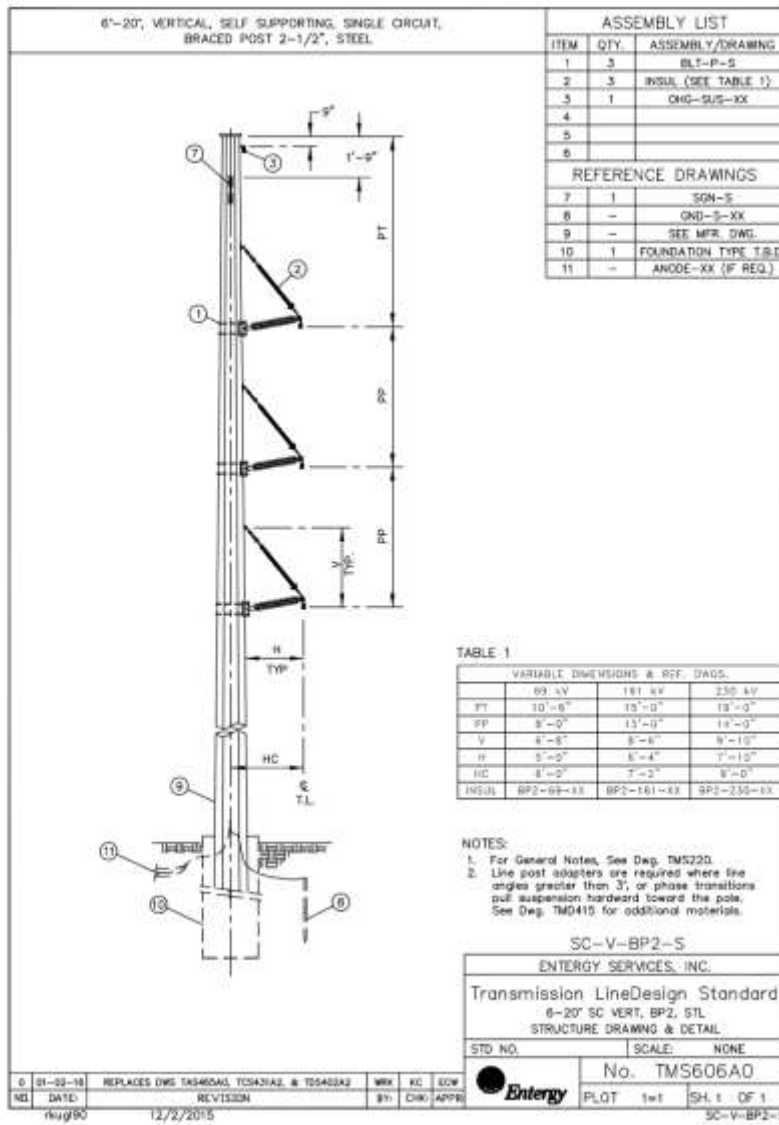
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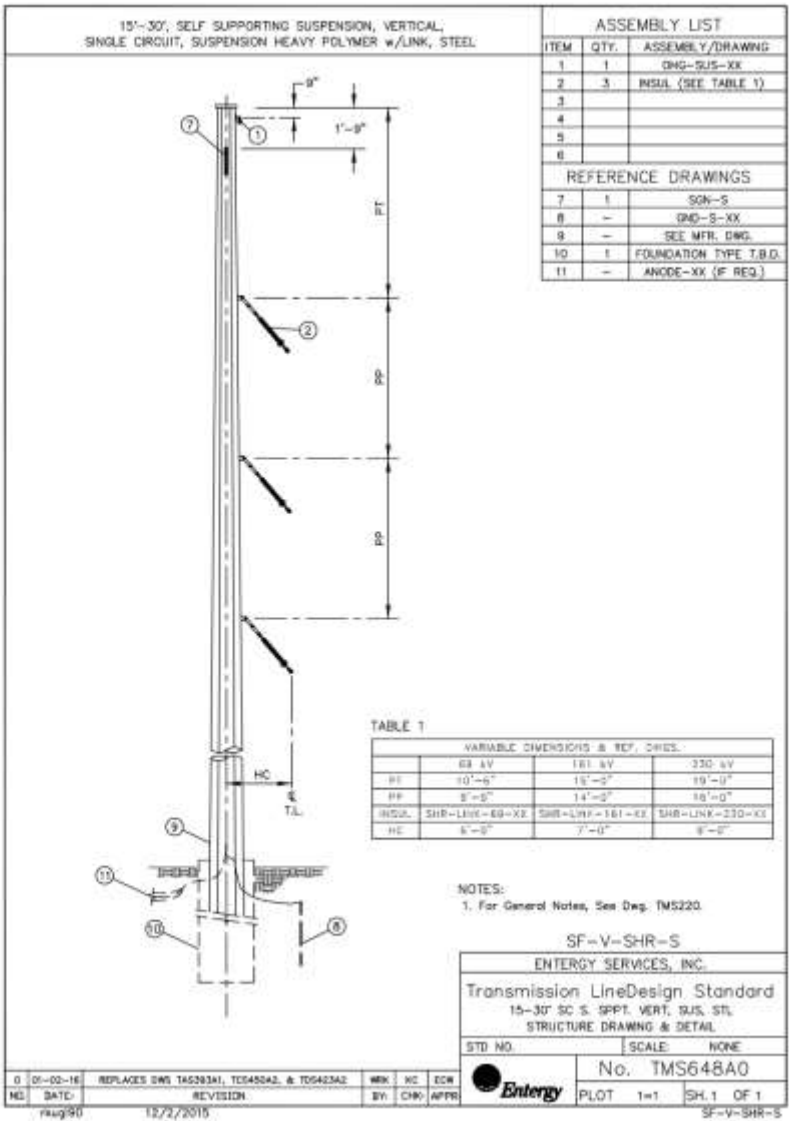
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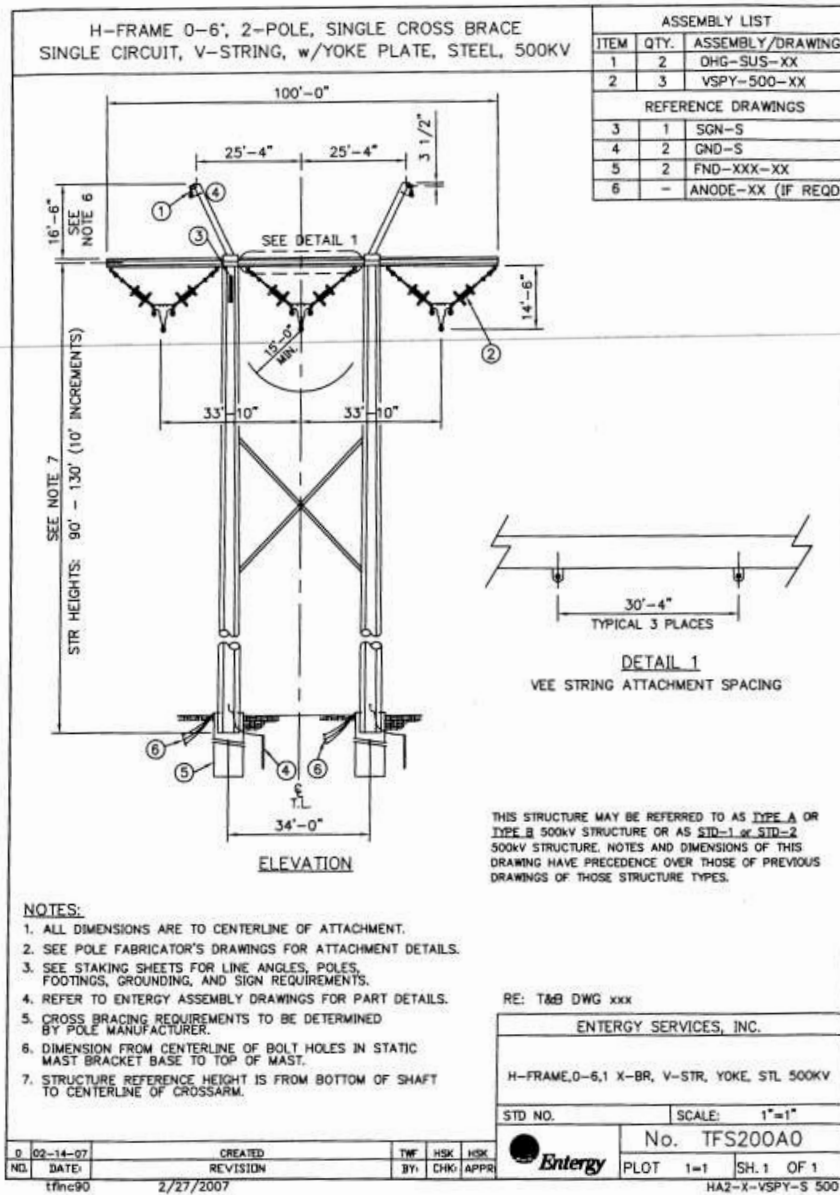
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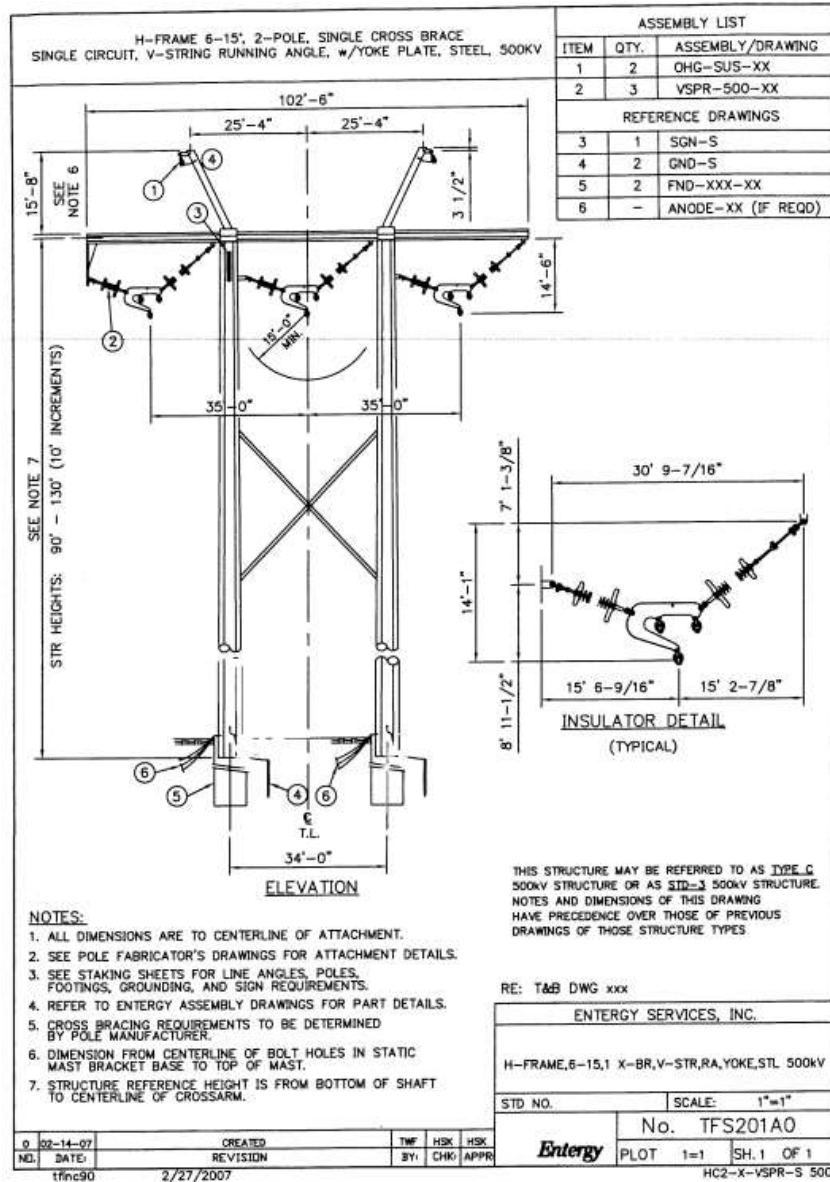


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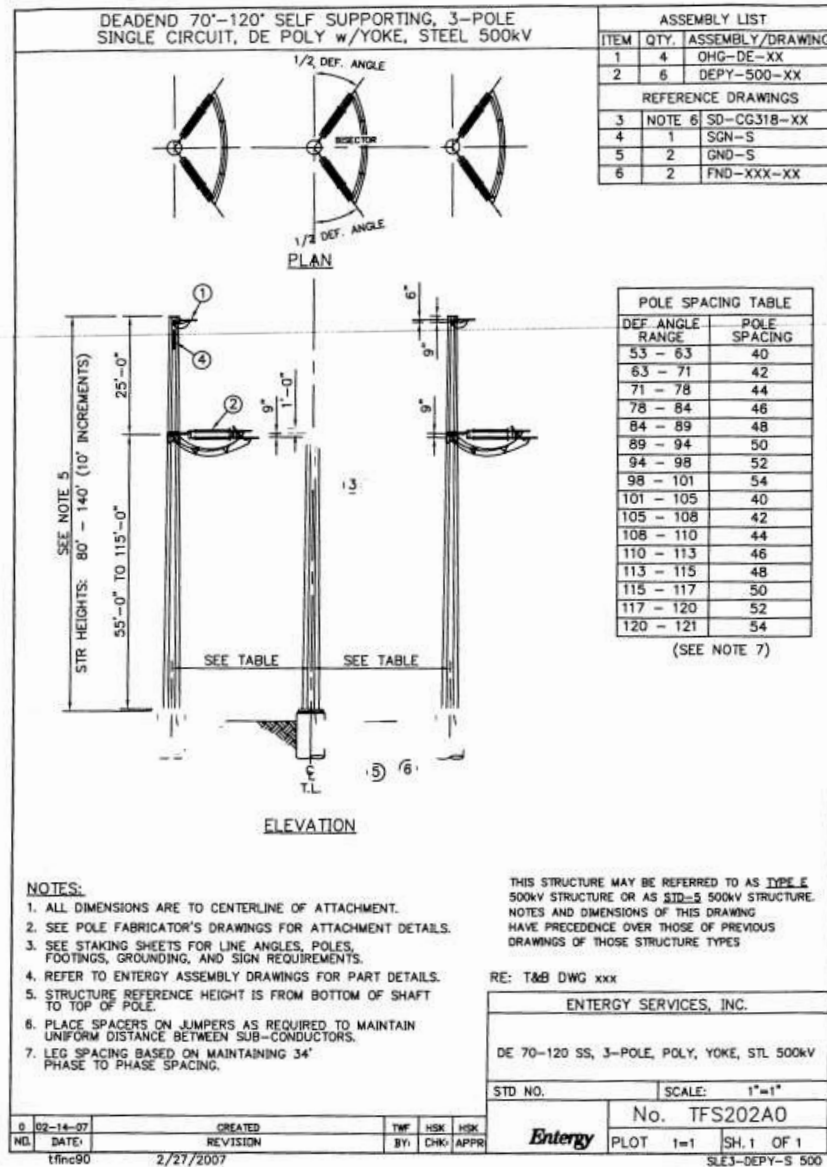
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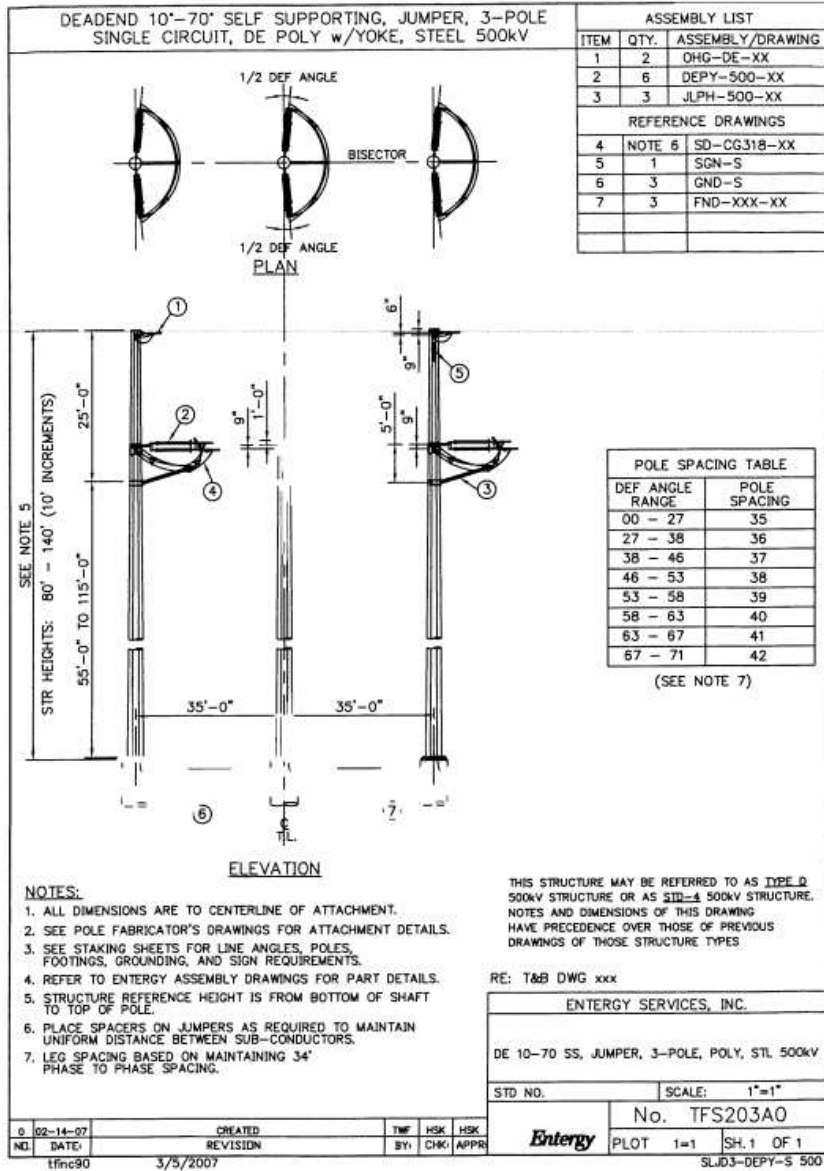
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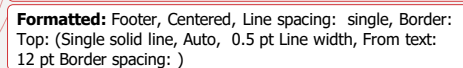


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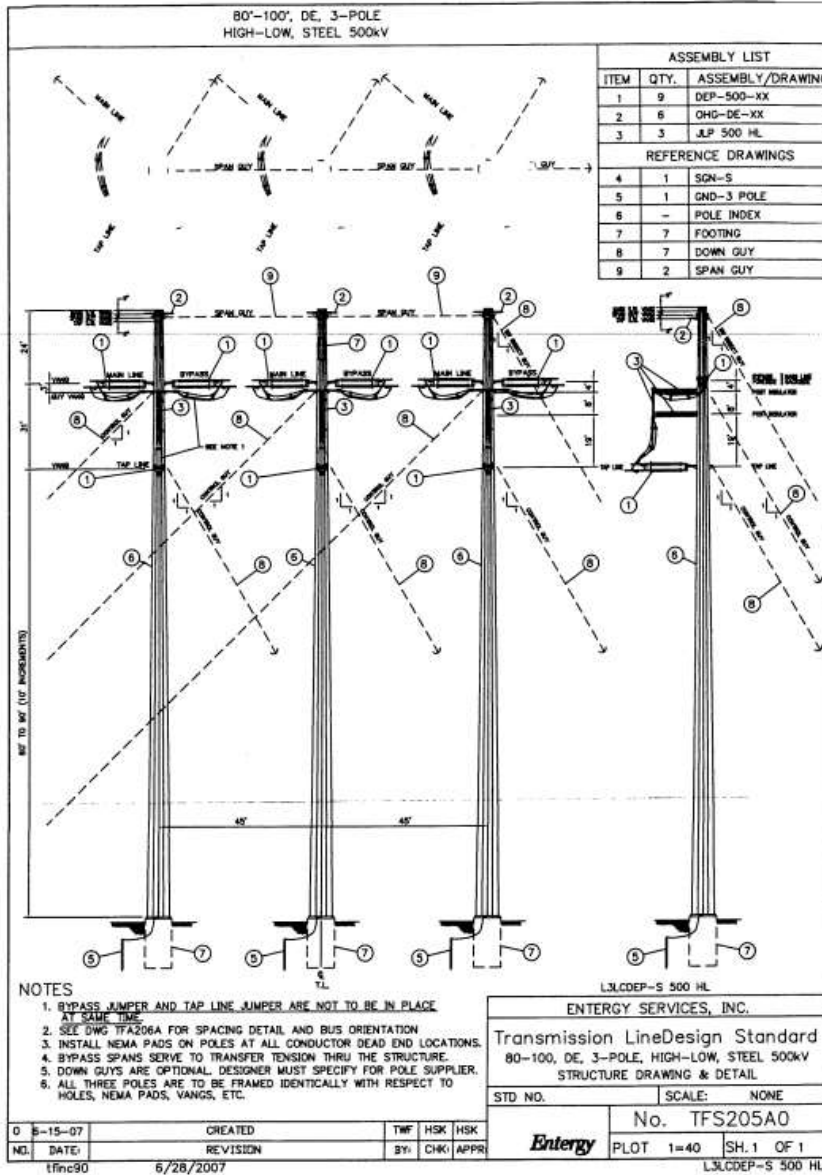


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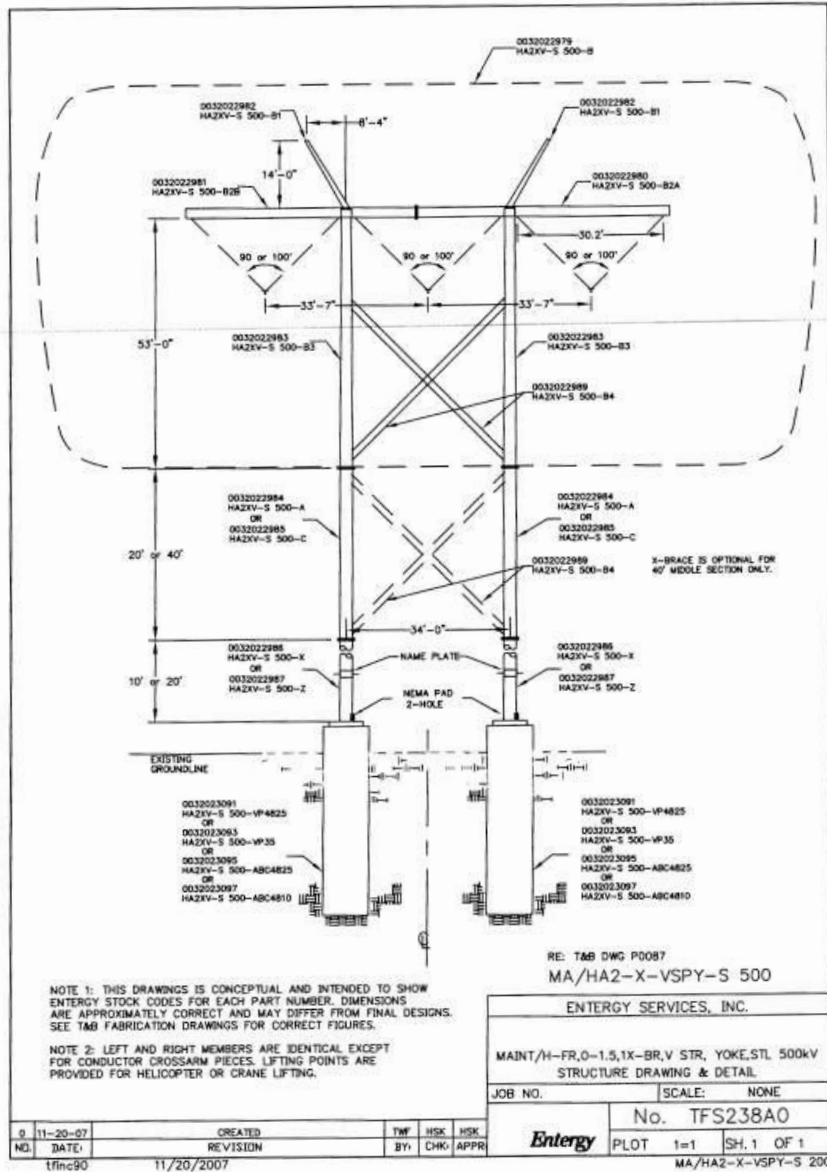
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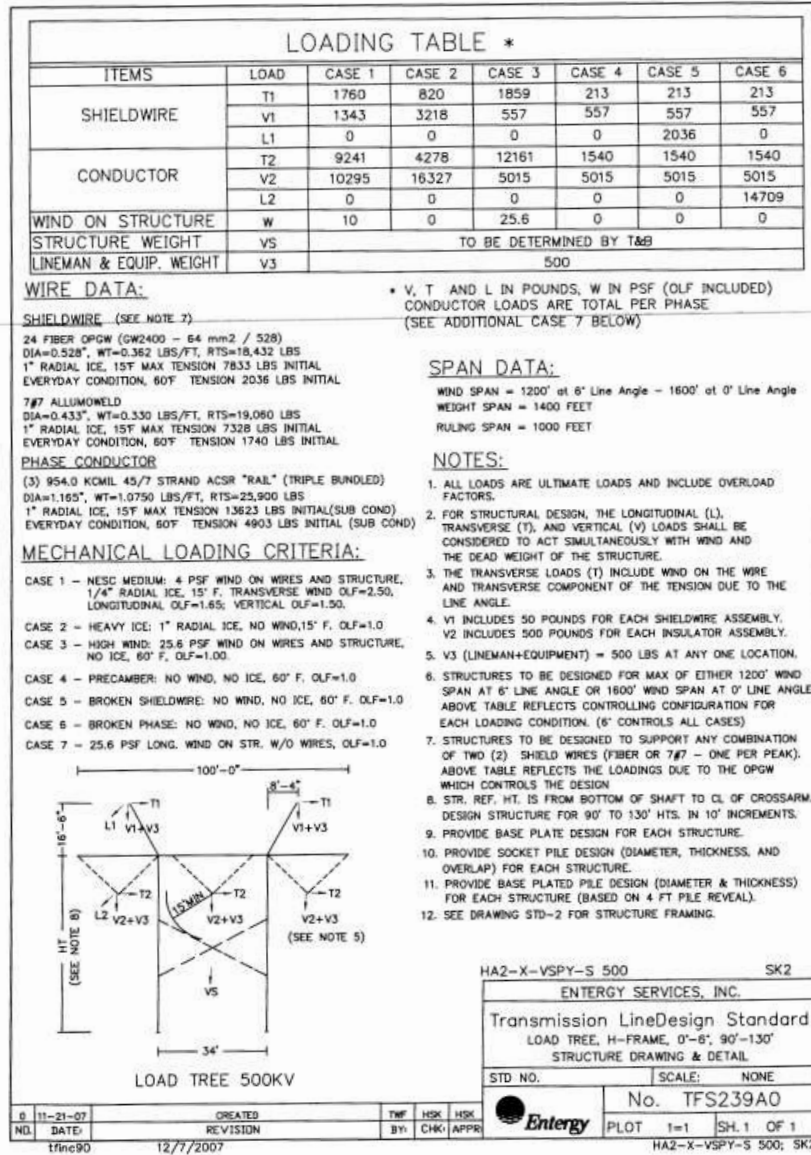
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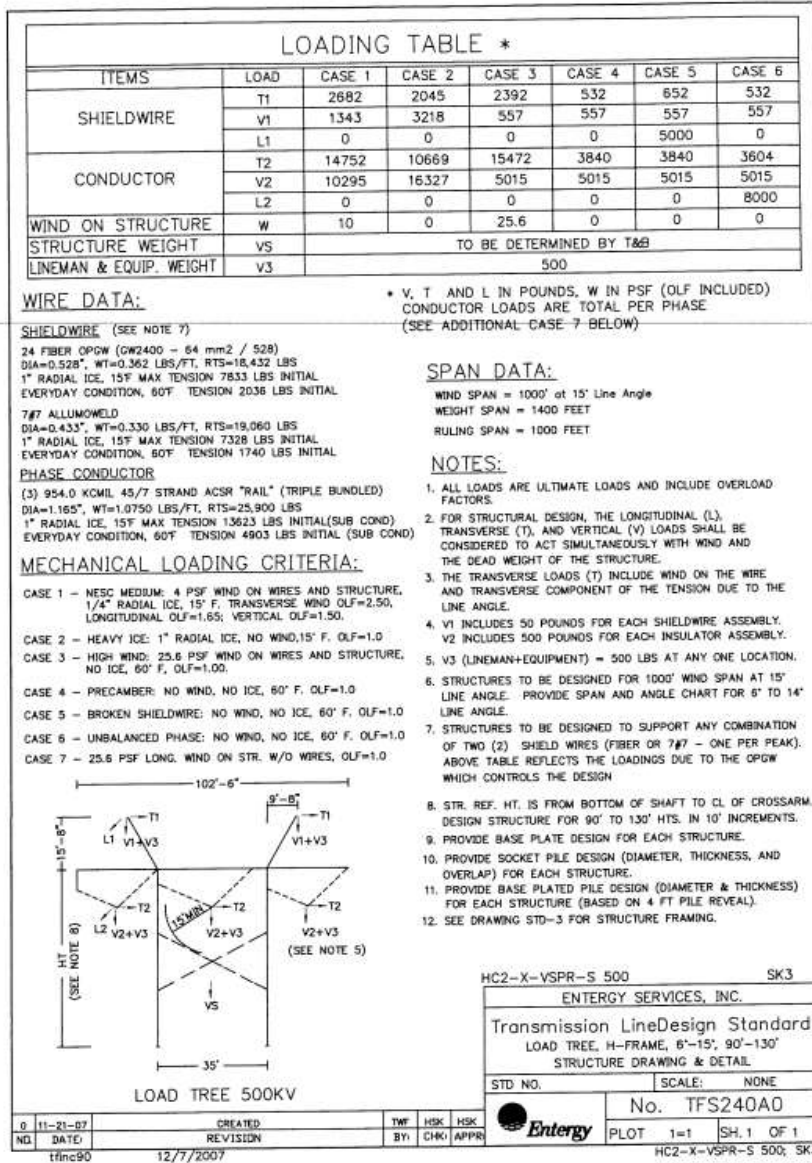
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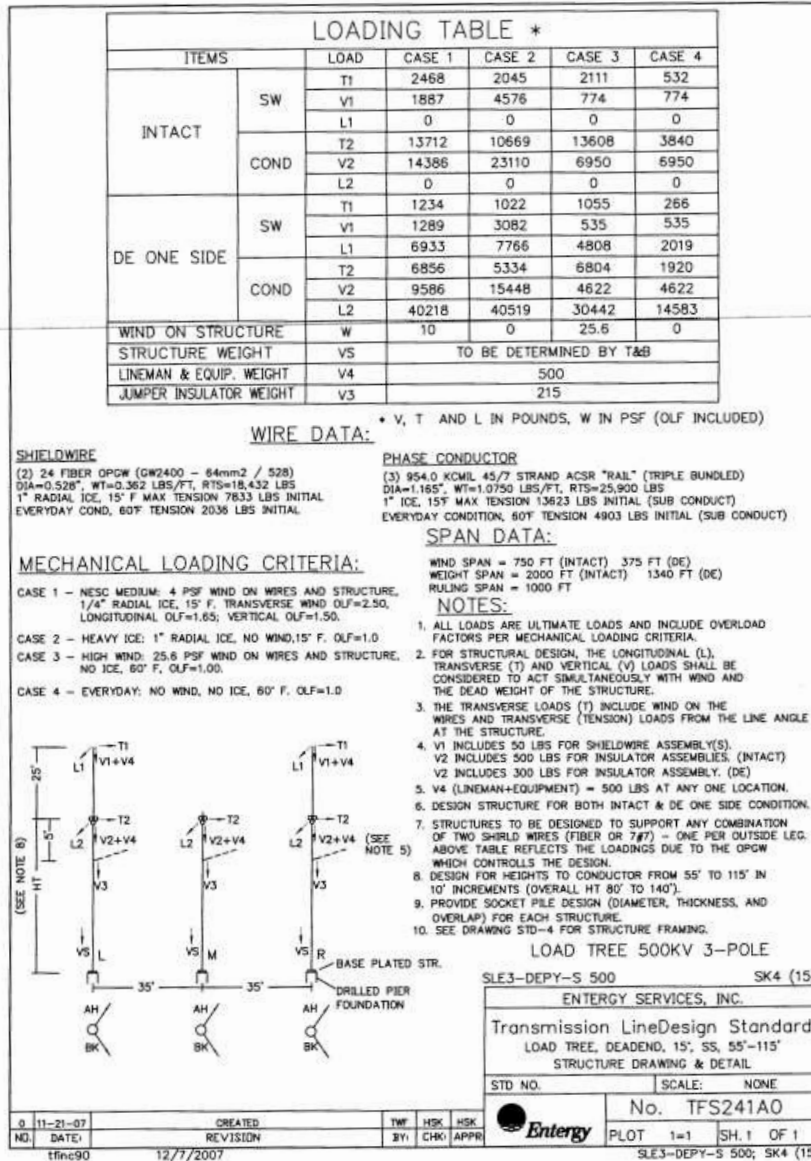
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LOADING TABLE *						
ITEMS		LOAD	CASE 1	CASE 2	CASE 3	CASE 4
INTACT	SW	T1	3669	3391	2944	881
		V1	1887	4576	774	774
		L1	0	0	0	0
	COND	T2	20682	17691	18884	6397
		V2	14386	23110	6950	6950
		L2	0	0	0	0
DE ONE SIDE	SW	T1	1835	1695	1472	441
		V1	1289	3082	535	535
		L1	6827	7647	4734	1988
	COND	T2	10341	8846	9442	3184
		V2	9586	15448	4622	4622
		L2	39604	39900	29977	14360
WIND ON STRUCTURE		W	10	0	25.6	0
STRUCTURE WEIGHT		VS	TO BE DETERMINED BY TAB			
LINEMAN & EQUIP. WEIGHT		V4	500			
JUMPER INSULATOR WEIGHT		V3	215			

* V, T AND L IN POUNDS, W IN PSF (OLF INCLUDED)

SHIELDWIRE

(2) 24 FIBER OPGW (GW2400 - 54mm² / 528)
DIA=0.528", WT=0.362 LBS/FT, RTS=18,432 LBS
1" RADIAL ICE, 15' F MAX TENSION 7833 LBS INITIAL
EVERYDAY COND, 60°F TENSION 2036 LBS INITIAL

PHASE CONDUCTOR

(3) 954.0 KCMIL 45/7 STRAND ACSR "RAIL" (TRIPLE BUNDLED)
DIA=1.165", WT=1.0750 LBS/FT, RTS=25,900 LBS
1" ICE, 15T MAX TENSION 13623 LBS INITIAL (SUB CONDUCT)
EVERYDAY CONDITION, 60T TENSION 4903 LBS INITIAL (SUB CONDUCT)

MECHANICAL LOADING CRITERIA:

CASE 1 - NESC MEDIUM: 4 PSF WIND ON WIRES AND STRUCTURE,
1/4" RADIAL ICE, 15' F. TRANSVERSE WIND OLF=2.50,
LONGITUDINAL OLF=1.65; VERTICAL OLF=1.50.

CASE 2 - HEAVY ICE: 1" RADIAL ICE, NO WIND, 15° F. GLF=1.0

CASE 3 - HIGH WIND: 25.6 PSF WIND ON WIRES AND STRUCTURE,
NO ICE, 60° F, DLF=1.00.

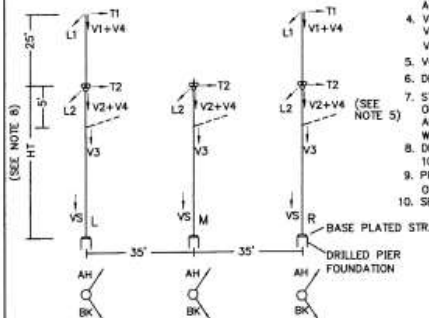
CASE 4 - EVERYDAY: NO WIND, NO ICE, 80° F. OLF=1.0

SPAN DATA:

WIND SPAN = 750 FT (INTACT) 375 FT (DE)
WEIGHT SPAN = 2000 FT (INTACT) 1340 FT (DE)
RULING SPAN = 1000 FT

NOTES:

1. ALL LOADS ARE ULTIMATE LOADS AND INCLUDE OVERLOAD FACTORS PER MECHANICAL LOADING CRITERIA.
2. FOR STRUCTURAL DESIGN, THE LONGITUDINAL (L), TRANSVERSE (T) AND VERTICAL (V) LOADS SHALL BE CONSIDERED TO ACT SIMULTANEOUSLY WITH WIND AND THE DEAD WEIGHT OF THE STRUCTURE.
3. THE TRANSVERSE LOADS (T) INCLUDE WIND ON THE WIRES AND TRANSVERSE (TENSION) LOADS FROM THE LINE ANGLE AT THE STRUCTURE.
4. V1 INCLUDES 50 LBS FOR SHIELDWIRE ASSEMBLY(S).
5. V2 INCLUDES 500 LBS FOR INSULATOR ASSEMBLIES (INTACT)
6. V2 INCLUDES 300 LBS FOR INSULATOR ASSEMBLY, (DE)
7. V4 (LINEMAN-EQUIPMENT) = 500 LBS AT ANY ONE LOCATION.
8. DESIGN STRUCTURE FOR BOTH INTACT & DE ONE SIDE CONDITION.
9. STRUCTURES TO BE DESIGNED TO SUPPORT ANY COMBINATION OF TWO SHIELD WIRES (FIBER OR 747) - ONE PER UPPER LEG. ABOVE TABLE REFLECTS THE LOADINGS DUE TO THE OPGW WHICH CONTROLS THE DESIGN.
10. DESIGN FOR HEIGHTS TO CONDUCTOR FROM 55' TO 115' IN 10' INCREMENTS (OVERALL HT 60' TO 140').
11. PROVIDE SAMPLE DESIGN FOR DIAMETER, THICKNESS, AND OVERLAP FOR EACH STRUCTURE.
12. SEE DRAWING STD-4 FOR STRUCTURE FRAMING.



LOAD TREE 500KV 3-POLE

SLE3-DEPY-S 500 SK4 (25)

ENTERGY SERVICES, INC.

Transmission Line Design Standard
LOAD TREE, DEADEND, 25', SS, 55'-115'
STRUCTURE DRAWING & DETAIL

STD NO.	SCALE: NONE
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No. TFS242A0

LOT	1=1	SH. 1 OF 1
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SLE3-DEPY-S 500; SK4 (25)

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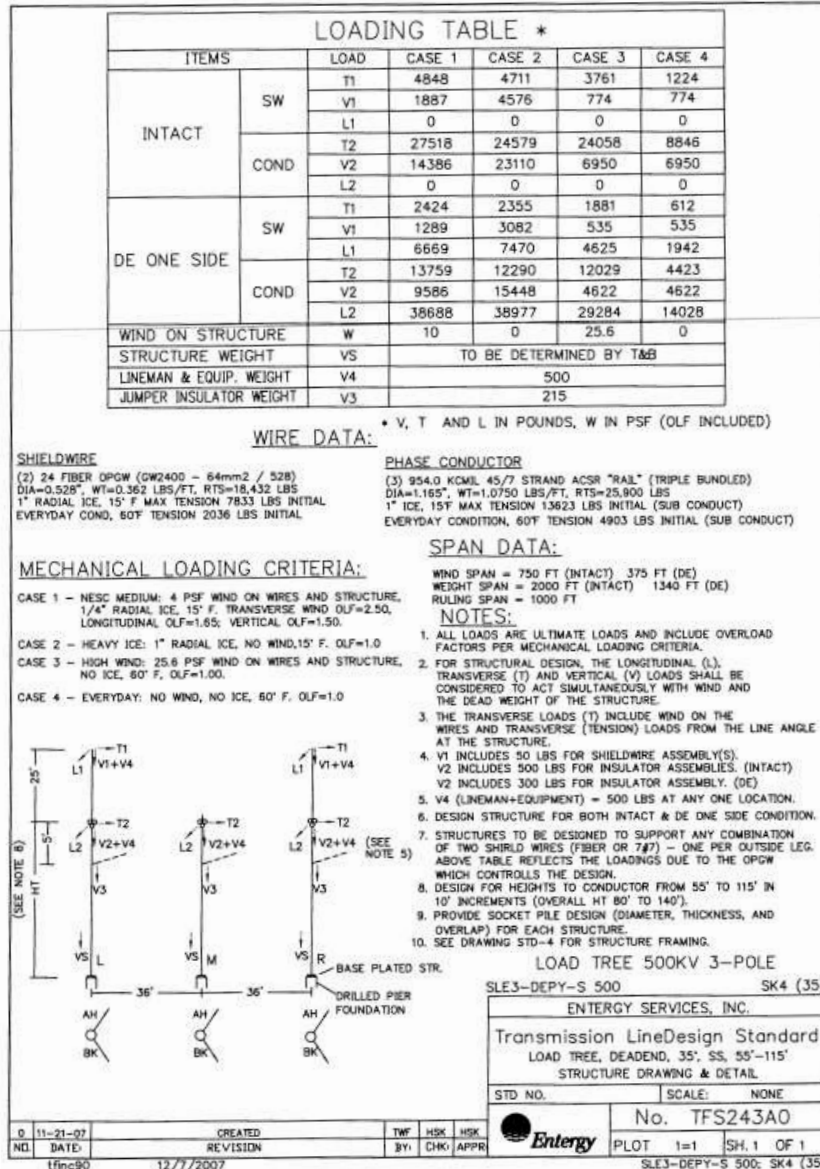
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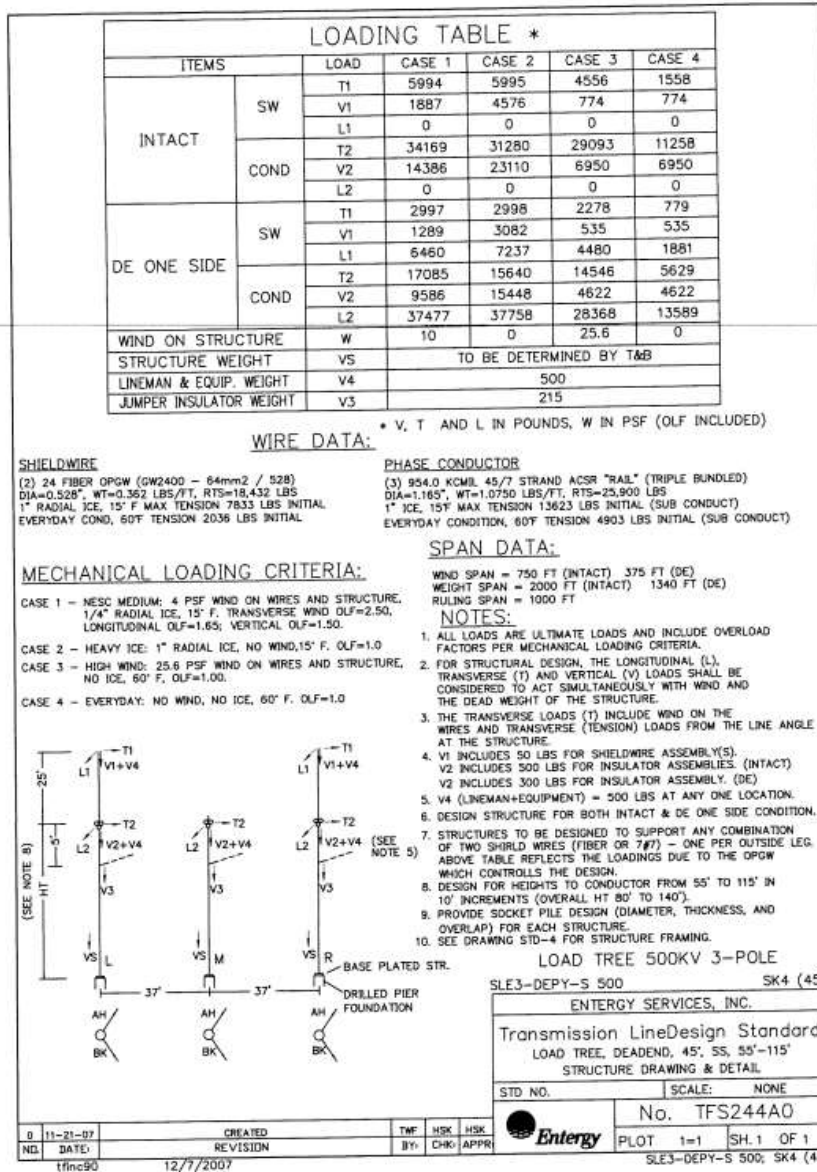
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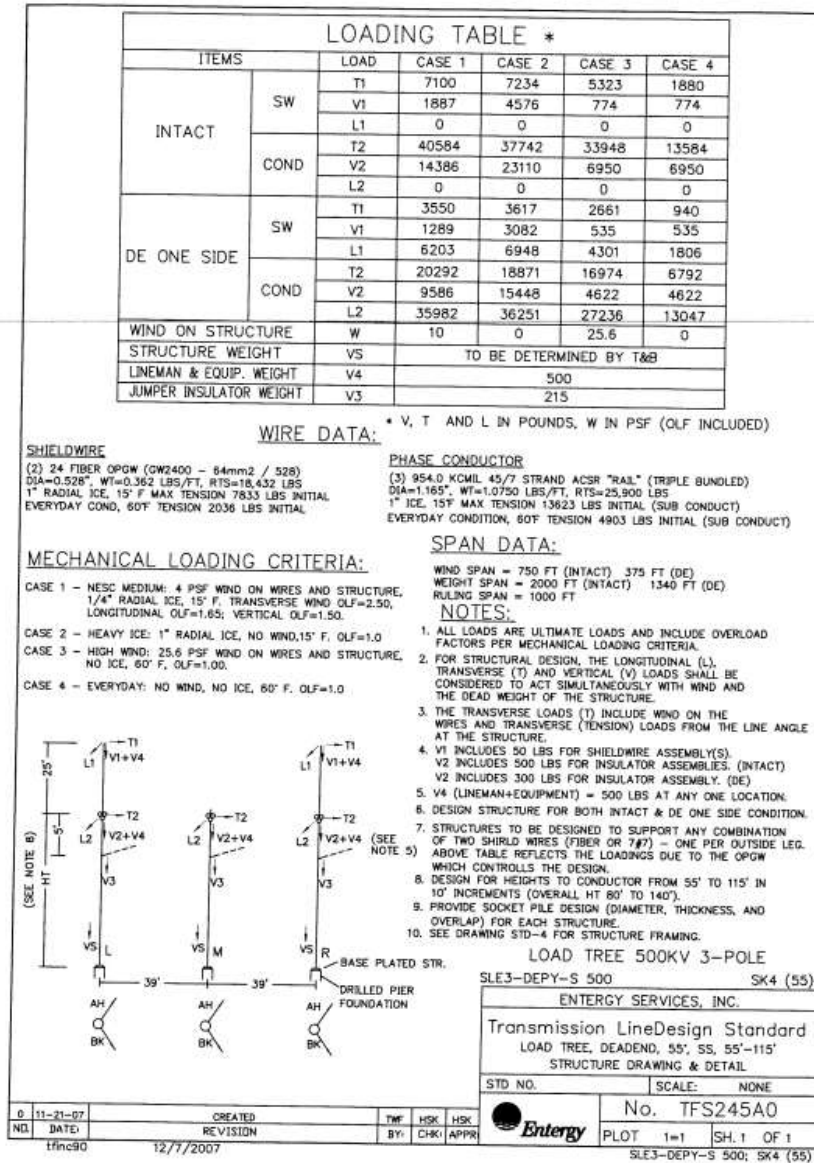
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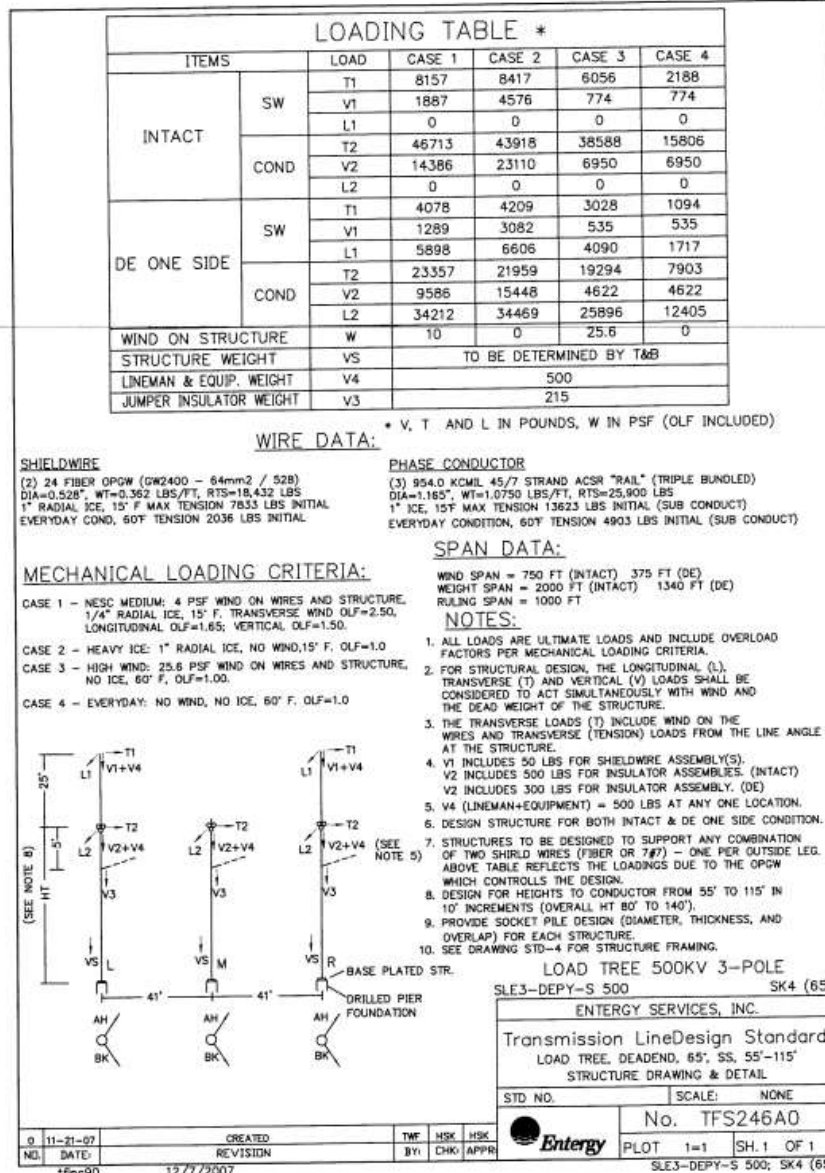
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LOADING TABLE *						
ITEMS		LOAD	CASE 1	CASE 2	CASE 3	CASE 4
INTACT	SW	T1	8664	8986	6407	2336
		V1	1887	4576	774	774
		L1	0	0	0	0
	COND	T2	49656	46883	40815	16873
		V2	14386	23110	6950	6950
		L2	0	0	0	0
DE ONE SIDE	SW	T1	4332	4493	3204	1168
		V1	1289	3082	535	535
		L1	5728	6416	3972	1668
	COND	T2	24828	23441	20408	8437
		V2	9586	15448	4622	4622
		L2	33229	33478	25152	12049
WIND ON STRUCTURE		W	10	0	25.6	0
STRUCTURE WEIGHT		VS	TO BE DETERMINED BY TAB			
LINEMAN & EQUIP. WEIGHT		V3	500			

* V, T AND L IN POUNDS, W IN PSF (OLF INCLUDED)

WIRE DATA:

SHIELDWIRE

(2) 24 FIBER OPGW (GW2400 - 64mm² / 528)
DIA=0.528", WT=0.352 LBS/FT, RTS=18,432 LBS
1" RADIAL ICE, 15' F MAX TENSION 7833 LBS INITIAL
EVERYDAY COND, 60' F TENSION 2036 LBS INITIAL

PHASE CONDUCTOR

(3) 954.0 KCMIL 45/7 STRAND ACSR "RAIL" (TRIPLE BUNDLED)
DIA=1.165", WT=1.0750 LBS/FT, RTS=25,900 LBS
1" ICE, 15' F MAX TENSION 13623 LBS INITIAL (SUB CONDUCT)
EVERYDAY CONDITION, 60' F TENSION 4903 LBS INITIAL (SUB CONDUCT)

SPAN DATA:

WIND SPAN = 750 FT (INTACT) 375 FT (DE)
WEIGHT SPAN = 2000 FT (INTACT) 1340 FT (DE)
RAILING SPAN = 1000 FT

NOTES:

1. ALL LOADS ARE ULTIMATE LOADS AND INCLUDE OVERLOAD FACTORS PER MECHANICAL LOADING CRITERIA.
2. FOR STRUCTURAL DESIGN, THE LONGITUDINAL (L), TRANSVERSE (T) AND VERTICAL (V) LOADS SHALL BE CONSIDERED TO ACT SIMULTANEOUSLY WITH WIND AND THE DEAD WEIGHT OF THE STRUCTURE.
3. THE TRANSVERSE LOADS (T) INCLUDE WIND ON THE WIRES AND TRANSVERSE (TENSION) LOADS FROM THE LINE ANGLE AT THE STRUCTURE.
4. V1 INCLUDES 50 LBS FOR SHIELDWIRE ASSEMBLY(S). V2 INCLUDES 500 LBS FOR INSULATOR ASSEMBLIES. (INTACT) V2 INCLUDES 300 LBS FOR INSULATOR ASSEMBLY. (DE)
5. V3 (LINEMAN+EQUIPMENT) = 500 LBS AT ANY ONE LOCATION.
6. DESIGN STRUCTURE FOR BOTH INTACT & DE ONE SIDE CONDITION.
7. STRUCTURES TO BE DESIGNED TO SUPPORT ANY COMBINATION OF TWO SHIRLO WIRES (FIBER OR 7/7) - ONE PER OUTSIDE LEG. ABOVE TABLE REFLECTS THE LOADINGS DUE TO THE OPGW WHICH CONTROLS THE DESIGN.
8. DESIGN FOR HEIGHTS TO CONDUCTOR FROM 55' TO 115' IN 10' INCREMENTS (OVERALL HT 80' TO 140').
9. PROVIDE SOCKET PILE DESIGN (DIAMETER, THICKNESS, AND OVERLAP) FOR EACH STRUCTURE.
10. SEE DRAWING STD-S FOR STRUCTURE FRAMING.

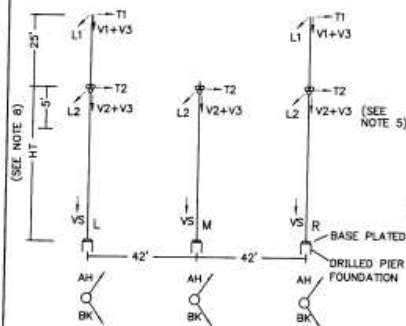
MECHANICAL LOADING CRITERIA:

CASE 1 - MESC MEDIUM: 4 PSF WIND ON WIRES AND STRUCTURE, 1/4" RADIAL ICE, 15' F. TRANSVERSE WIND OLF=2.50, LONGITUDINAL OLF=1.65; VERTICAL OLF=1.50.

CASE 2 - HEAVY ICE: 1" RADIAL ICE, NO WIND, 15' F. OLF=1.0

CASE 3 - HIGH WIND: 25.6 PSF WIND ON WIRES AND STRUCTURE, NO ICE, 60' F. OLF=1.00.

CASE 4 - EVERYDAY: NO WIND, NO ICE, 60' F. OLF=1.0



LOAD TREE 500KV 3-POLE

SLE3-DEPY-S 500 SK5 (70)

ENTERGY SERVICES, INC.

Transmission LineDesign Standard

LOAD TREE, DEADEND, 70', SS, 55'-115'

STRUCTURE DRAWING & DETAIL

STD NO.

SCALE:

NONE

No. TFS247A0



PLOT 1=1 SH. 1 OF 1

SLE3-DEPY-S 500; SK5 (70)

0	11-21-07	CREATED	TWF	HSK	HSK
1	12-7-2007	REVISION	BY:	CHK:	APPR:

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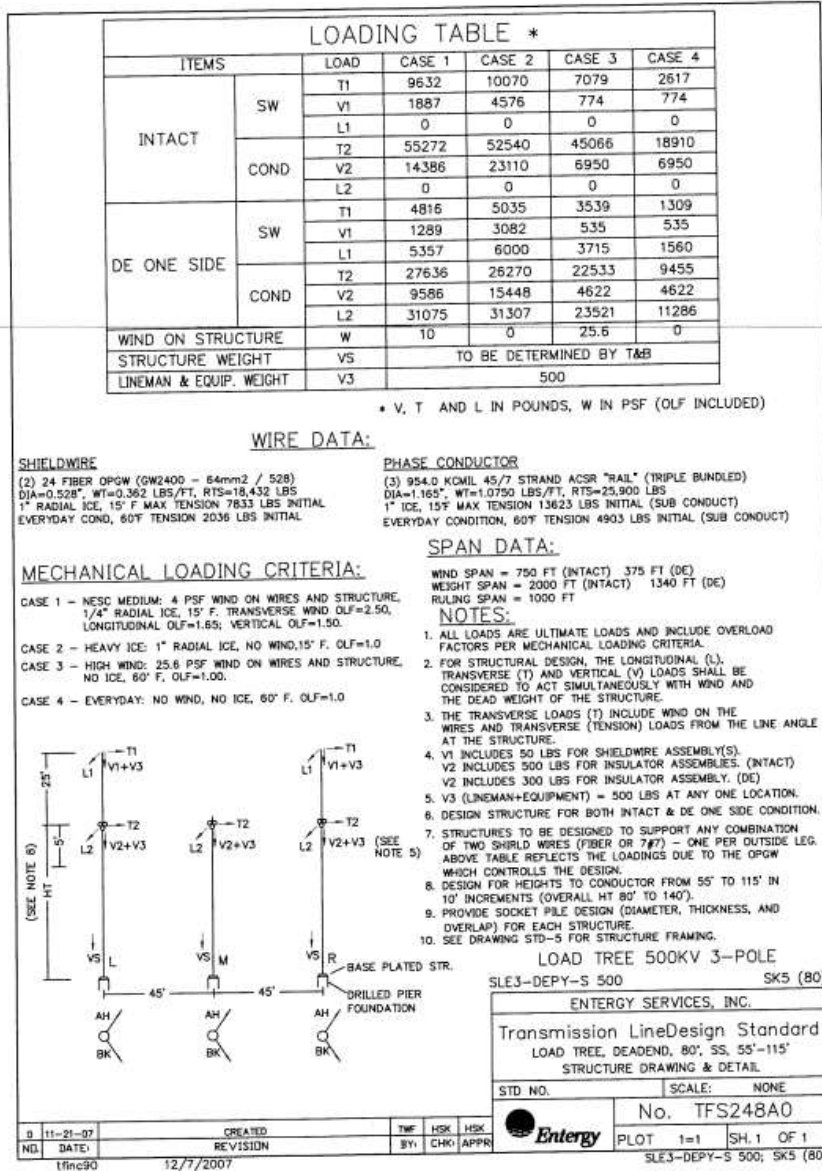
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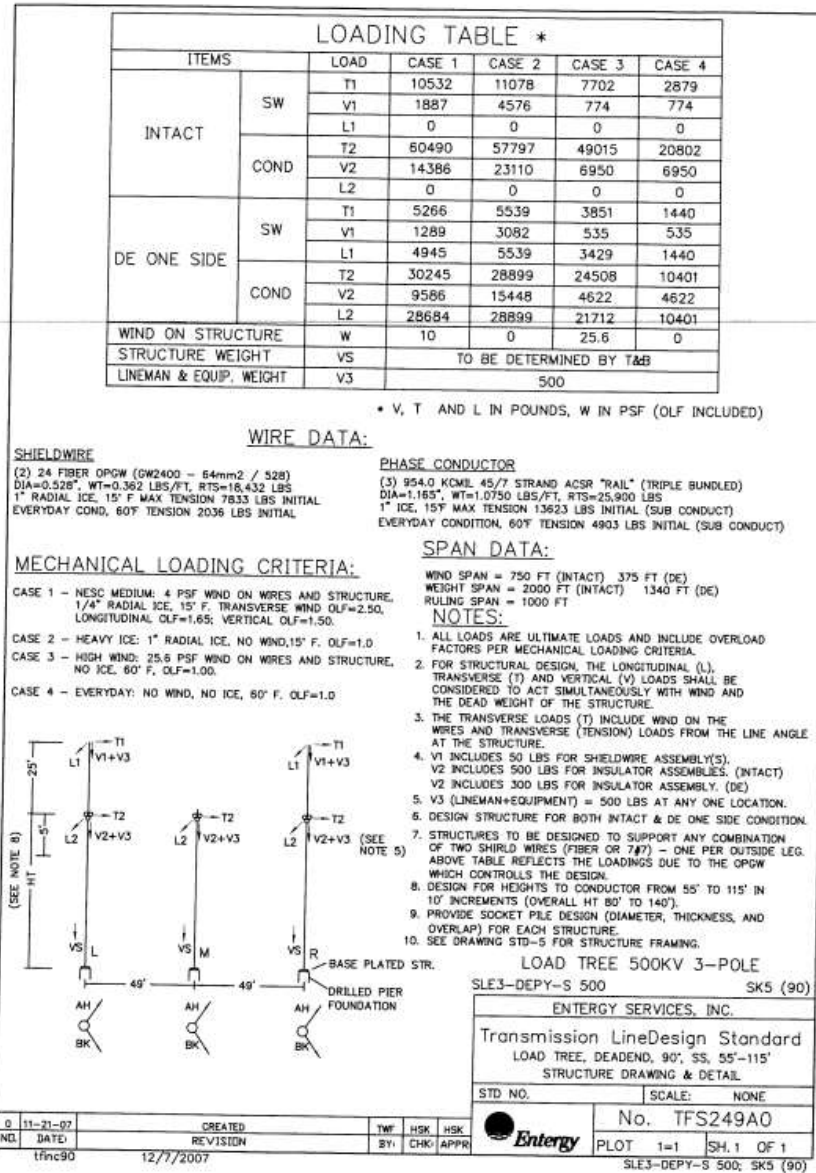
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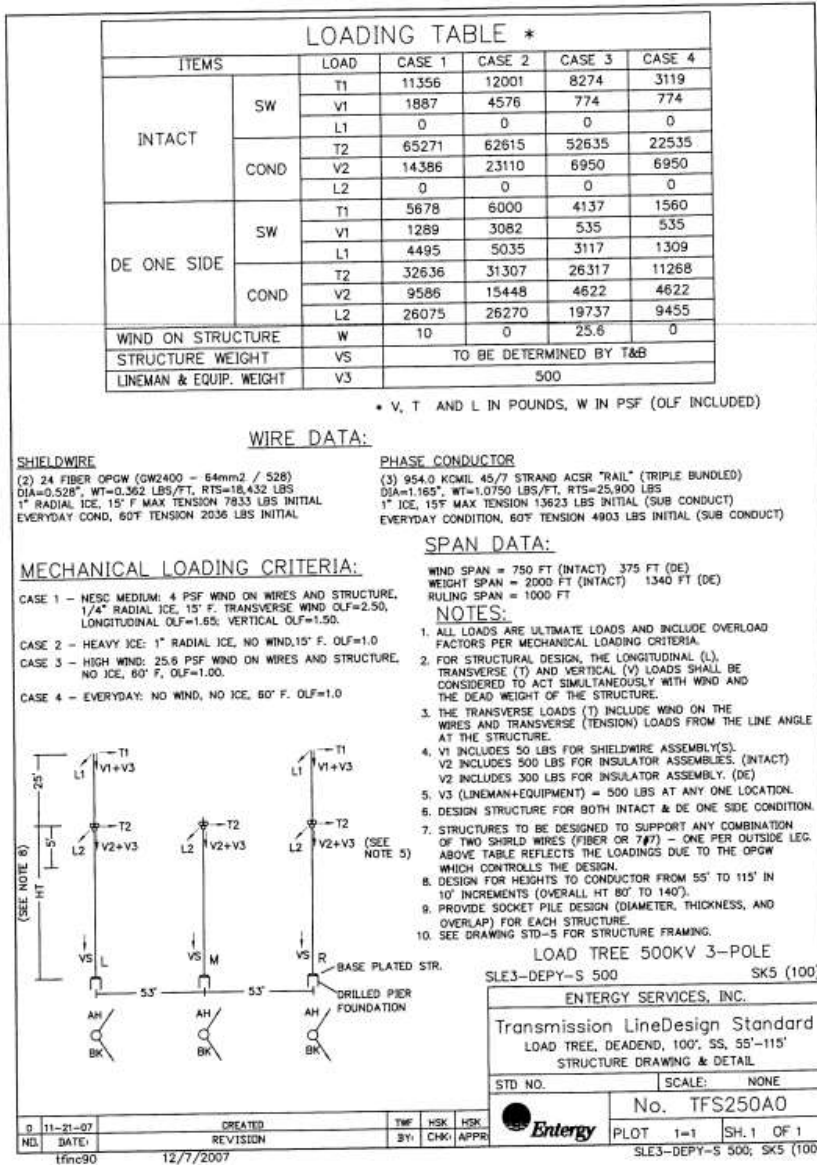
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BILL OF MATERIALS			
VARIABLE BOLT ASSY, DOUBLE POLY POST FOR CONCRETE WITH GROUNDING			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	EN000171	NUT, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
2	1	EN000358	CLIP, BONDING, 7/8", STL, GALV, FOR GROUNDING TO 7/8" BOLT
3	1	EN000362	WIRE, COPPERWELD, #4 (-1158 lbs/TN)
4	8	EN000426	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
5	1	EN000360	CONNECTOR, #4 COPPER CRIMPIT
6	2	LS909XX	BOLT, DOUBLE ARMING, 7/8"xVARIABLE LENGTH, GALV, w/4 SQ NUTS
7	8	EN000685	WASHER, FLAT ROUND, 2" STEEL, GALV, FOR 7/8" BOLT

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

2) Grounding Lug location may be above or below assembly depending on pole tank ground location.

BLT-2P-C	
ENTERGY STANDARD DWG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
BOLT ASSY (CONCRETE) DOUBLE POLYMER POST INS.	
APPROVED BY: E.J.G.	DATE: 01-27-97
CHECKED BY: JWS	SCALE: NONE
DRAWN BY: ECSI	ESI NO. TMD207A1
No. BLT2PC	
PLOT 1=B SH. 1 OF 1	

NO.	DATE	REV.	DIM.	CHANGE	WASHER	FROM	TO	FROM	TO
1	5-28-03	REV.	DIM.	CHANGE	WASHER	FROM	TO	FROM	TO

NO. DATE: REVISION BY: APPR:

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BILL OF MATERIALS			
VARIABLE BOLT ASSY, DOUBLE POLY POST FOR STEEL			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	8	EN000428	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 8 THD
2	8	EN000685	WASHER, FLAT ROUND, 2" STEEL, GALV, FOR 7/8" BOLT
3	2	LS909XX	BOLT, DOUBLE ARMING, 7/8"xVARIABLE LENGTH, GALV, w/4 SQ NUTS

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

BLT-2P-S	
ENTERGY STANDARD DWG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
BOLT ASSY (STEEL) DOUBLE POLYMER POST INS.	
APPROVED BY:	DATE: 2-12-96
CHECKED BY:	SCALE: NONE
DRAWN BY: ECS	ESI NO. TMD208A1
No. BLT2PS	
PLOT 1=8 SH. 1 OF 1	

NO.	DATE:	CHANGE	BY:	APPR:
1	5-28-03	CHANGE WASHER, DIM.	ITRON	

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BILL OF MATERIALS			
VARIABLE BOLT ASSY, SINGLE POLY POST FOR CONCRETE WITH GROUNDING			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	EN000171	NUT, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
2	1	EN000358	CLIP, BONDING, 7/8", STL, GALV, FOR GROUNDING TO 7/8" BOLT
3	1	EN000362	WIRE, COPPERWELD, #4 (.1158 lbs/ft)
4	8	EN000428	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
5	2	EN012280	WASHER, SQUARE CURVED, STL, GALV, 7/8" BOLT, 3"x3"x1/4"
6	1	EN000360	CONNECTOR, #4 COPPER CRIMPIT
7	2	LS909XX	BOLT, DOUBLE ARMING, 7/8"xVARIABLE LENGTH, GALV, w/4 SQ NUTS
8	4	EN005685	WASHER, FLAT ROUND, 2" STEEL, GALV, FOR 7/8" BOLT

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

2) Grounding Lug location may be above or below assembly depending on pole tank ground location.

BLT-P-C	
ENTERGY STANDARD DWG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
BOLT ASSY (CONCRETE) SINGLE POLYMER POST INS.	
APPROVED BY: EJD	DATE: 01-27-97
CHECKED BY: JWS	SCALE: NONE
DRAWN BY: ECSI	ESI NO: TMD211A1
No. BLTPC	
PLOT 1=B SH. 1 OF 1	

1 5-30-03	
NO.	DATE
CHANGE WASHER, DIM.	
REVISION	
BY:	APPR:

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BILL OF MATERIALS			
VARIABLE BOLT ASSY, SINGLE POLY POST FOR STEEL			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	6	EN000426	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
2	6	EN000685	WASHER, FLAT ROUND, 2" STEEL, GALV, FOR 7/8" BOLT
3	2	LS909XX	BOLT, DOUBLE ARMING, 7/8"xVARIABLE LENGTH, GALV, w/4 SQ. NUTS

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

BLT-P-S			
ENTERGY SERVICES, INC.			
Transmission LineDesign Standard			
BOLT ASSEMBLY (STEEL) SINGLE POLYMER POST INS			
STRUCTURAL ASSEMBLY DETAIL			
1	07-21-10	ADDED ASSEMBLY NAME	CRM ECR ECR
2	01-11-10	INCREASED STOCK NO. FROM EN000685 FROM 4 TO 6	BAR
1	05-30-03	CHANGE WASHER, DIM.	IRON
0	02-12-04	ISSUED	ECN
NO	DATE	REVISION	BY: CHK: APPR:
00000000	8/11/2010		

ENTERGY
PLOT SH. OF

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BILL OF MATERIALS			
OHGW DEADEND			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	2	EN000492	SHACKLE, ANCHOR, 40K ULT, 3/4" PIN DIA, 2-3/4" LONG
2	1	LS9004XX	TERMINAL CONNECTOR, 15 DEG, FOR VARIABLE SIZE WIRE
3	1	LS9005XX	DEADEND, ALUMINUM COMPRESSION BODY, SINGLE TONGUE, VARIABLE WIRE SIZE
4	-	LS5012XX	CONNECTOR, AMPACT, SEE GND ASSEMBLY DRAWING FOR MATERIAL ALTERNATE FOR BOLTED ASSEMBLY
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	2	EN000492	SHACKLE, ANCHOR, 40K ULT, 3/4" PIN DIA, 2-3/4" LONG
4	-	LS5012XX	CONNECTOR, AMPACT, SEE GND ASSEMBLY DRAWING FOR MATERIAL
5	1	LS913XX	DEADEND BOLTED STRAIN ALUMINUM
6	1	LS5012XX	CONNECTOR, AMPACT, VARIABLE CONDUCTOR SIZE TO VARIABLE CONDUCTOR SIZE
7	1	EN000390	LINK, CHAIN, XMSN, CONNECTING, CS, 1/2" PITCH, 2 1/4" LONG

FOR GROUNDING DETAIL AND MATERIALS SEE DWG. GND-XX.

See note 2

ALTERNATE PARTS
No. (LS913XX) deadend clamp
No. (LS5012XX) ampack connector

1) Item #2, #3 and #6 are conductor dependent.
2) For grounding detail and materials, see applicable Gnd-xx drawing.
3) For horizontal vane orientation, omit one of item 1.

OHG-DE-XX			
ENTERGY SERVICES, INC.			
Transmission LineDesign Standard			
OVERHEAD GROUNDWIRE DEADEND ASSY			
STRUCTURAL ASSEMBLY DETAIL			
REV	DATE	DESCRIPTION	BY
1	07-21-10	SHOW ITEM 4 ON ASSEMBLY	CEM
2	08-15-08	REVISED ITEM #4	RA
3	01-31-02	MODIFIED STOCK NUMBER LS9002XX	LS
4	01-04-01	MODIFIED CALLOUTS	LS
5	04-07-00	MODIFIED STOCK NUMBER LS9012XX	RMR
6	11-16-99	ADDED AMPACT & CARTRIDGE DESCRIPTION	RMR
7		ISSUED	ECB
8		REVISION	BF

NO. TMD222A6

SCALE: NONE

1=8 SH.1 OF 1

8/15/2006

OHG-DE-XX

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BILL OF MATERIALS			
OHGW SUSPENSION, 0-30"			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	EN004375	BALL CLEVIS, 45 DEG Y, 30K ULT, 3/4" PIN DIA
2	1	LS9003XX	ROD, ARMOR, PREFORMED ALUMINUM, VARIABLE CONDUCTOR SIZE
3	1	LS9008XX	CLAMP, SUSPENSION, ALUMINUM, VARIABLE WIRE SIZE, #/SOCKET EYE
4	-	LS5012XX	CONNECTOR, IMPACT

1) Item #2 and #3 are conductor dependent. These items are selected for each project and may be with or without Armor Rod.

2) For grounding detail and materials see applicable GND-XX drawing.

OHG-SUS-XX			
ENTERGY STANDARD OHG.			
DESIGN APPROVAL		STANDARDS APPROVAL	
SIGNED / DATE	SIGNED / DATE	SIGNED / DATE	SIGNED / DATE
OVERHEAD GROUNDWIRE SUSPENSION ASSY			
APPROVED BY:		DATE: 2-15-03	
CHECKED BY:		SCALE: NONE	
DRAWN BY: JTRON		ESI NO. TMD223A9	
No. OHGSUS		PLT: 1-8 SH. 1 OF 1	

NO.	DATE	REVISION	BY	APPR.
9	8-15-06	REMOVED OPTGW OPTION, DELETED ITEM #4	RAL	
8	12-9-03	ADDED BACK GROUNDING DETAILS	JTRON	
7	5-20-03	ADDED OPTGW OPTION	JTRON	
6	2-17-03	ADDED POLE CAP AND GROUNDING NOTE 2	JTRON	
5	10-15-02	REMOVE GROUNDING DETAIL	JTRON	
4	1-18-02	MODIFIED ITEMS 1, 2 AND 3.	LSFT	
3	1-29-01	MODIFIED STOCK NUMBER LS9007XX	LSFT	
2	1-29-01	MODIFIED STOCK NUMBER LS5012XX	RMB	

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BILL OF MATERIALS			
OHGW SUSPENSION, 30'-50' WITH YOKE PLATE			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	2	EN000482	SHACKLE, ANCHOR, 40K ULT, 3/4" PIN DIA, 2-3/4" LONG
2	2	EN004375	BALL CLEVIS, 45 DEG Y, 30K ULT, 3/4" PIN DIA
3	1	EN015676	PLATE, YOKE, DUCTILE IRON, 18" WIDTH, 30K ULT, 3/4" GALV
4	1	LS9003XX	ROD, ARMOR, PREFORMED, ALUMINUM, VARIABLE CONDUCTOR SIZE
5	2	LS9007XX	CLAMP, SUSPENSION, ALUMINUM, VARIABLE SIZE WIRE, W/SOCKET EYE
6	-	LS5012XX	CONNECTOR, IMPACT, SEE GROUND ASSEMBLY DRAWING FOR MATERIAL

PLAN

DETAIL A
YOKE ASSEMBLY

1) ITEM #4 AND #5 ARE CONDUCTOR DEPENDENT. THESE ITEMS ARE SELECTED FOR EACH PROJECT AND MAY BE WITH OR WITHOUT ARMOR ROD.

2) FOR GROUNDING DETAIL AND MATERIALS SEE APPLICABLE GND-XX DRAWING.

OHG-SUY-XX		
ENTERGY STANDARD DWG.		
DESIGN APPROVAL	STANDARDS APPROVAL	
SIGNED / DATE	SIGNED / DATE	
OVERHEAD GROUNDWIRE HEAVY ANGLE ASSY		
APPROVED BY:	DATE:	1-29-01
CHECKED BY:	SCALE:	NONE
DRAWN BY: ECSE	ESI NO.	TMD224A6
No. OHGSUY		
PLT:	1=16	SH. 1 OF 1

NO.	DATE	REVISION	BY	APPR.
6	8-15-06	REVISED ITEM #6		
5	12-8-03	ADDED BACK GROUNDING DETAILS	ITRON	
4	2-18-03	ADDED POLE CAP AND GROUNDING NOTE	ITRON	
3	1-29-01	MODIFIED STOCK NUMBER LS9007XX	LS	
2	9-7-00	MODIFIED STOCK NUMBER LS5012XX	RMB	
1	11-16-99	ADDED IMPACT & CARTRIDGE DESCRIPTION	RMB	

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BILL OF MATERIALS			
TEE ASSY, BRACE POST FOR STEEL WITH BOLTS			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	EN000171	NUT, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
2	4	EN000429	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
3	2	EN003796	WASHER, SQUARE, CURVED, STL, GALV, ANSI-C135.1, 7/8" BOLT, 1/4" THK, 4"x4"
4	1	EN011909	PLATE, POLE EYE, GALV STL, DBL EYE, 70K ULT, 8" BOLT SPACING
5	2	LS909XX	BOLT, DOUBLE ARMING, 7/8"xVARIABLE LENGTH, GALV, w/4 SQ NUTS

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

2) Grounding Lug location may be above or below assembly depending on pole tank ground location.

TEE-B-S	
ENTERGY STANDARD DWG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
TEE ASSY (STEEL) BRACE	
APPROVED BY: E.J.G.	DATE: 12-19-00
CHECKED BY: JWS	SCALE: NONE
DRAWN BY: ECS	ESI NO. TMD279AD
No. TBS	
PLOT 1=8 SH. 1 OF 1	

NO. DATE: REVISION BY: APPR:

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BILL OF MATERIALS			
TEE ASSY, BRACE TO BRACE FOR STEEL WITH BOLTS			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	EN000171	NUT, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
2	4	EN000426	NUT, LOCK, SQUARE, STL, GALV, ANSI-C135.1, 7/8" DIA, 9 THD
3	2	EN011809	PLATE, POLE EYE, GALV STL, DBL EYE, 70K ULT, 8" BOLT SPACING
4	2	L5909XX	BOLT, DBL ARMING, 7/8"xVARIABLE LENGTH, GALV, #4 SQ NUTS

1) All Double Arming Bolts shall be trimmed to avoid conflict with guys, grounding, conductors, etc. and painted with galvanized paint.

2) Grounding Lug location may be above or below assembly depending on pole tank ground location.

TEE-B-B-S	
ENTERGY STANDARD DWG.	
DESIGN APPROVAL	STANDARDS APPROVAL
SIGNED / DATE	SIGNED / DATE
TEE ASSY (STEEL) BRACE - BRACE	
APPROVED BY: EJS	DATE: 12-19-00
CHECKED BY: JWS	SCALE: NONE
DRAWN BY: ECS	ESI NO. TMD280AD
No. TBBS	
PLOT 1=8 SH. 1 OF 1	

NO.	DATE:	REVISION	BY:	APPR:

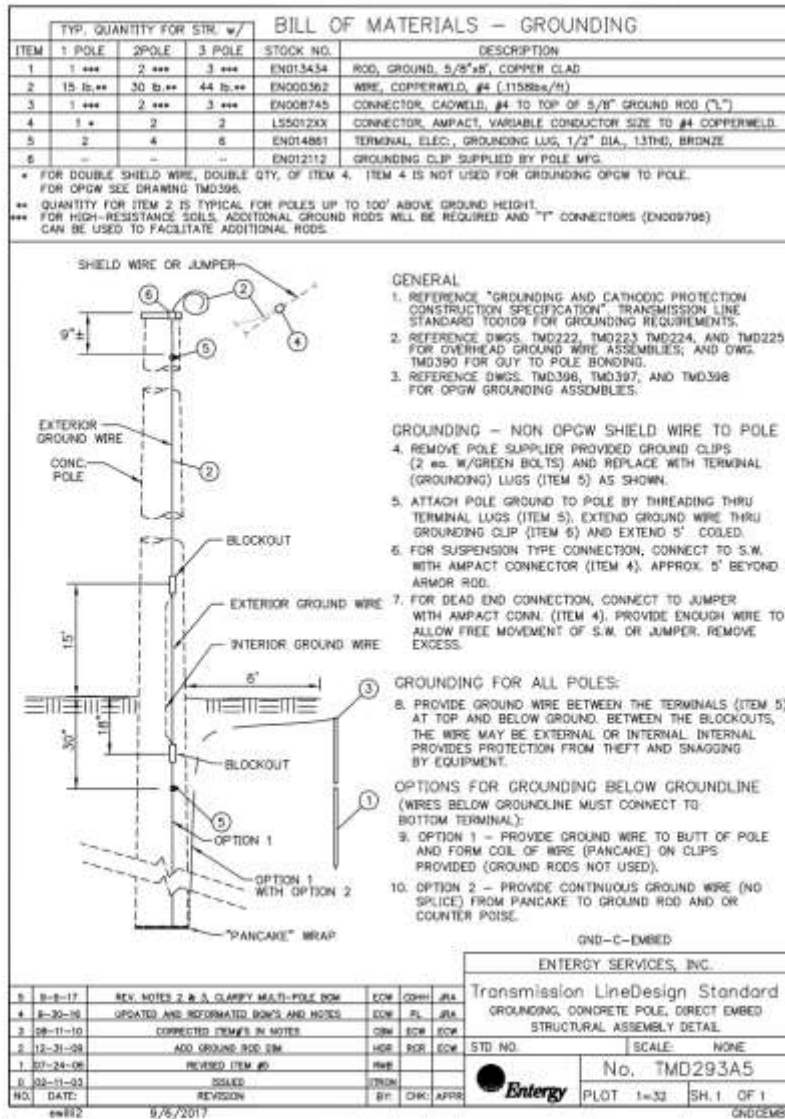
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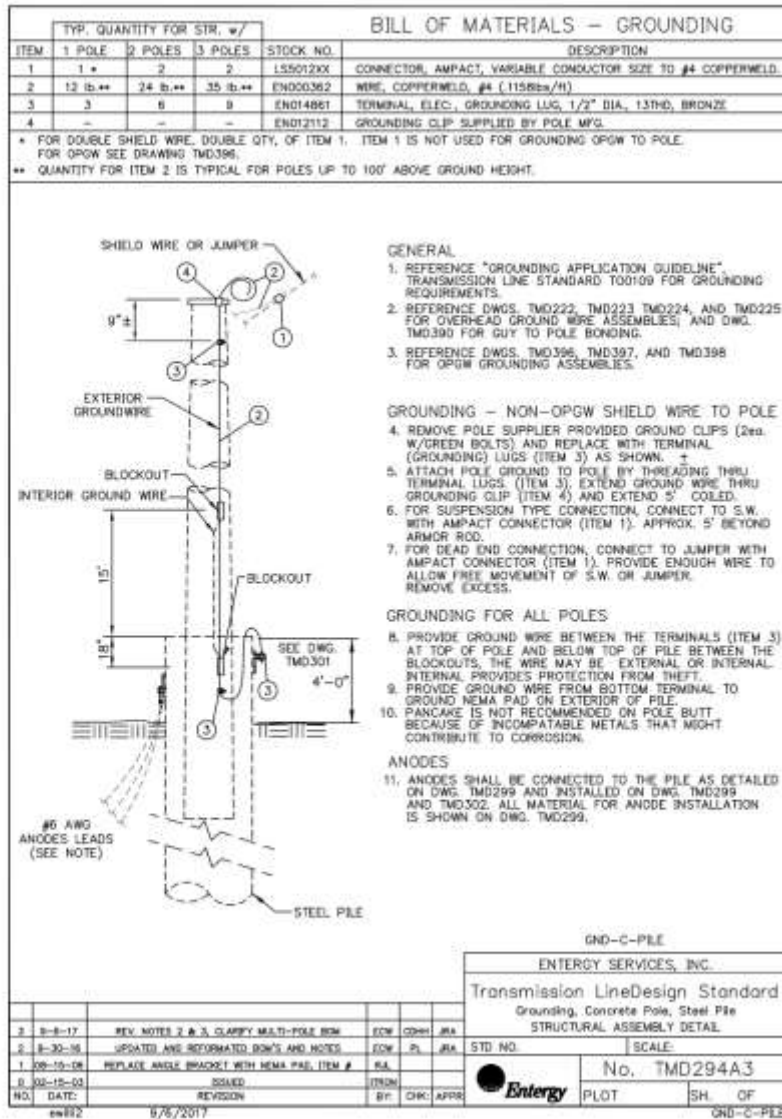
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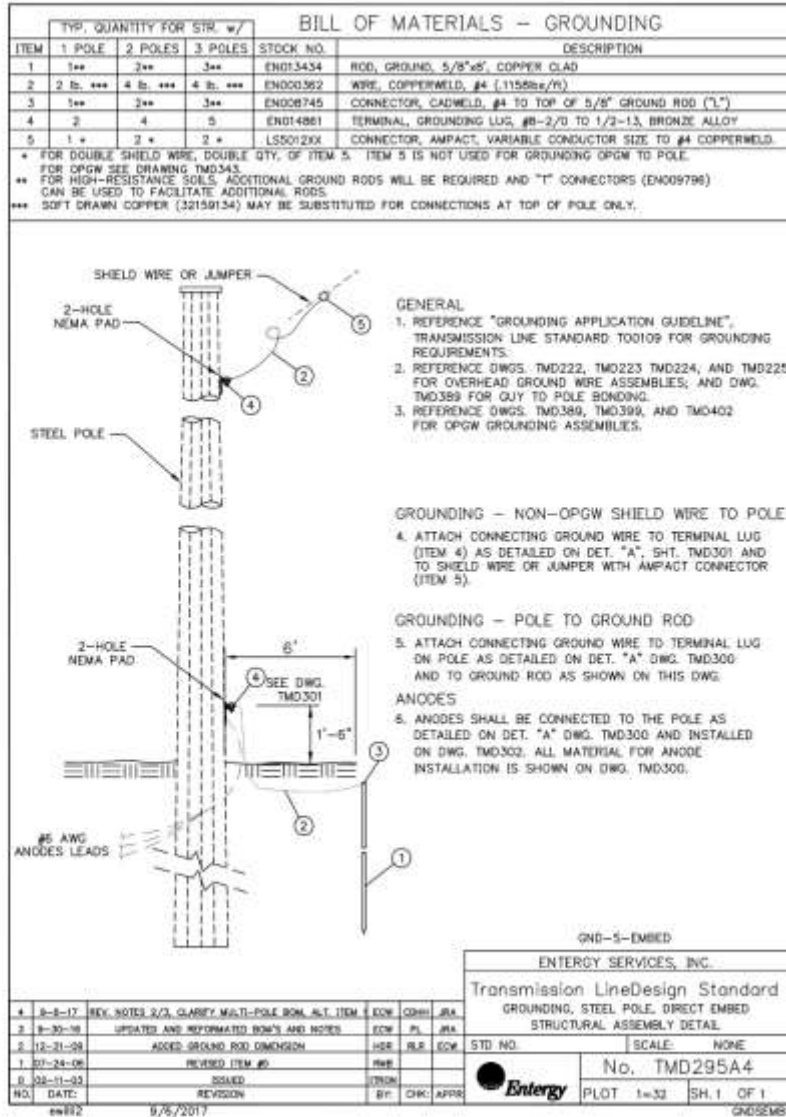
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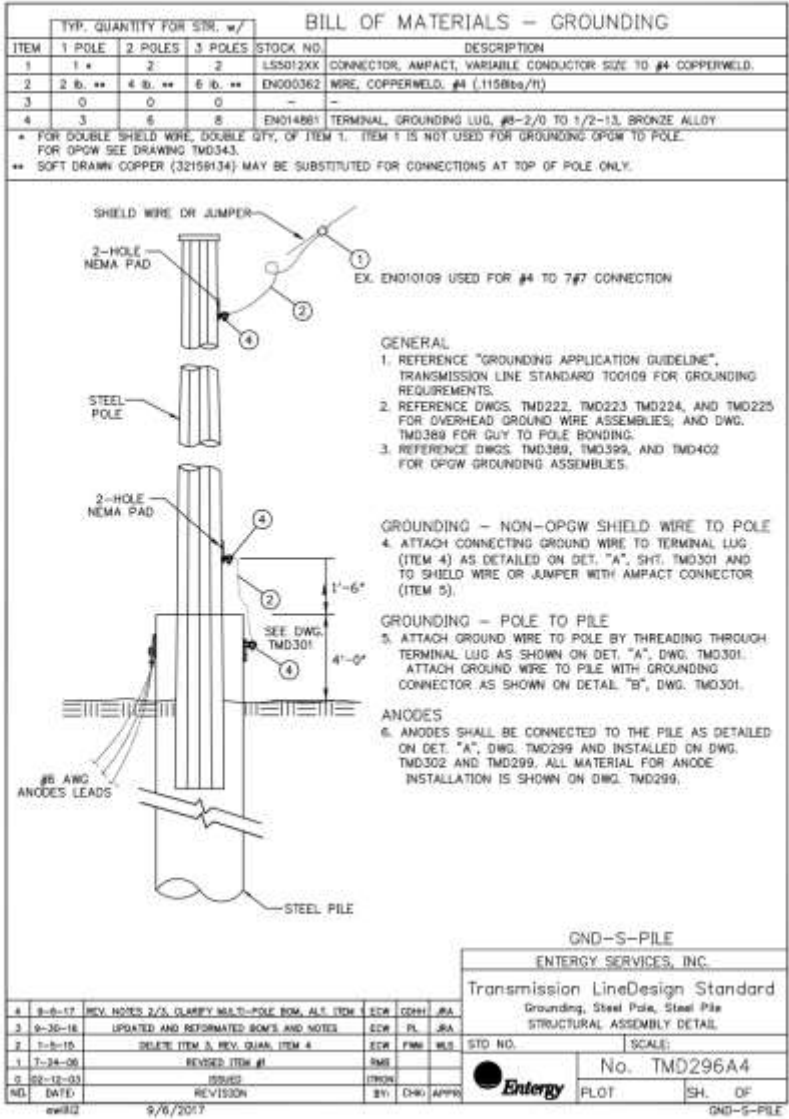
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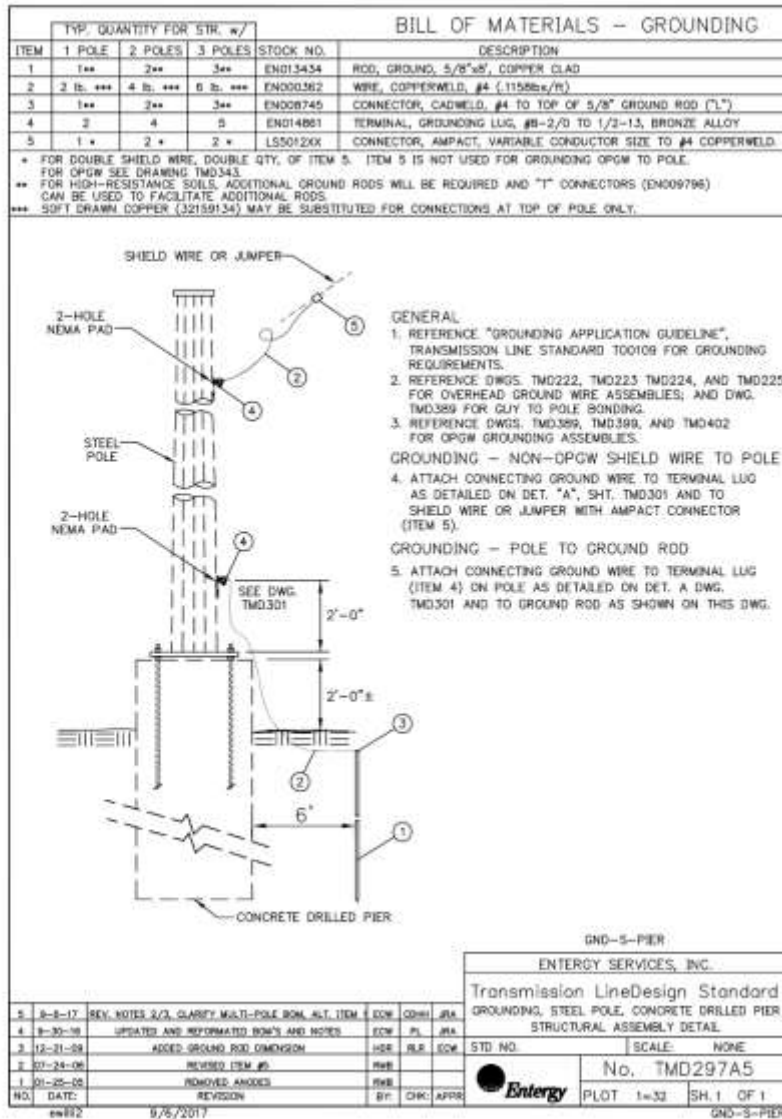
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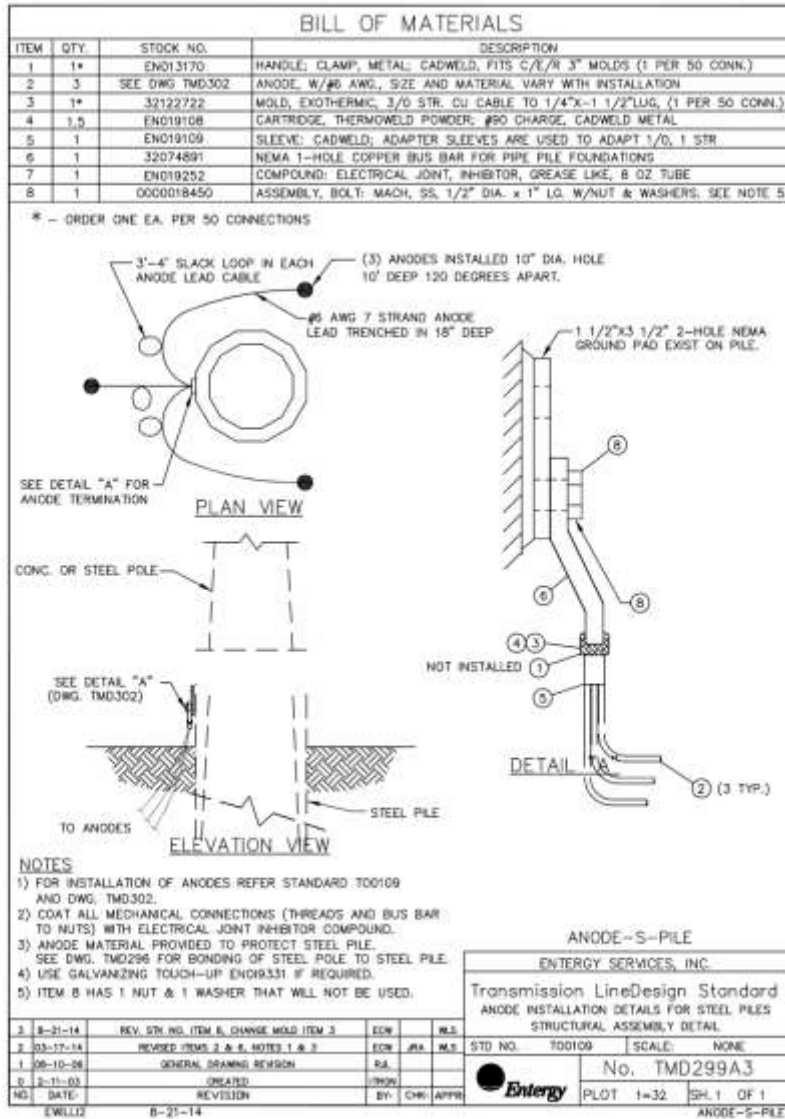
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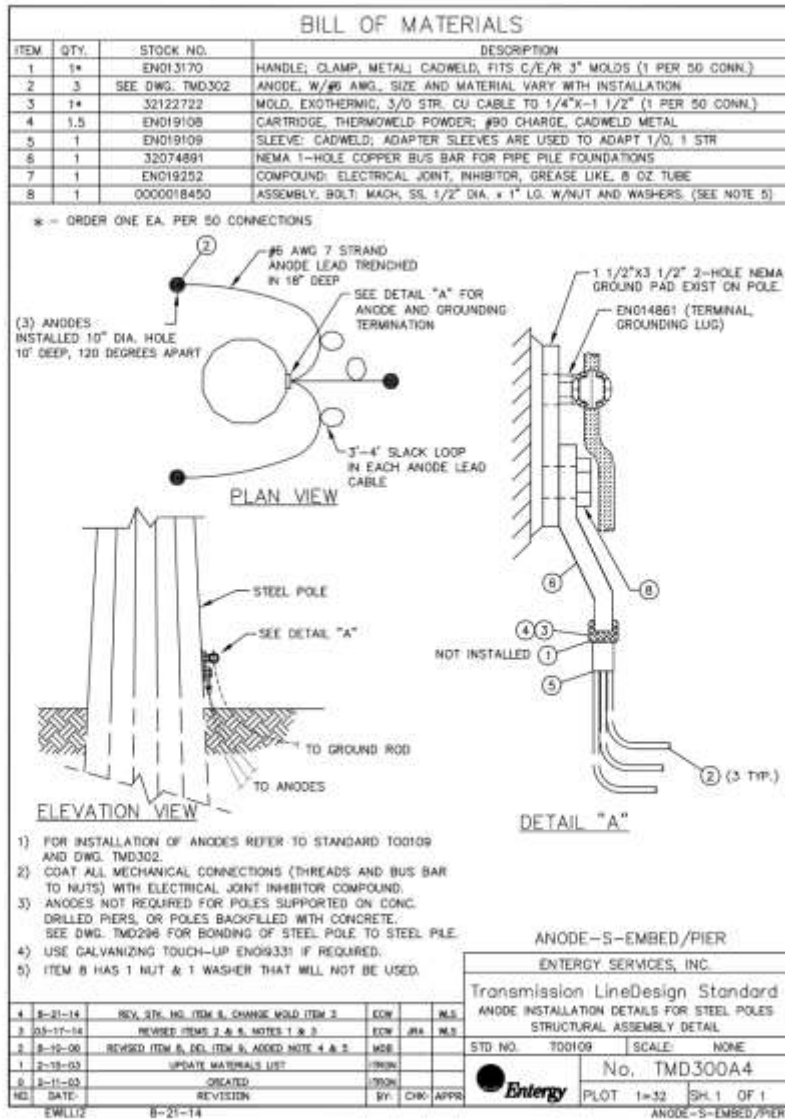
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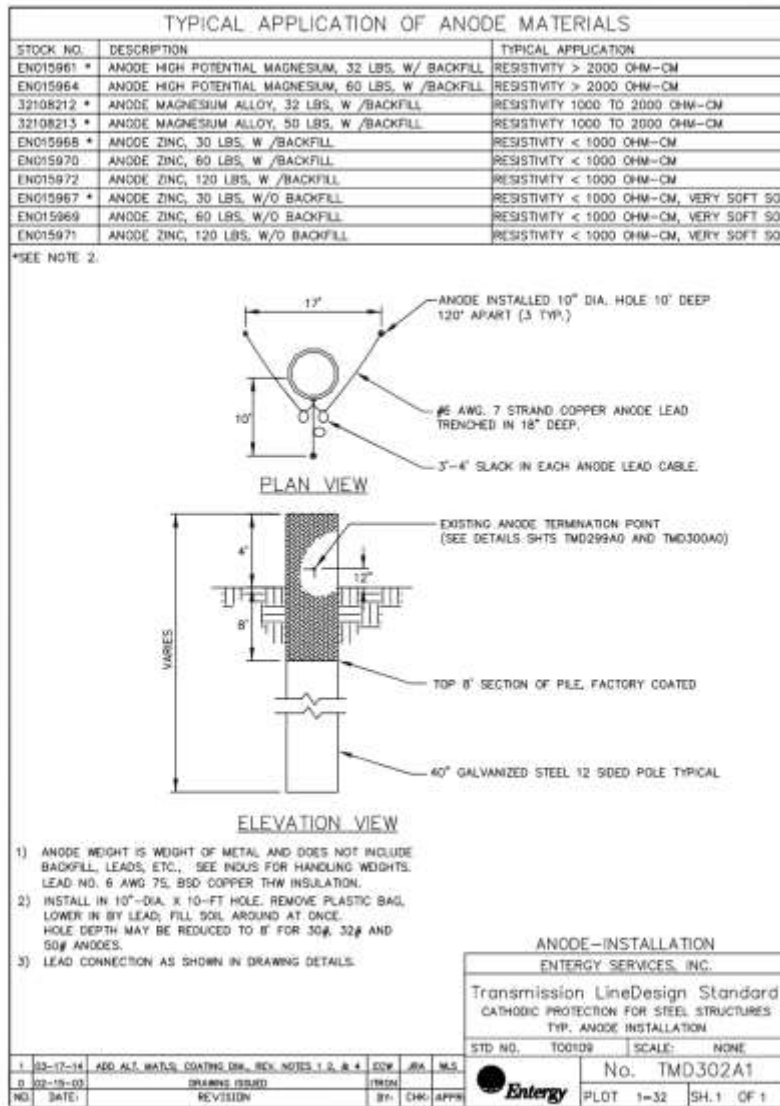
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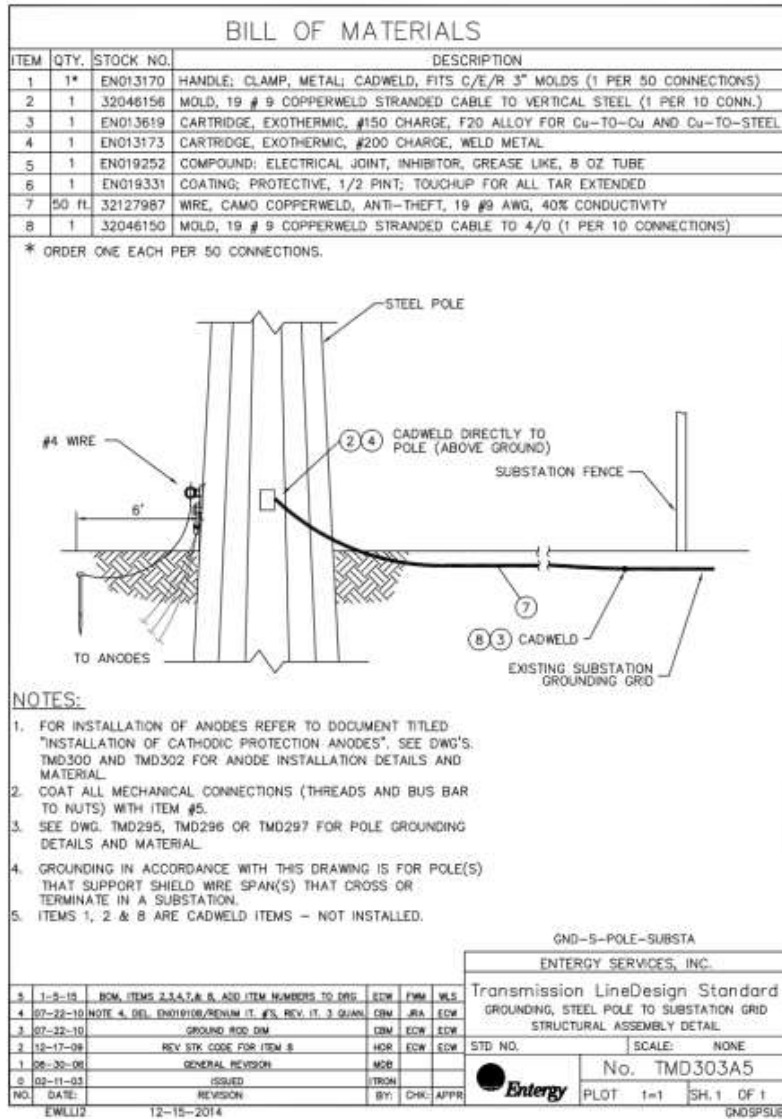
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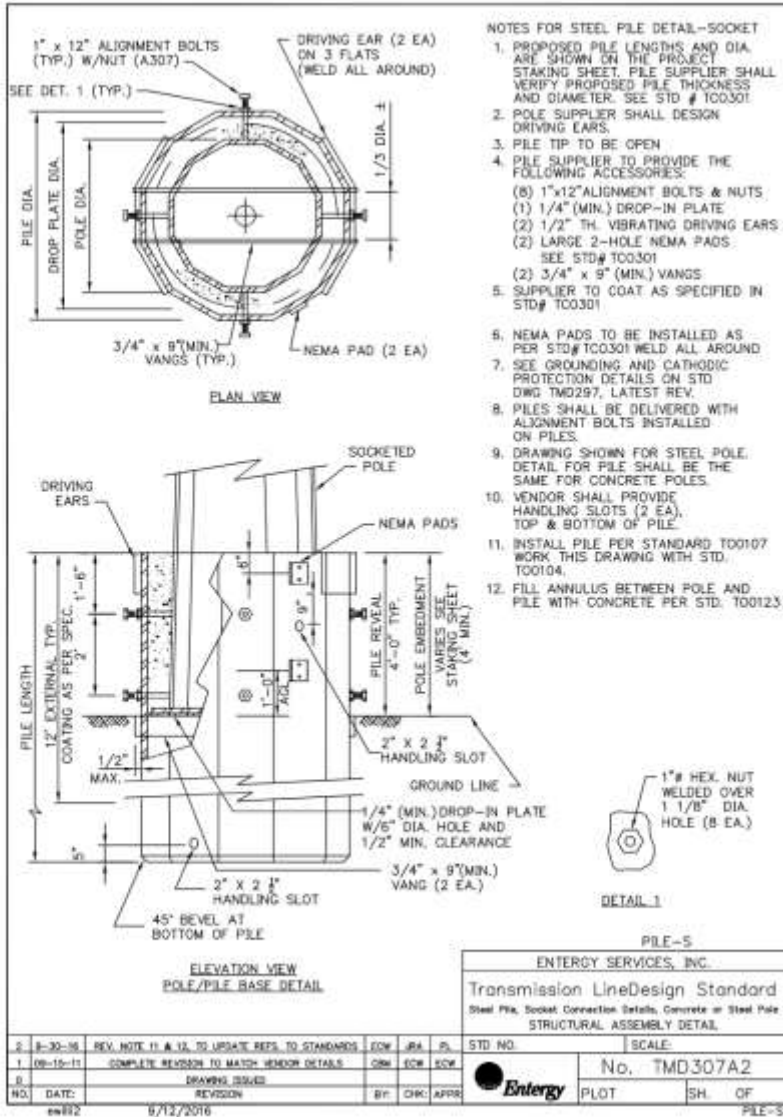
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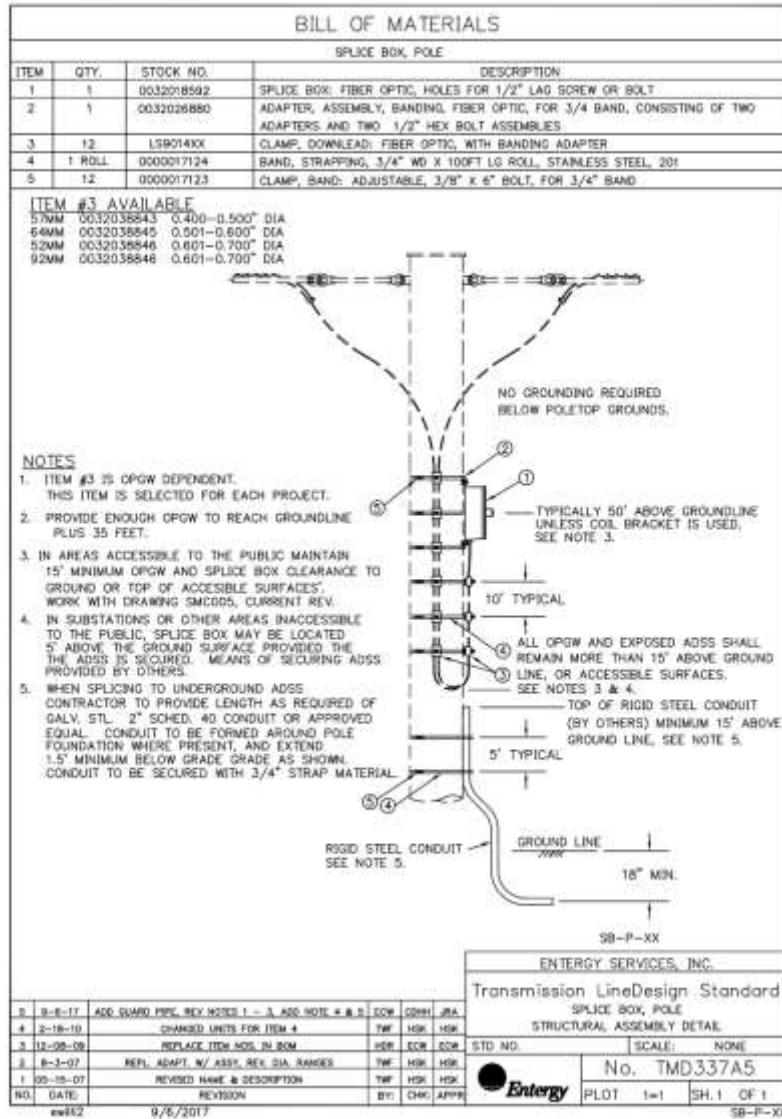
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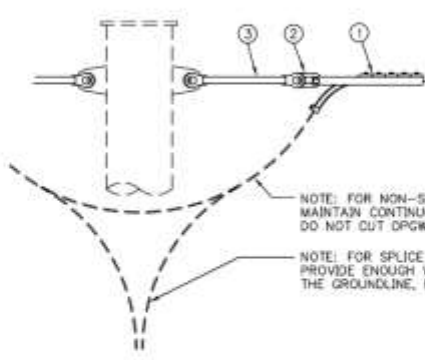
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BILL OF MATERIALS			
OVERHEAD GROUND WIRE, DEADEND, OPGW POLE			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	LS9011XX	DEADEND BOLTED STRAIN, OPGW, 3/4" PIN DIA.
2	1	0000012586	LINK, CHAIN: 5/8" X 3-1/4", 40K
3	1	0000024787	CLEVIS CLEVIS: Y-Y, 30K, 3/4" PD, 15" LONG

NOTE: ILLUSTRATED AS TANGENT OR SMALL ANGLE STRUCTURE. LARGER ANGLES WILL HAVE THE PULLOFFS AT DIFFERENT ELEVATIONS BY SEVERAL INCHES.



NOTE: FOR NON-SPLICE BOX LOCATIONS, MAINTAIN CONTINUOUS LOOP AND DO NOT CUT OPGW.

NOTE: FOR SPLICE BOX LOCATIONS, PROVIDE ENOUGH WIRE TO REACH THE GROUNDLINE, PLUS 15 FEET.

ITEM #1 AVAILABLE:

57MM	0000018531	0.465" DIA
64MM	0032018594	0.528" DIA
52MM	0032018595	0.646" DIA
92MM	0032018596	0.671" DIA

1) ITEM #1 IS OPGW DEPENDENT.
THIS ITEM IS SELECTED FOR EACH PROJECT.

OHG-DE-OP-P-XX

ENTERGY SERVICES, INC.

Transmission LineDesign Standard
OVERHEAD GROUNDWIRE, DE. OPGW POLE
STRUCTURAL ASSEMBLY DETAIL

2	5-13-07	REVISED NOTES, NAME & DESCRIPTION	TWF	HSK	HSK	STD NO.	SCALE: NONE
1	8-23-06	UPDATED BILL OF MATERIAL	R.L.	HSK	HSK		
0	X	CREATED		HSK	HSK		
NO	DATE:	REVISION	BP	CHK	APPR		

11/11/2007 6/25/2007

Entertry

No. TMD339A2

PLOT 1:1 SH.1 OF 1

OHG-DE-OP-P-XX

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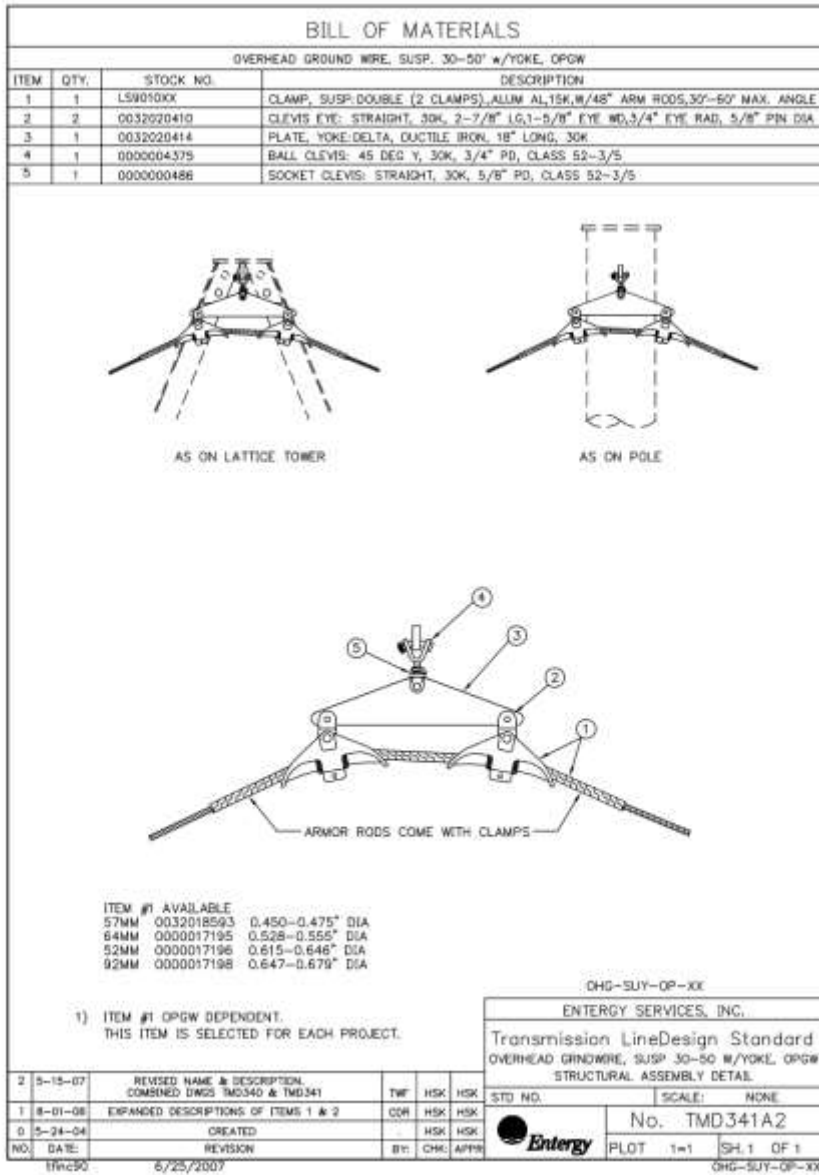
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Attachment 1: Applicable Standard Framing and Assembly Drawings

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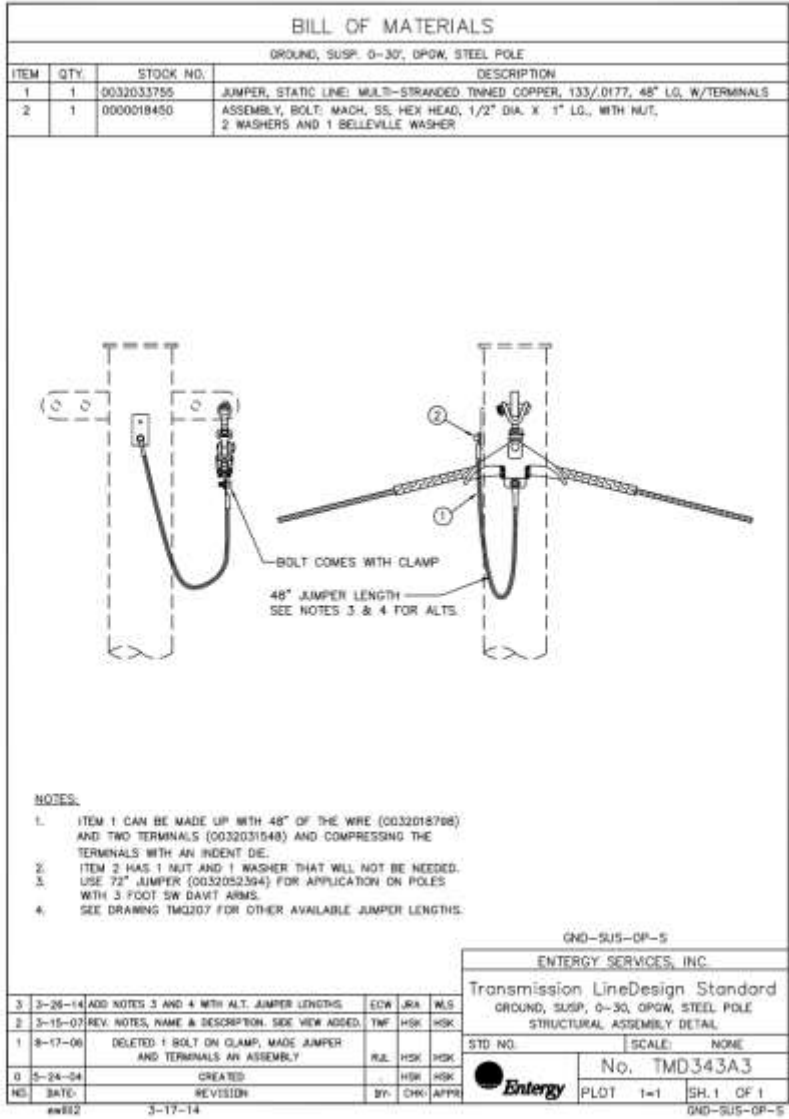
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BILL OF MATERIALS				
COIL BRACKET, OPGW, STEEL POLE				
ITEM	QTY.	STOCK NO.	DESCRIPTION	
1	1	0032031230	BRACKET, COIL: 60 INCH, GALV. STEEL, PER ENTERGY DWG TMM060A	
2	2	—	BOLT, MACHINE, 1/2"-13 X 1", ALL THREAD, GALV. STEEL, NO NUT, NO WASHER (ANY SUPPLIER)	
3	0	0000000139	BOLT ASSEMBLY, MACHINE: HEX HEAD, GALV. STEEL, 5/8"-11 X 1-1/2", WITH HEX NUT	
4	0	0000005532	WASHER, ROUND, FLAT, 11/16" ID, 1-1/2" OD, 1/8" THICK, ASTM A153, GALV. STEEL	
5	0	0032031232	PLATE, BENT, GALV. STEEL, PER ENTERGY DWG. TMM061A	

NOTE #1: ASSEMBLY WILL TYPICALLY BE Banded TO POLE USING 3/4" SS BAND MATERIAL AND ADAPTERS SUPPLIED WITH THE SPLICE BOX. ALTERNATELY, THE COIL BRACKET ASSEMBLY MAY BE SECURED WITH TWO 1/2" BOLTS (ITEM 2) USING ANY TWO OF THE FOUR THREADED RECEIVER PROVIDED.

NOTE #2: TWO EACH OF ITEMS 3 AND 5, AND FOUR OF ITEM 4 MAY ALSO BE USED TO SECURE THE COIL BRACKET ASSEMBLY TO POLES ALREADY IN SERVICE THAT WERE MANUFACTURED WITH STEP CLIPS. THE STEP CLIP DETAIL IS COMMON ON OLDER POLES MANUFACTURED BY THOMAS & BETTS.

NOTE #3: COIL BRACKET ASSEMBLY CAN BE INSTALLED WITH EITHER END UP. BEFORE TIGHTENING BOLTS, BE SURE THAT WEIGHT OF COMPONENTS PULLS THEM FIRMLY INTO SLOTTED HOLES IN THE CHANNEL.

NOTE #4: THE LOWEST PART OF THE INSTALLATION MUST BE A MINIMUM OF 15 FEET ABOVE GROUNDLINE AND THE CABLE MUST COME INTO THE BOTTOM OF THE SPLICE BOX WITH NO STRAIN ON THE CONNECTORS. ADDITIONAL BANDING MAY BE NECESSARY TO GATHER AND STABILIZE THE EXCESS CABLE LENGTH TO THE BRACKET AND POLE. HOLES ARE PROVIDED IN THE END OF EACH ARM TO ACCOMMODATE CABLE TIES OR WIRE TIES.

15' MINIMUM ABOVE GL. IF ALTERNATE SPLICE BOX LOCATION IS USED, NO PART OF INSTALLATION CAN BE LOWER THAN 15' ABOVE THE GROUND LINE.

CB-OP-S				
ENTERGY SERVICES, INC.				
Transmission LineDesign Standard				
COIL BRACKET, OPGW, STEEL POLE				
STRUCTURAL ASSEMBLY DETAIL				
3	9-24-15	ADD REF. LINE FOR 15' MIN. DIMENSION	ECW	ECW
2	8-21-14	QTY. ITEMS 3-5, REV. NOTES 1 & 2	ECW	WLS
1	5-15-07	REVISED NAME & DESCRIPTION	TWF	HSK
0	3-30-06	CREATED	RMB	HSK
NO.	DATE	REVISION	BY	CHKD APPR
EWILL2	08-24-15			

No. TMD386A3	
PLOT 1=1	SH. 1 OF 1

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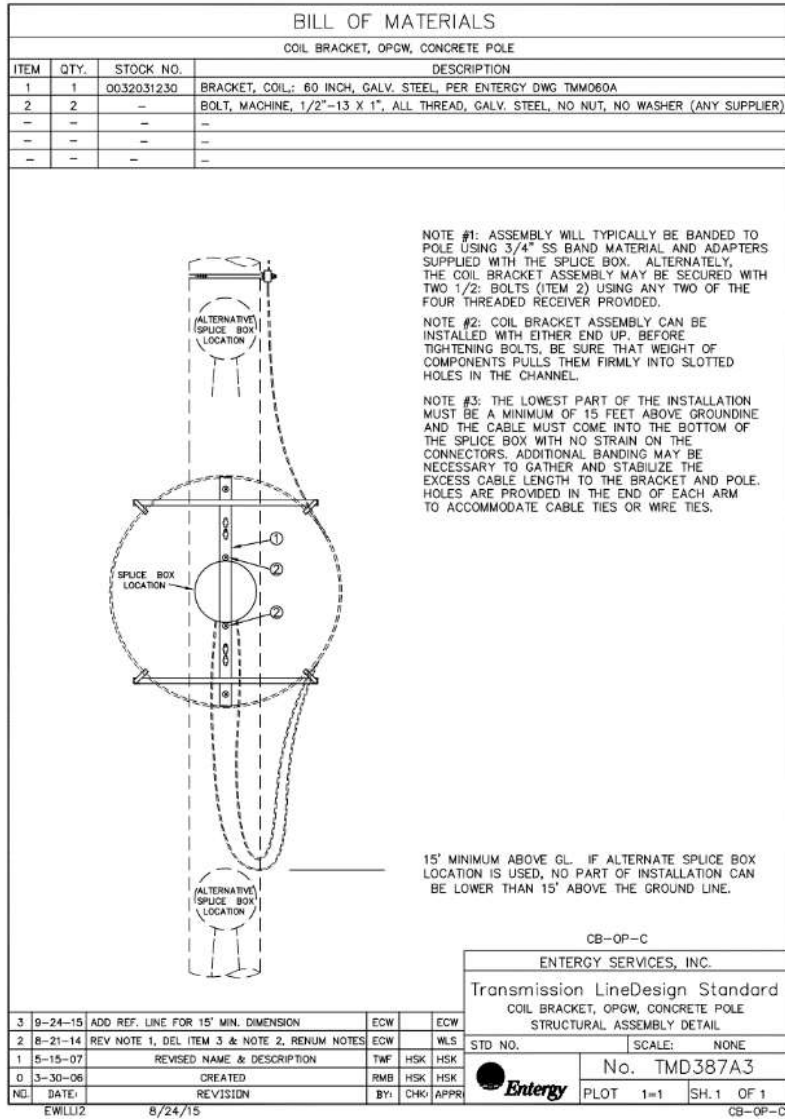
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BILL OF MATERIALS			
GROUND, DEADEND, OPWM, CONCRETE POLE			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	0032033755	JUMPER, STATIC LINE: MULTI-STRANDED TINNED COPPER, 133/.0177, 48" LG. W/TERMINALS

NOTE: ITEM 1 CAN BE MADE UP WITH 48" OF THE WIRE (0032018798) AND TWO TERMINALS (0032031548) AND COMPRESSING THE TERMINALS WITH AN INDENT DIE.

TOP GROUND CLIP ON CONCRETE POLES COMES WITH GREEN BOLT TO IDENTIFY INSERT HAVING CADWELD TO INTERNAL STEEL REINFORCING. RETAIN BOLT FOR FASTENING GROUND TERMINAL TO POLE GROUND.

BOLT COMES WITH DEADEND BODY

48" JUMPER LENGTH

GROUND-DE-OP-C

ENTERGY SERVICES, INC.

Transmission LineDesign Standard
GROUND, DEADEND, OPWM, CONCRETE POLE
STRUCTURAL ASSEMBLY DETAIL

STD. NO. SCALE: NONE

No. TMD398A0

NO.	DATE	REVISION	TWF	HSK	HSK
0	5-15-07	CREATED			
1	5/31/2007	REVISION			

Wincro 5/31/2007

ENTERGY

PLOT 1=1 SH.1 OF 1

GROUND-DE-OP-C

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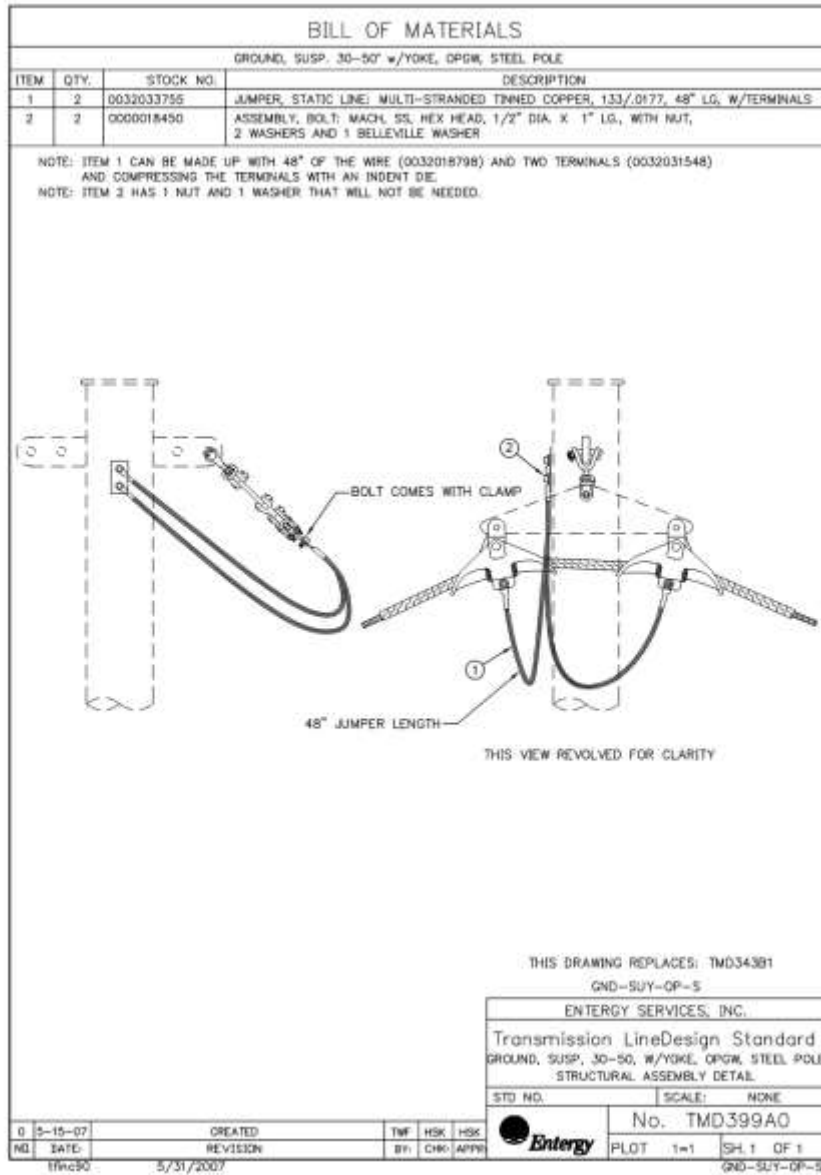
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BILL OF MATERIALS			
GROUND, DEADEND, OPGW, STEEL POLE			
ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	0032033755	JUMPER, STATIC LINE; MULTI-STRANDED TINNED COPPER; 133/.0177, 48" LG. W/TERMINALS
2	1	0000018450	ASSEMBLY, BOLT: MACH. SS. HEX HEAD, 1/2" DIA. X 1" LG., WITH NUT, 2 WASHERS AND 1 BELLEVILLE WASHER

NOTE: ITEM 1 CAN BE MADE UP WITH 48" OF THE WIRE (0032018798) AND TWO TERMINALS (0032031548) AND COMPRESSING THE TERMINALS WITH AN INDENT DIE.
NOTE: ITEM 2 HAS 1 NUT AND 1 WASHER THAT WILL NOT BE NEEDED.

THIS DRAWING REPLACES: TMD343C1
GND-DE-OP-S

ENTERGY SERVICES, INC.	
Transmission LineDesign Standard	
GROUND, DEADEND, OPGW, STEEL POLE	
STRUCTURAL ASSEMBLY DETAIL	
STD. NO.	SCALE: NONE
No. TMD402A0	
PLT	1=1 SH.1 OF 1

0	5-15-07	CREATED	TWF	HSK	HSK
NO	DATE	REVISION	BY	CHK	APPV
1	5/31/2007				

11/11/2007 5/31/2007 GND-DE-OP-S

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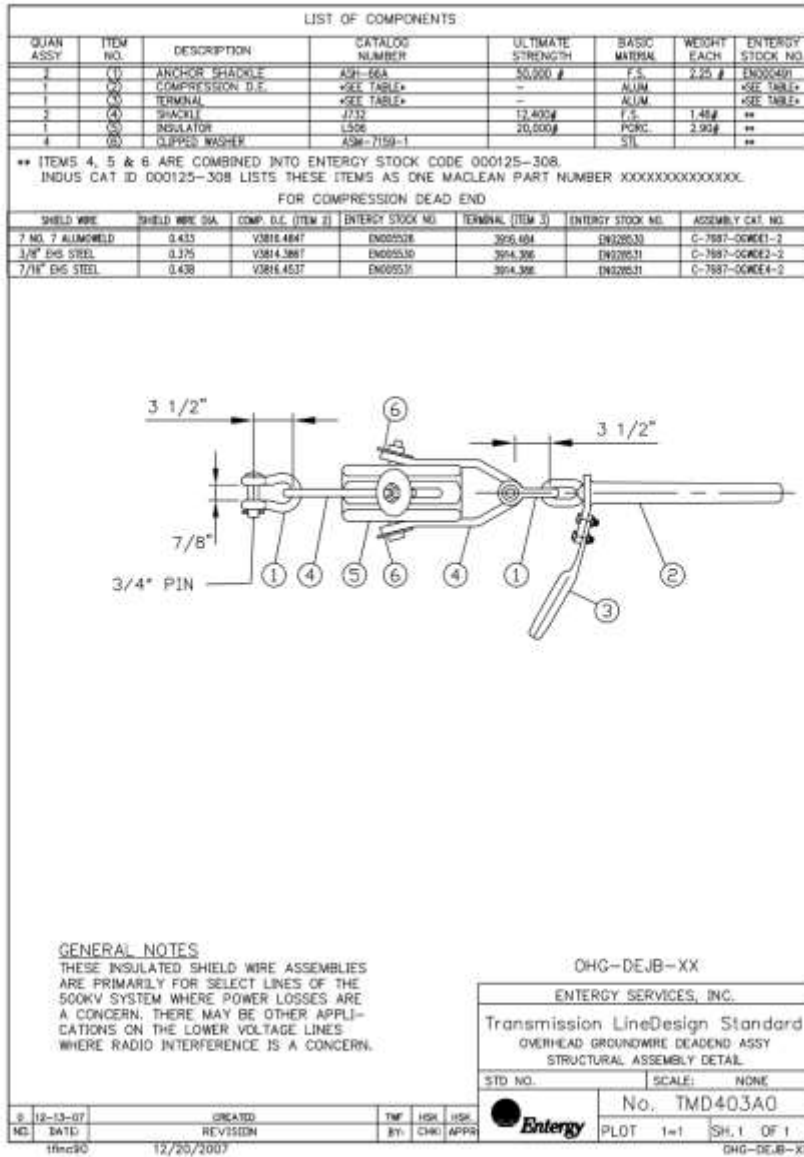
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REVISIONS		EXTENT APPROVAL	
REV.	DATE	BY	DATE
1	2/22/01		
2	2/27/01		
3	4/23/01		
4	6/4/01		
5	6/14/01		
6	10/3/01		
7	11/13/01		
8	12/13/01		
9	1/24/02		

REV.	DATE	DESCRIPTION
1	2/22/01	ENL. DRAWING
2	2/27/01	ADD 2ND SET
3	4/23/01	ADD 3RD SET
4	6/4/01	REV 1 INC. CAP-56
5	6/14/01	REV 2 INC. CAP-56
6	10/3/01	ENL. DRAWING
7	11/13/01	ENL. DRAWING
8	12/13/01	ENL. DRAWING
9	1/24/02	ENL. DRAWING

REF. DWG. NO. BC7687-0 FOR MATERIAL NOTES
ALL DIMENSIONS IN INCHES

ASSEMBLY C-7687-00WS1

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

ASSEMBLY C-7687-00WS1A

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ASSEMBLY C-7687-00WS1A

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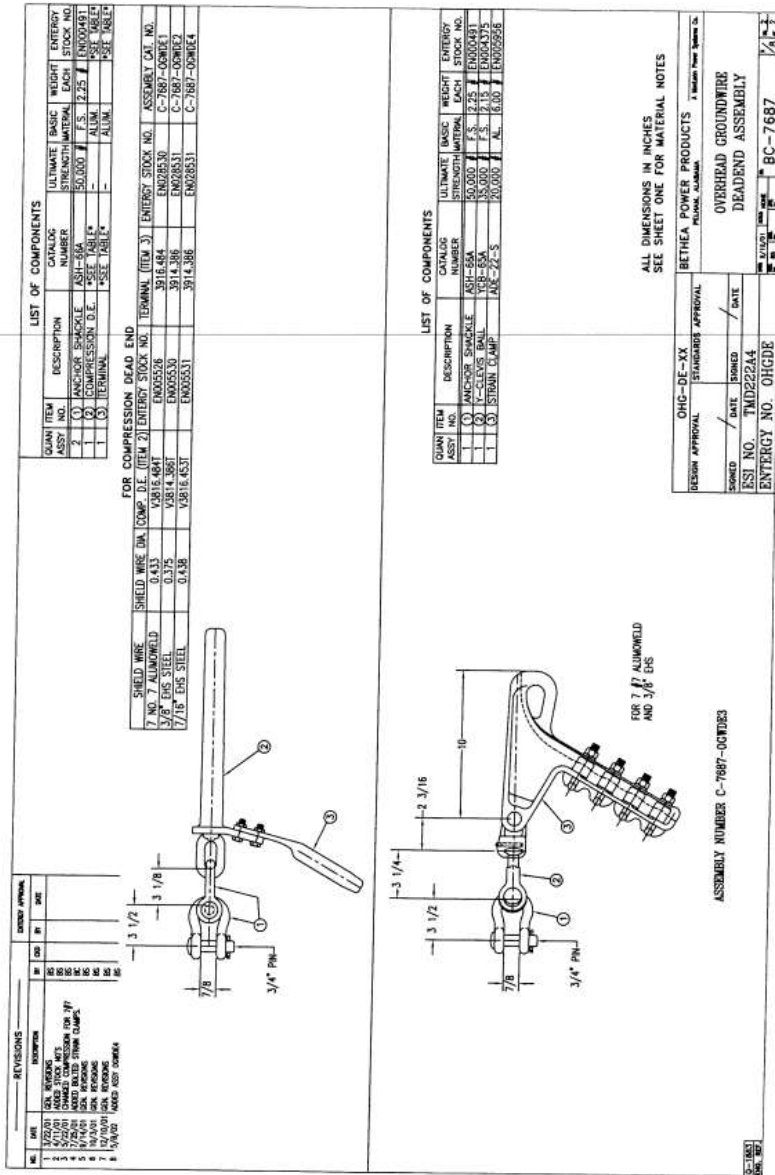
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REVISIONS				DESIGN APPROVAL			
NO.	DATE	DESCRIPTION	BY	CHKD BY	DATE		
1	1/27/04	FIG 1 BNC GP-804-C, 6025 OHM, 100 OHM	BE				

SHEILD WIRE (ITEM 5)		ENERGY STOCK NO.		ASSEMBLY CAT. NO.	
7/16" ALUMINUM	0.4335	AB-133			
7/16" BNC	0.4335	AB-133			
7/16" BNC	0.4375	AB-133			

QUANTITY	ITEM NO.	DESCRIPTION	CATALOG NUMBER	ULTIMATE STRENGTH	BASIC MATERIAL	WEIGHT EACH	ENERGY STOCK NO.
2	1	ANCHOR SHACKLE	ASH-56	140,000	1.5	1.47	FS018625
2	2	YOCHE PLATE	ASH-748-11	35,000	2.5	2.5	FS018625
2	3	SUSPENSION CLAMP	SC-1-S	18,000	AL 70/14.1	2.15	EN000392
2	4	ARMOR ROD	SEE TABLE				
2	5	SUSPENSION CLAMP	FS0-70-5	18,000	D.I.	6.00	

NOTE: ARMOR ROD NOT SHOWN

1 1/16

3/4 BOLT

2 3/4

2 3/4

1/2

3 1/4

2 3/16

2 3/8

30° MAX

6 3/8

9

18

7 7/16

2 5/16

30° MAX

CLAMPING RANGE: 0.40 - 0.87

CLAMPING RANGE: 0.30 - 0.70

ASSEMBLY C-7687-OCWS5

ASSEMBLY C-7687-OCWS4 & OCWS5

DESIGN APPROVAL		STANDARD APPROVAL	
SIGNED	DATE	SIGNED	DATE
ESI NO. TMD24A3		ESI NO. TMD24A3	
ENERGY NO. OHGSUY		ENERGY NO. OHGSUY	

BETHEA POWER PRODUCTS	
NATION, CALIFORNIA	
OVERHEAD GROUNDWIRE SUSPENSION ASSEMBLY	
BC-7687-3	BC-7687-3

REF. DWG. NO. BC7687-0 FOR MATERIAL NOTES
ALL DIMENSIONS IN INCHES

END

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LIST OF COMPONENTS			
QTY	ITEM NO.	DESCRIPTION	CATALOG NUMBER
2	1	ANCHOR SHOCKLE	ASH-50A
2	2	COMPRESSION D.E.	SEE TABLE*
2	3	TERMINAL	SEE TABLE*
2	4	INSULATOR	1500
4	5	CUPPED WASHER	ASM-7159-1

FOR COMPRESSION DEAD END			
SHIELD WIRE	SHIELD WIRE DIA.	COMP. D.E.	ENERGY STOCK NO.
7/8" ALUM.	0.315	13816.46H	EN055528
7/8" EPS STEEL	0.315	13816.46H	EN055530
7/8" EPS STEEL	0.418	13816.45H	EN055531

REF. DWG. NO. BC7687-G FOR MATERIAL NOTES
ALL DIMENSIONS IN INCHES

ENERGY REV. A
REVISION DATE 10/12/07
ESI NO. BC-7687-4

OVERHEAD GROUNDWIRE DEADEND ASSEMBLY

BC-7687-4

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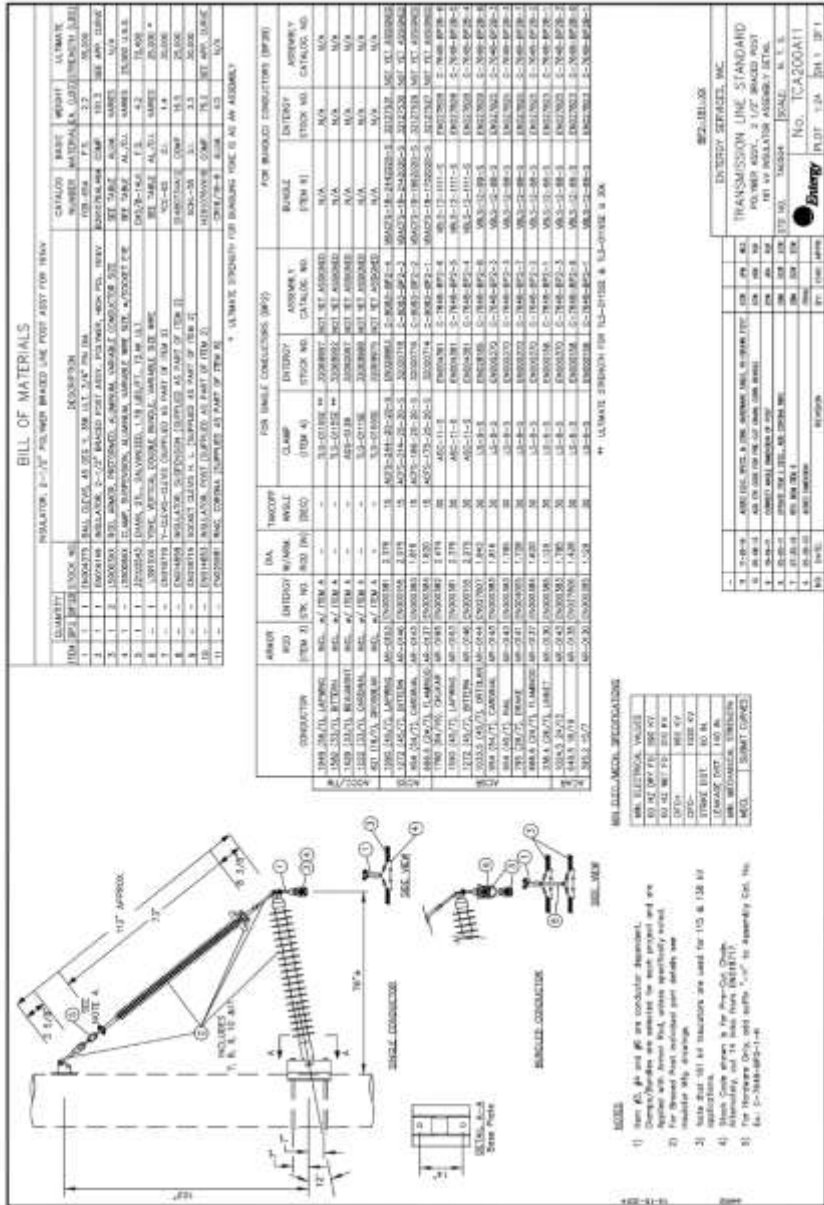
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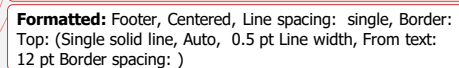
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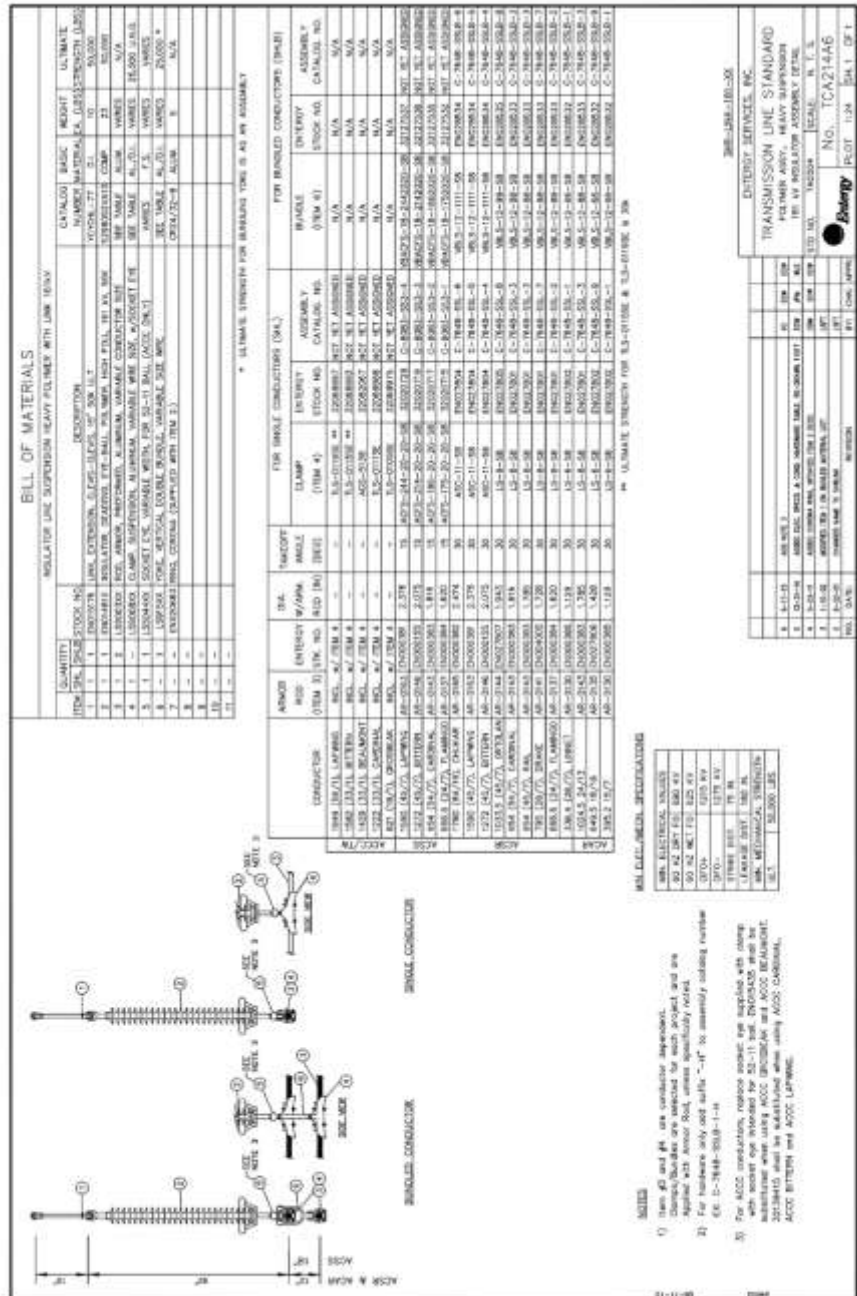
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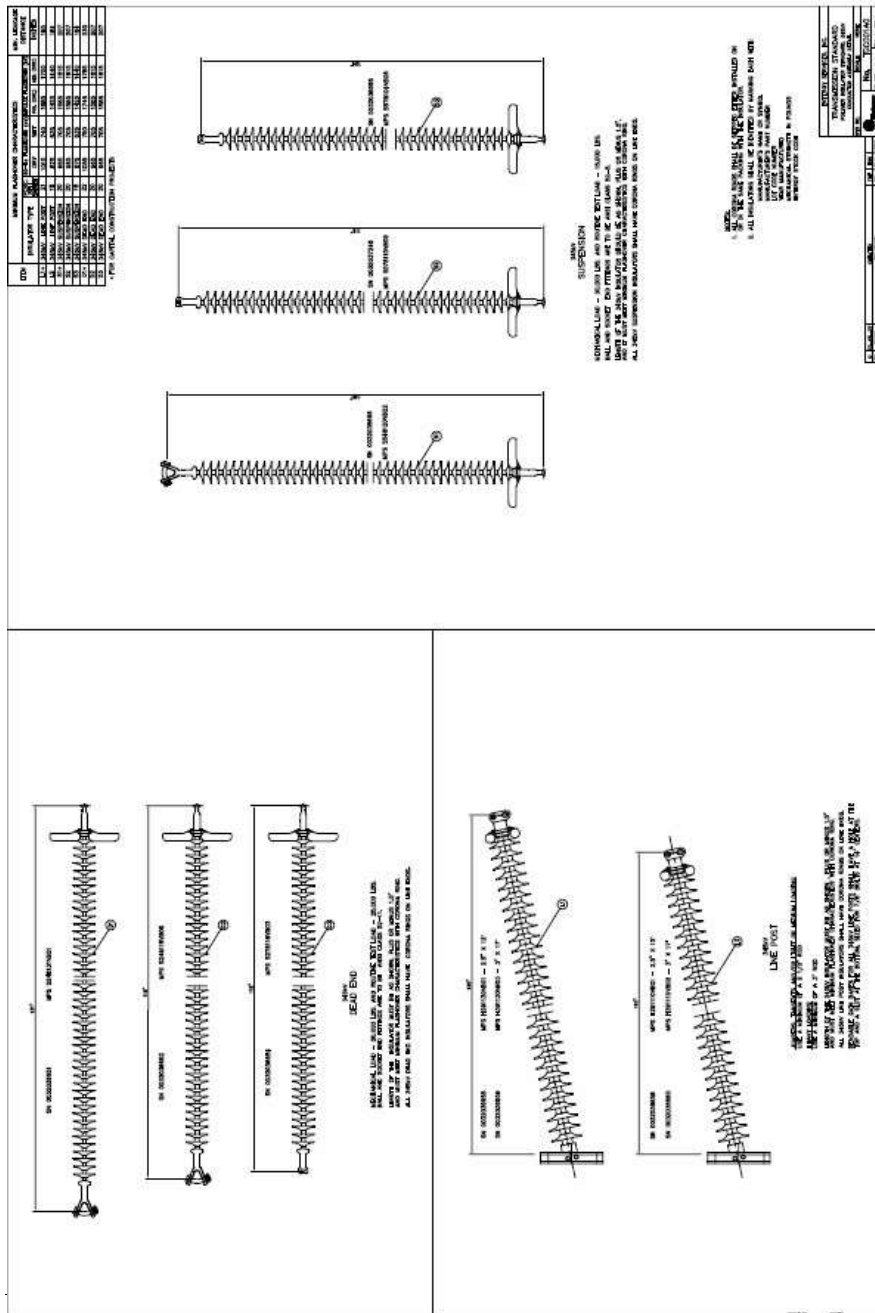
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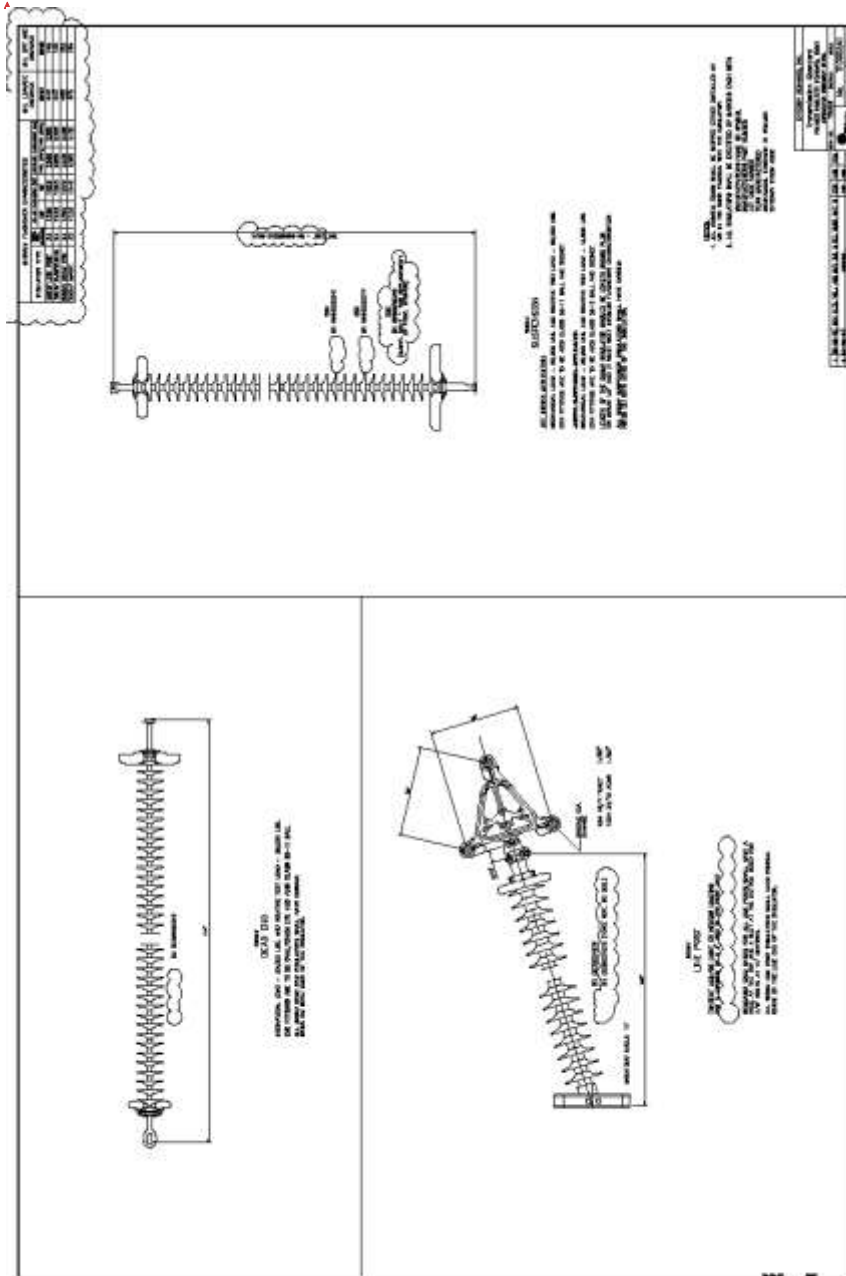
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BILL OF MATERIALS

DEADEND, POLYMER, WITH BUNDLING YOKE, 500KV

ITEM	COMP. QTY.	BOLTED QTY.	STOCK NO.	DESCRIPTION
1	2	2	0032009672	SHACKLE, CHAIN, 150k ULT. STR.
2	1	1	0032009669	YOKE PLATE, TRIPLE BUNDLE, DEADEND, 18" SEPARATION, 110k ULT. STR.
3	14	11	0000000689	SHACKLE, ANCHOR, 50k ULT. STR.
4	1	1	0032009670	YOKE PLATE, TRIPLE BUNDLE, DEADEND, 18" SEPARATION, 110k ULT. STR.
5	1	1	0032009665	LINK EXTENSION, EYE-EYE, 40k ULT. STR.
6	3	3	0032009668	PLATE, ADJUSTMENT, 40k ULT. STR.
7	3	3	0032000342	INSULATOR, LINE, EYE-BALL, POLYMER, 500KV, 50k ULT. STR.
8	3	3	LS9012XX	DEADEND, COMPRESSION, ALUMINUM, SINGLE TONGUE, 33k, FOR VARIABLE
9	3	3	0000028529	SOCKET, Y-CLEVIS, 50k
10	1	1	0032000136	LINK, CHAIN, 132k ULT., 7" LONG
11	3	3	0032021867	CLEVIS BALL, 35k, BALL CLASS 52-3/5
12	3	3	LS9013XX	DEADEND, BOLTED, STRAIN, ALUM., 30k, FOR VARIABLE WIRE SIZE
13	1	1	0032009685	CORONA RING, 500KV DEADEND, ALUM.
14	3	3	LS9014XX	TERMINAL CONNECTOR, 15-DEG., FOR VARIABLE WIRE SIZE
15	3	3	LS5029XX	JUMPER, SPLICE, FOR VARIABLE WIRE SIZE

CONDUCTOR	CONDUCTOR DIA.	COMP. D.E. (ITEMS 8 & 14)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR	1.165	VES-130-EHV**	0032000078	C-7686-DE1	NA
954.0 45/7 "RAIL"	1.165	VES-133-EHV**	0032021873	C-7686-DE2	NA
954 54/7 "CARDINAL"	1.196	VES-135-EHV**	0032021874	C-7686-DE4	NA

CONDUCTOR RANGE: BOLTED STRAIN CLAMP (ITEM 12)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
.710" - 1.318"	0000028892	C-7686-DE3	NA

* ITEMS 15 ARE NOT FURNISHED WITH THE MACLEAN ASSEMBLIES.
** COMPRESSION DEADEND BODIES COME WITH JUMPER TERMINALS, ITEM 14. EITHER OF
OF ITEMS 8 AND 14 CAN BE RETURNED TO STORES WITH THEIR SEPARATE STOCK CODES.

COND. CONFIG.

1) ITEM #8, #12, #14 & #15 ARE CONDUCTOR DEPENDENT.
2) DESIGNER MAY SUBSTITUTE #11 & #12 & #15.
FOR ITEMS #3 (QTY. 2) & #8. STRAIN CLAMP SHALL
INCLUDE SOCKET EYE FOR A 52-3/5 BALL. USE OF
BOLTED CLAMPS WILL REQUIRE THE USE OF NON-TENSION
JUMPER SPLICES.

RE: MACLEAN DWG. BC-7686-1

ENTERGY SERVICES, INC.

DEADEND, POLYMER, W/BUNDLING YOKE, 500KV

STD NO.	SCALE:
	NONE

No. TFA200A0

PL0T 1=1 SH.1 OF 1

DEPY-500-XX; BC-7686-1

0	03-05-07	CREATED	TWF	HSK
ND.	DATE:	REVISION	BY:	CHK

tffc90 3/5/2007

APPR

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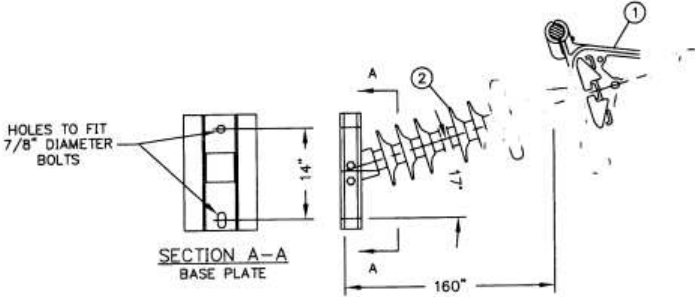
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BILL OF MATERIALS						
JUMPER LINE POST, POLYMER, W/BUNDLING YOKE, HORIZONTAL, 500kV						
ITEM	QTY.	STOCK NO.	DESCRIPTION			
1	1	LS9015XX	JUMPER YOKE, 10k ULT. STR. 18" SEPARATION, ALUMINUM ALLOY			
2	1	0032021878	INSULATOR, LINE POST, 3", POLYMER, 500kV, 10k ULT. STR.			

CONDUCTOR	CONDUCTOR DIA.	JUMPER YOKE (ITEM 1)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR	1.165	C-7686-4	0032021850	C-7686-J2	NA
954.0 45/7 "RAIL"	1.165	C-7686-4	0032021850	C-7686-J2	NA
954 54/7 "CARDINAL"	1.196	C-7686-4A	0032021860	C-7686-J2A	NA



1) ITEM #1 IS CONDUCTOR DEPENDENT. THIS ITEM IS SELECTED FOR EACH PROJECT (WITHOUT ARMOR RODS).

RE: MACLEAN DWG. BC-7686-4

ENTERGY SERVICES, INC.

JUMPER LINE POST, POLYMER, W/YOKE, HOR, 500kV

STD. NO. SCALE: NONE

No. TFA201A0

Entergy

PLOT 1=1 SH.1 OF 1

JLPB-HJ-500-XX; BC-7686-4

NO.	DATE	CREATED	THW	HSK
0	03-05-07	REVISION	BY:	CHK: APPR

tfinc90 3/19/2007

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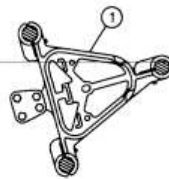
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BILL OF MATERIALS

JUMPER LINE POST, POLYMER, w/BUNDLING YOKE, VERTICAL, 500kV

ITEM	QTY.	STOCK NO.	DESCRIPTION
1	1	LS9015XX	JUMPER YOKE, 10k ULT. STR. 18" SEPARATION, ALUMINUM ALLOY
2	1	0032021879	INSULATOR, LINE POST, 3", POLYMER, 500kV, 10k ULT. STR.

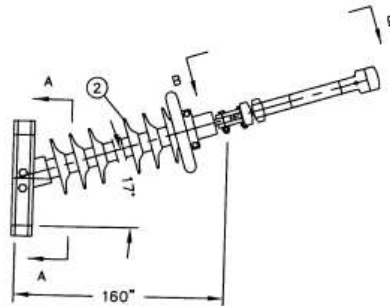
CONDUCTOR	CONDUCTOR DIA.	JMPR. YOKE (ITEM 1)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR	1.185	C-7686-4	0032021850	C-7686-J3	NA
954.0 45/7 "RAIL"	1.185	C-7686-4	0032021850	C-7686-J3	NA
954 54/7 "CARDINAL"	1.196	C-7686-4A	0032021860	C-7686-J3A	NA



SECTION B-B
YOKE PLATE

HOLES TO FIT
7/8" DIAMETER
BOLTS

SECTION A-A
BASE PLATE



1) ITEM #1 IS CONDUCTOR DEPENDENT. THIS ITEM IS
SELECTED FOR EACH PROJECT (WITHOUT ARMOR RODS).

RE: MACLEAN DWG. BC-7686-5

ENTERGY SERVICES, INC.

JUMPER LINE POST, POLYMER, W/YOKE, VER, 500kV

STD NO.

SCALE: NONE



No. TFA202A0

PLOT 1=1 SH.1 OF 1
JLPB-VJ-500-XX; BC-7686-5

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Attachment 1: Applicable Standard Framing and Assembly Drawings

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BILL OF MATERIALS					
JUMPER SUSPENSION, POLYMER, w/ BUNDLING YOKE 500kV					
ITEM	QTY.	STOCK NO.	DESCRIPTION		
1	1	0000004466	SHACKLE, ANCHOR, 30k ULT. STR., 5/8" PIN DIA. 2-13/16"		
2	1	0000028889	BALL EYE, OVAL, 35k ULT. STR., BALL CLASS 52-3/5		
3	1	LS9016XX	YOKE, JUMPER, 10k ULT. STR. 18" SEPARATION, ALUM. ALLOY		
4	1	0032000277	INSULATOR, SUSPENSION, B&S, POLYMER, 500kV, 25k ULT. STR.		
5	1	0032021870	CLEVIS, SOCKET, 30k ULT. STR., CLASS 52-3/5		

CONDUCTOR	CONDUCTOR DIA.	JMPR. YOKE (ITEM 3)	ENTERGY STOCK NO.	ASSEMBLY CAT. NO.	ENTERGY STOCK NO.
1024 ACAR	1.165	C-6549-3	0032021827	C-7686-J1	NA
954.0 45/7 "RAIL"	1.165	C-6549-3	0032021827	C-7686-J1	NA
954 54/7 "CARDINAL"	1.196	C-7686-5	0032021863	C-7686-J1A	NA

1) ITEM #3 IS CONDUCTOR DEPENDENT.
THIS ITEM IS SELECTED FOR EACH
PROJECT WITHOUT ARMOR RODS.

RE: MACLEAN DWG. BC-7686-2

ENTERGY SERVICES, INC.

JUMPER SUSPENSION, POLYMER, W/YOKE, 500kV

STD. NO. SCALE: NONE

No. TFA203A0

Entergy PLOT 1=1 SH.1 OF 1
JSPB-500-XX; BC-7686-2

DATE	CREATED	BY	CHK	APP
05-07	3 5 2007			

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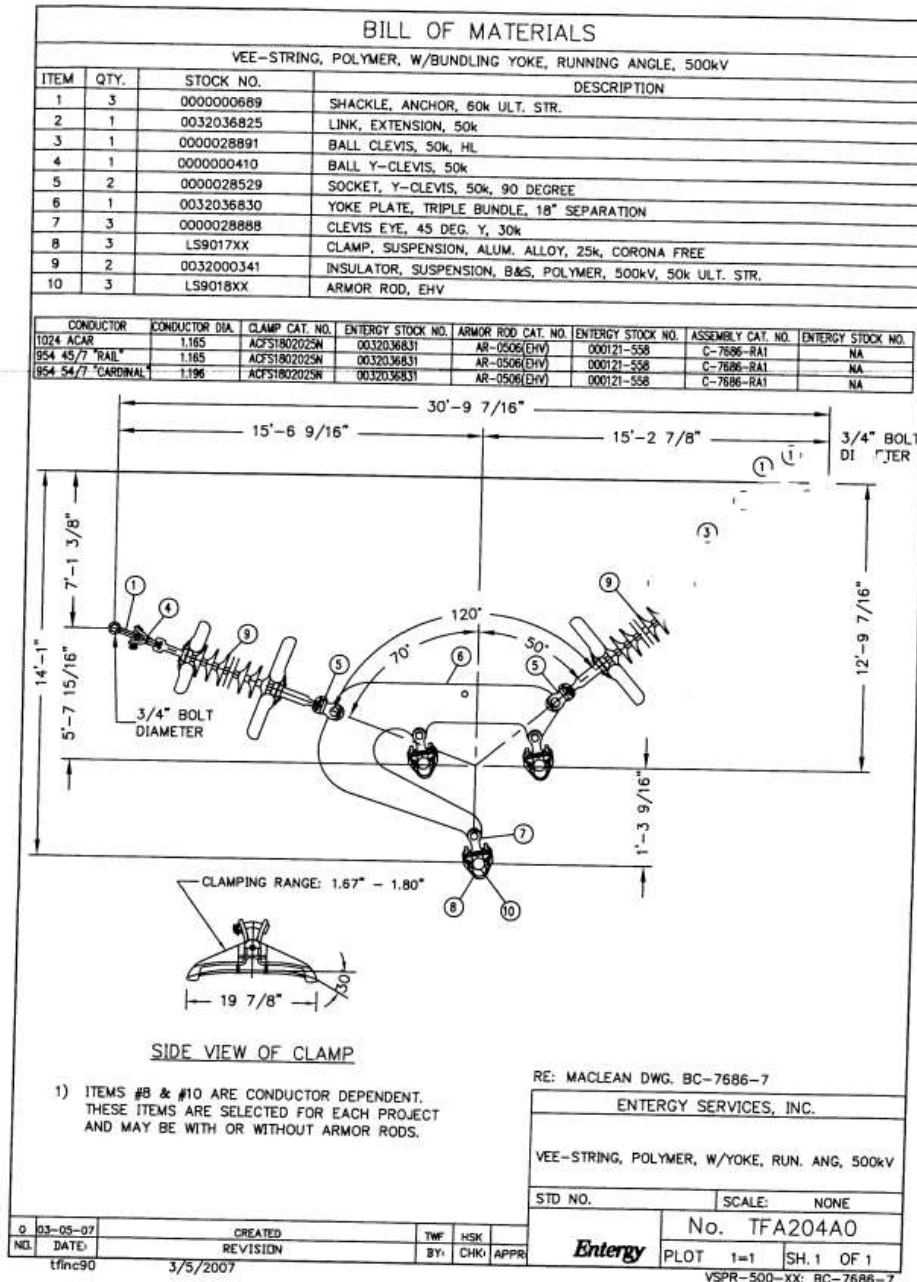
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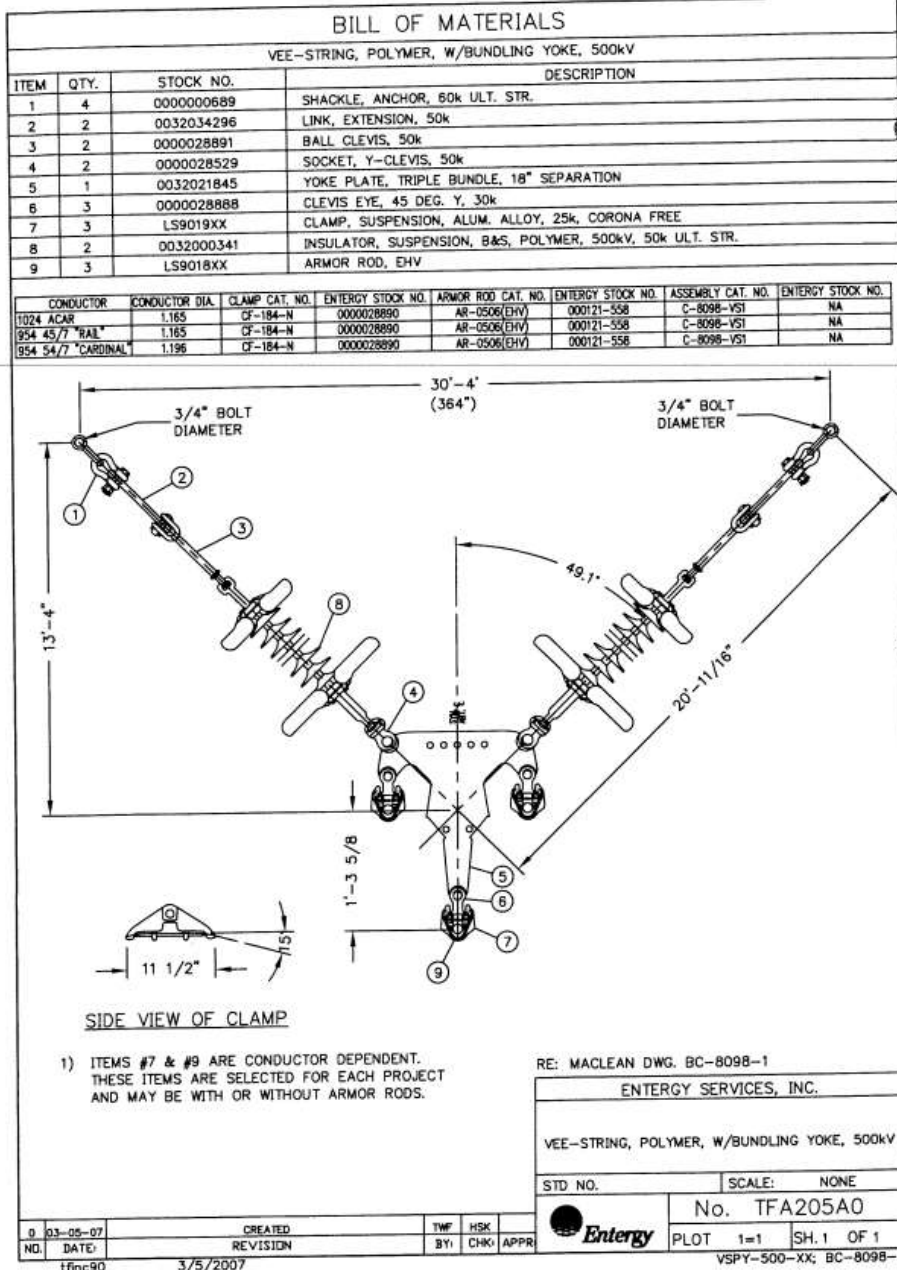
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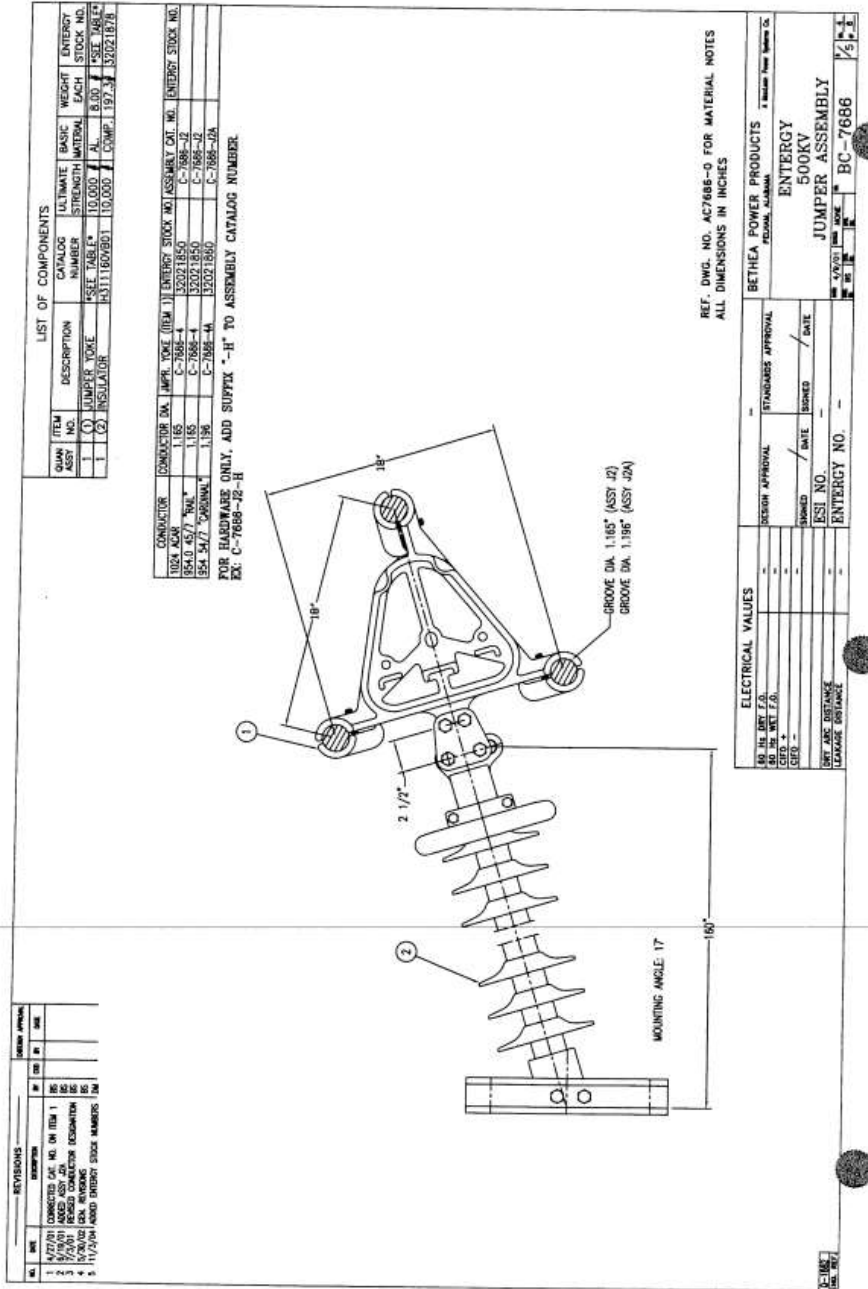
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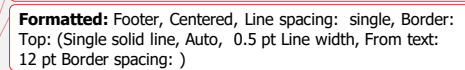


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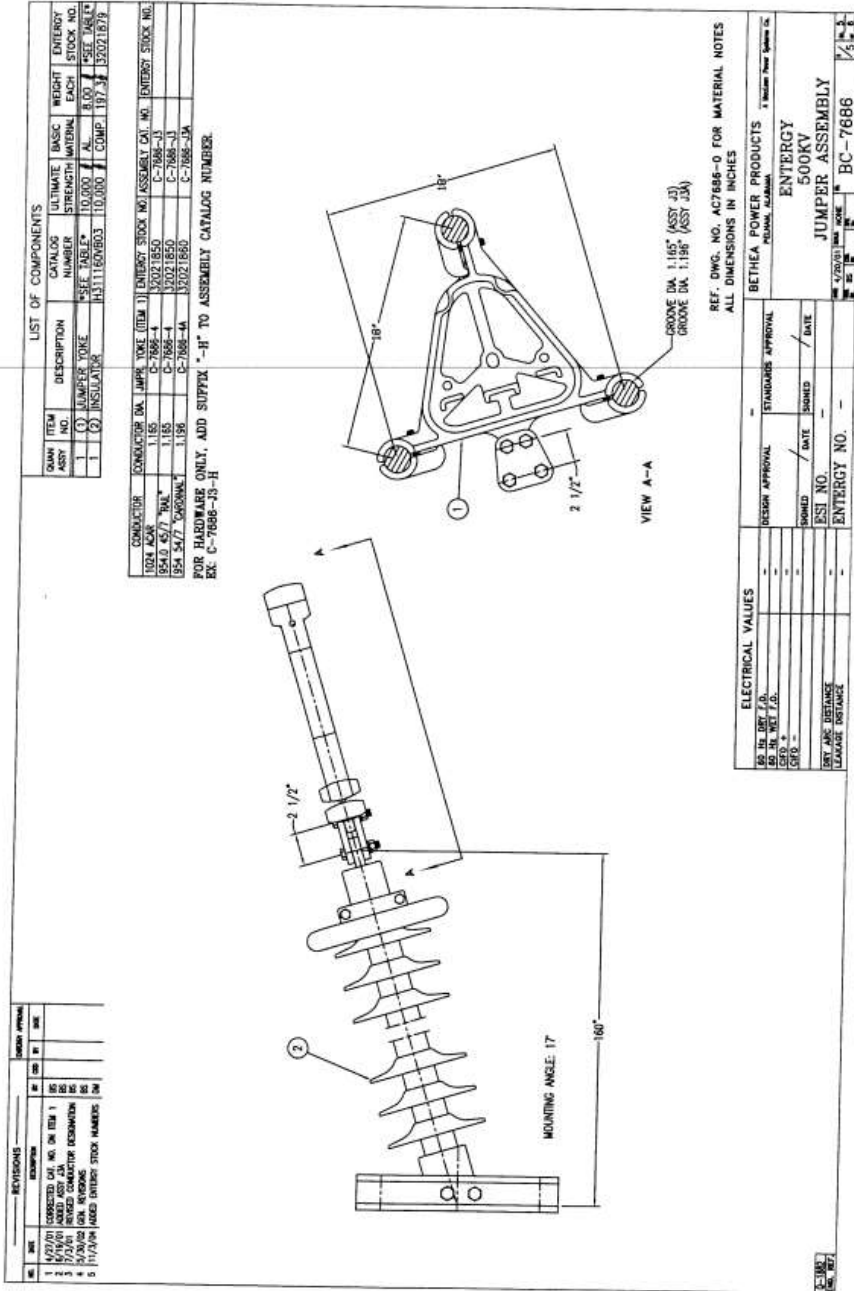


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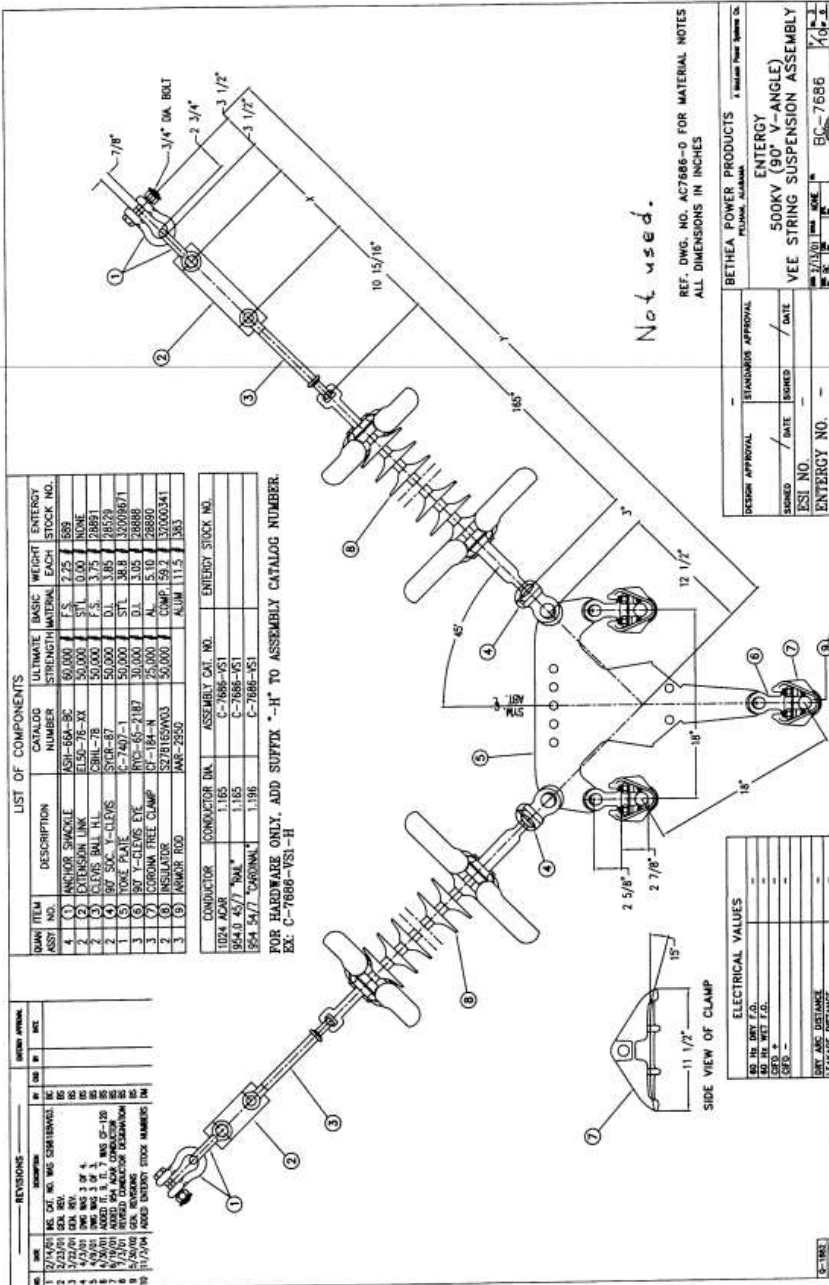
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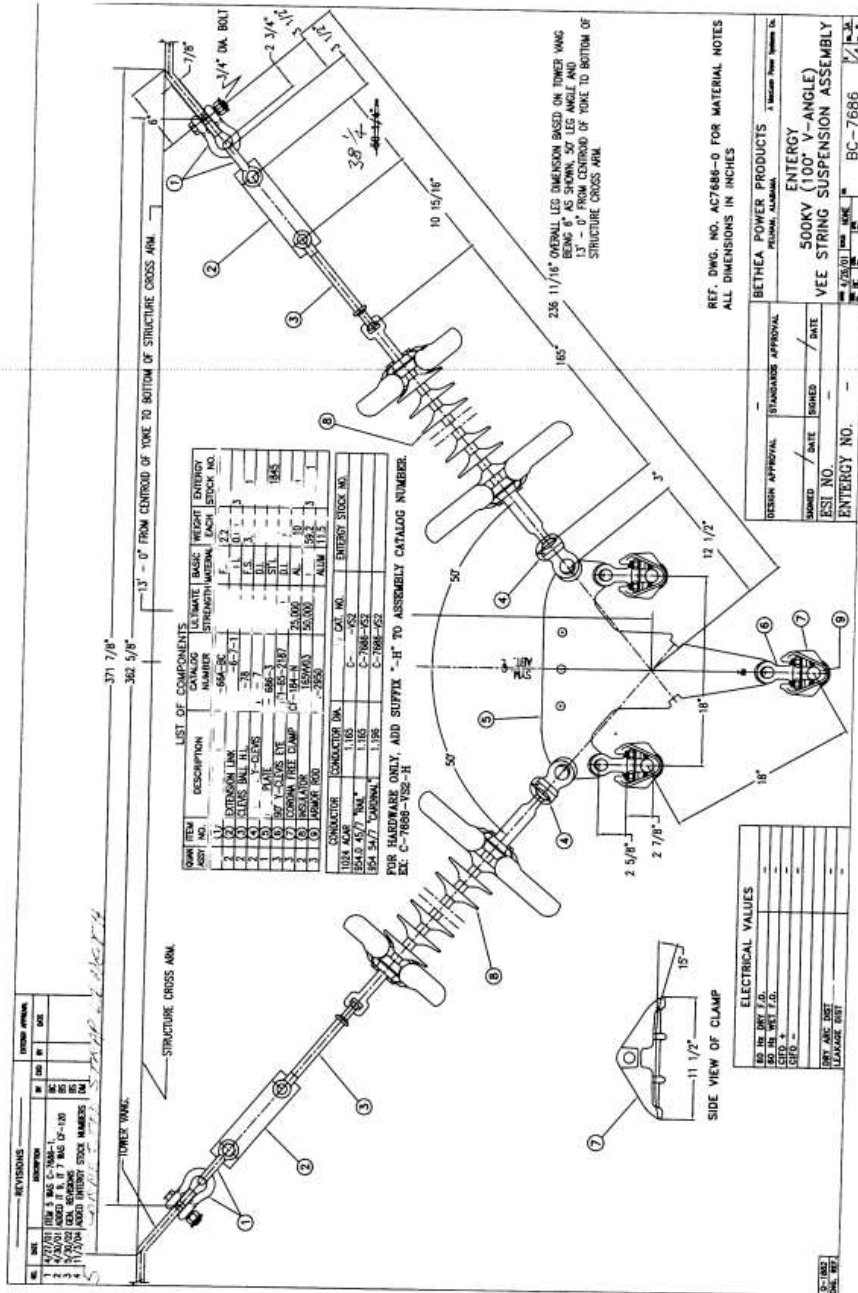
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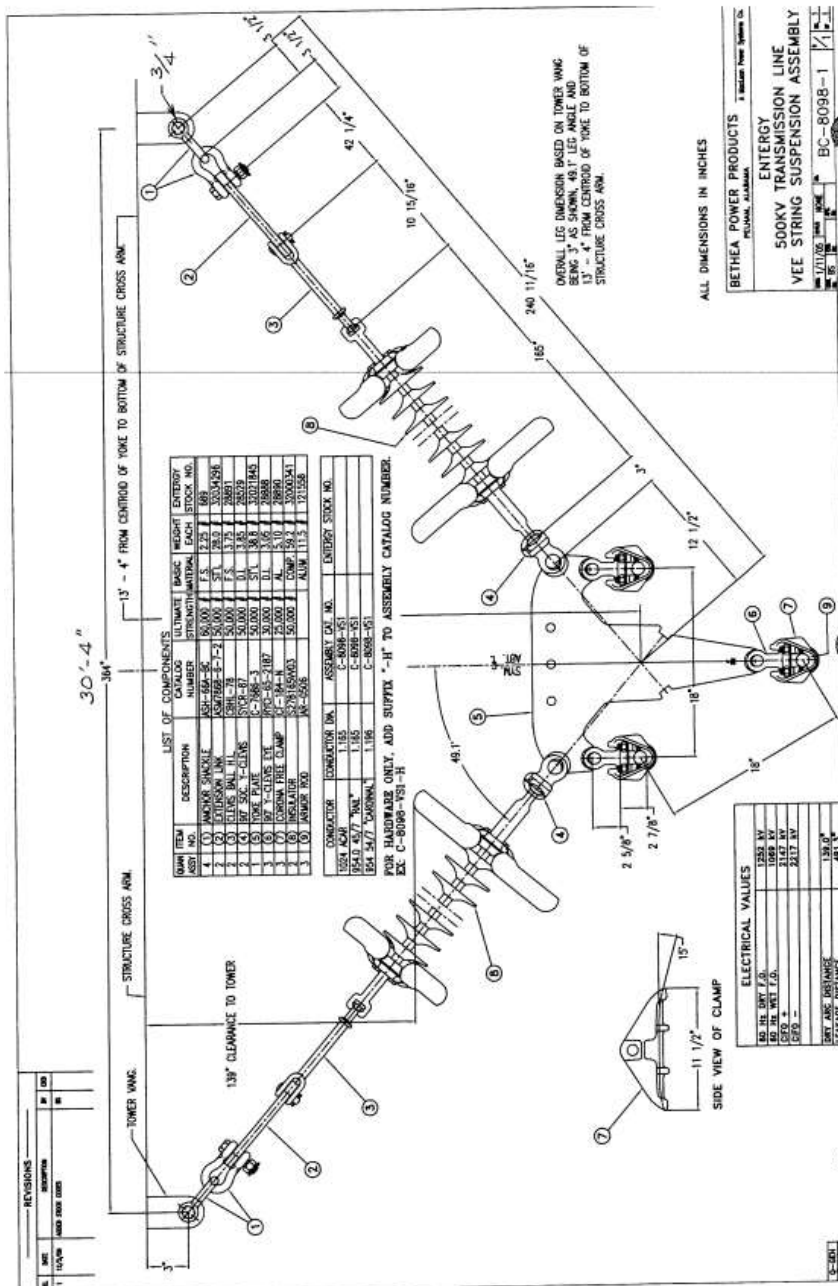
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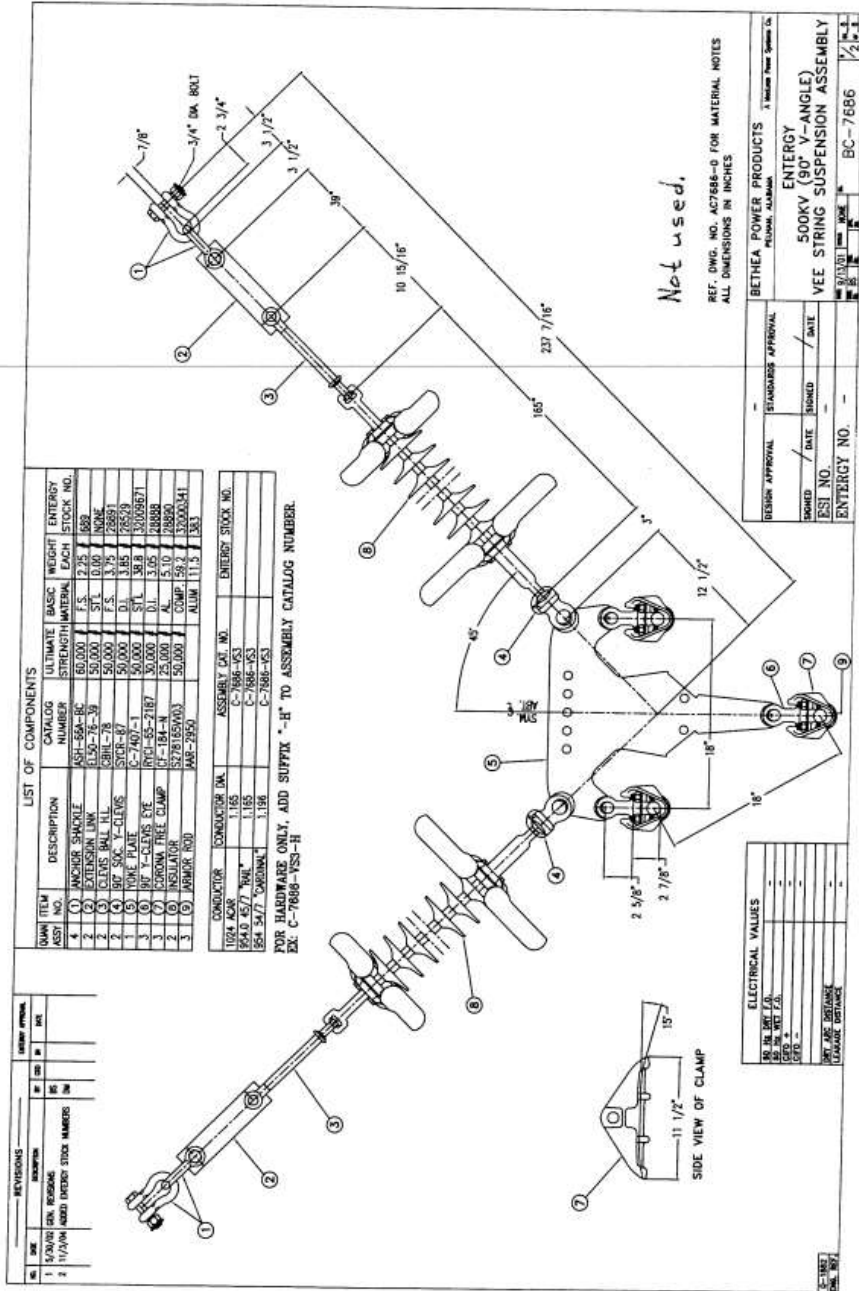
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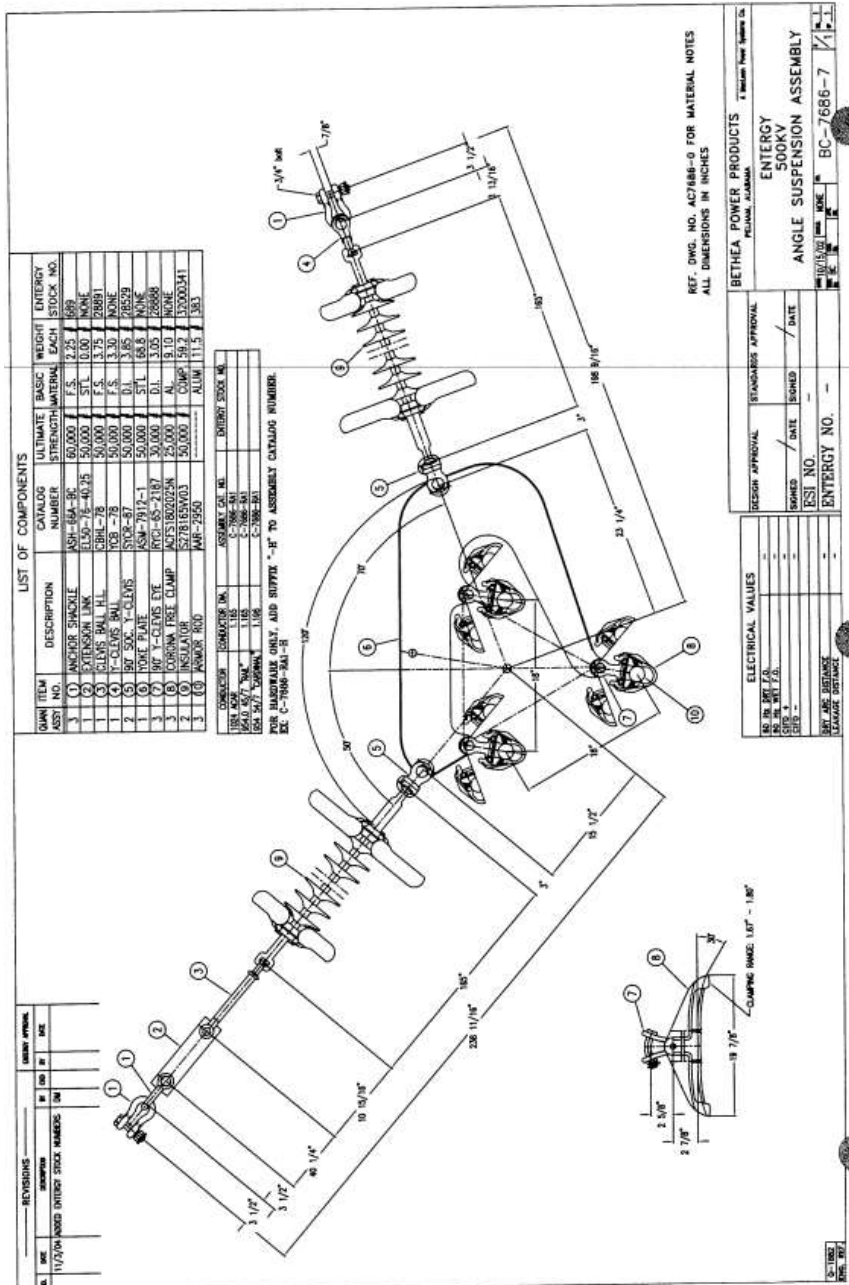
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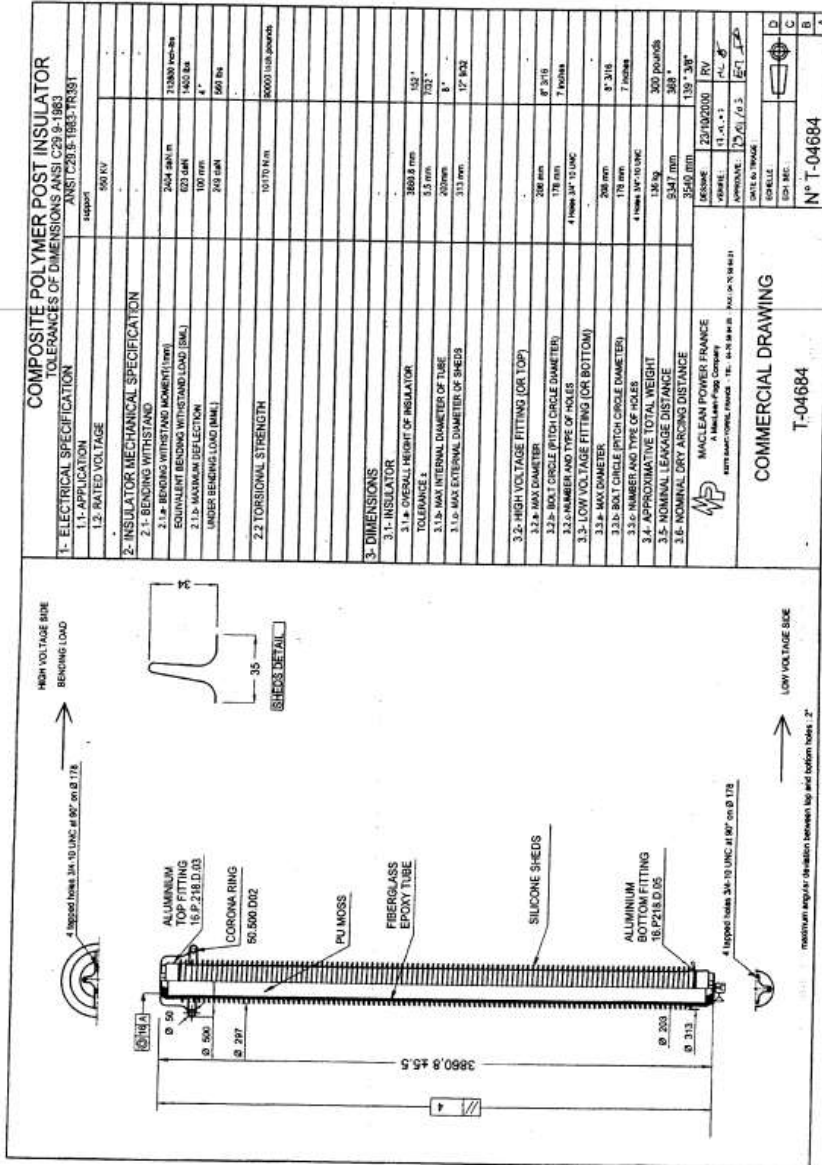
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Exhibit A - Page 90

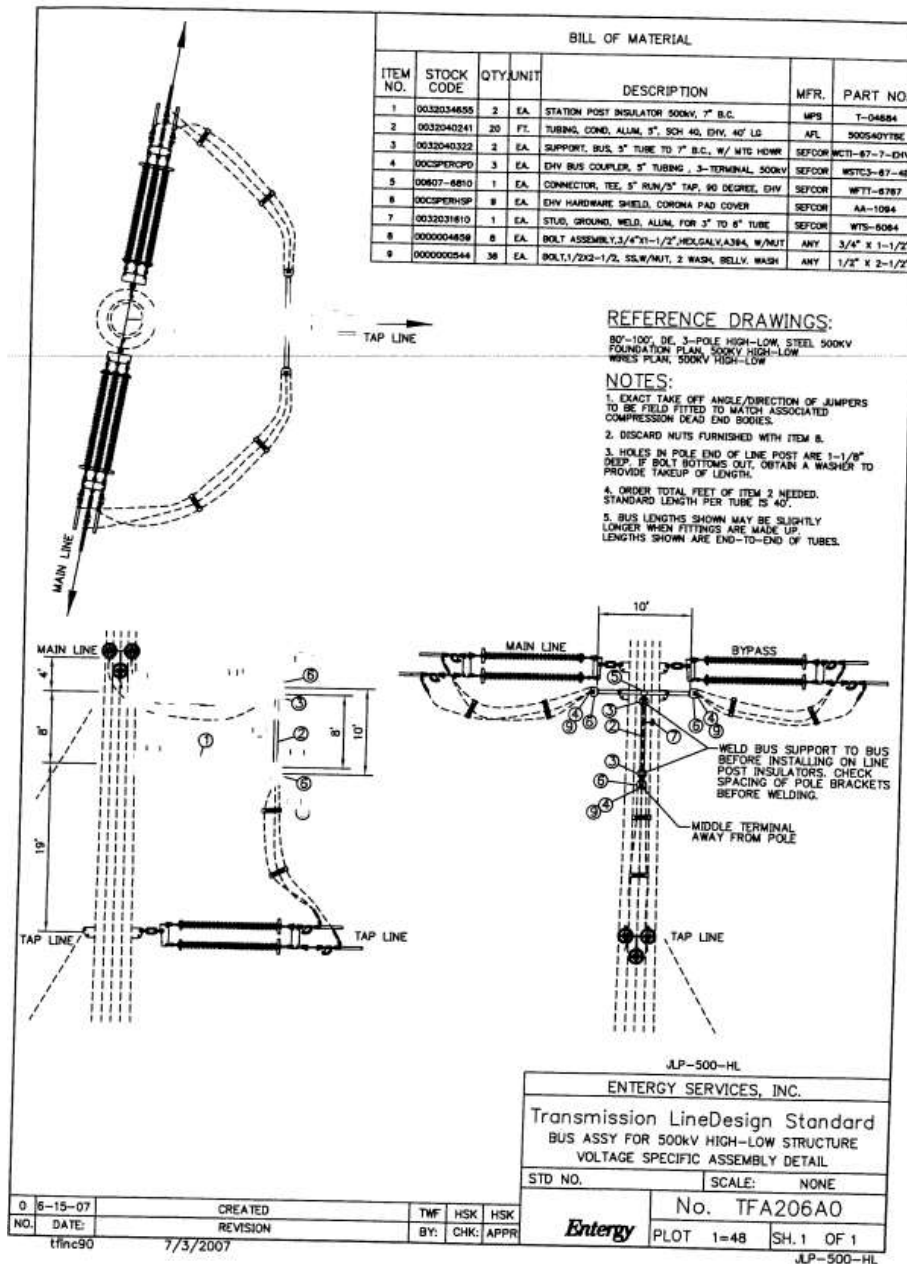
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Exhibit A - Page 91

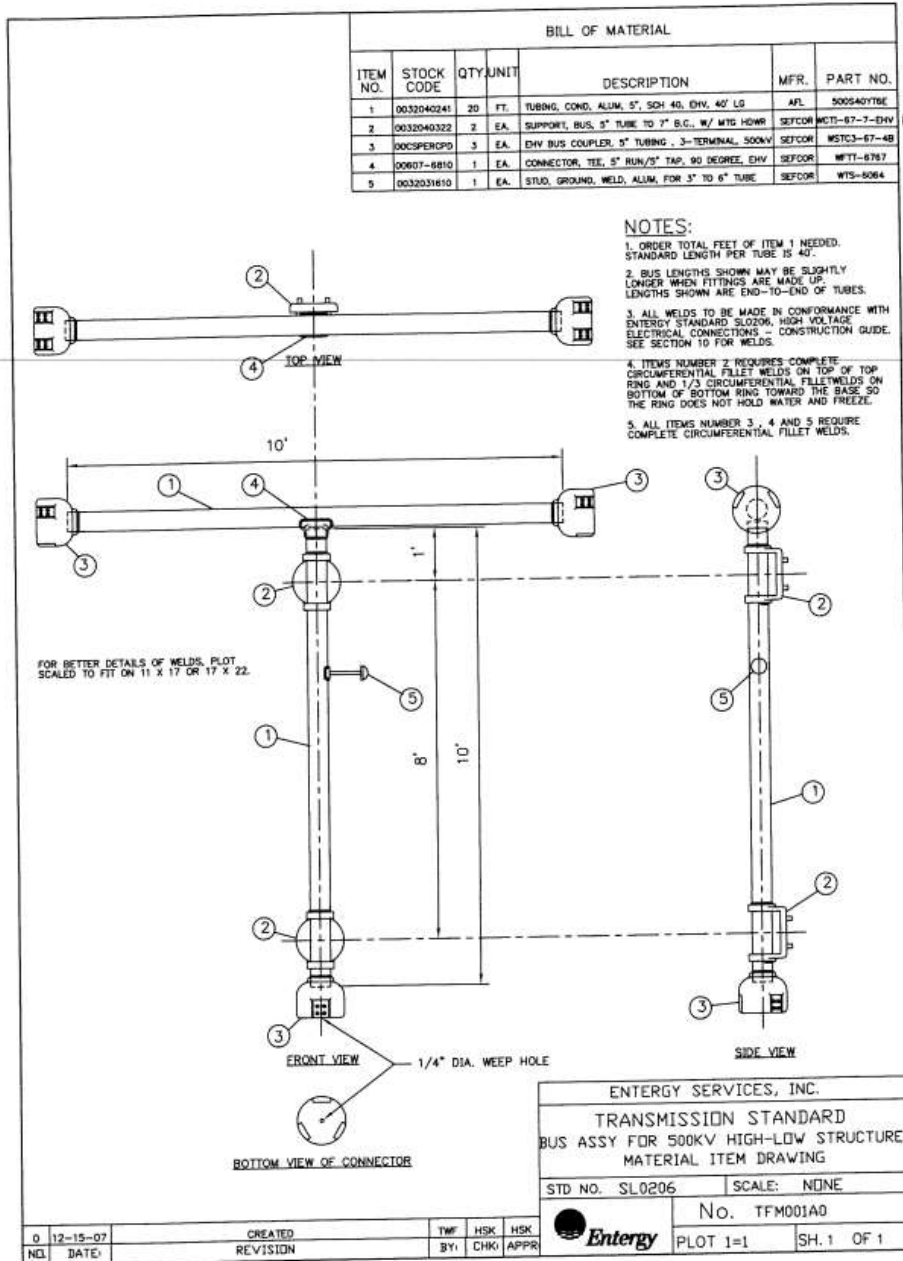
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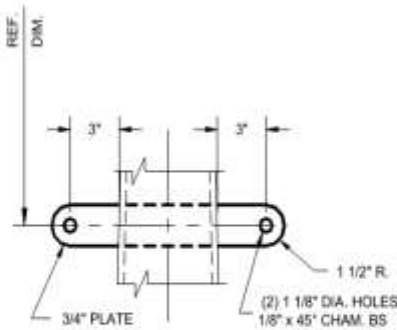
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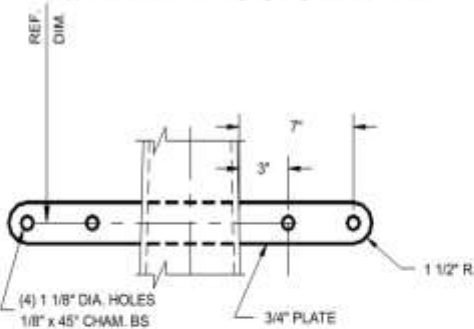
Vang Details for Steel Poles



LIGHT-DUTY 2-HOLE VANG

Primary uses:

- Support shield wire span guys
- Support top of braced-post insulator assemblies
- Support conductor swinging angle assemblies



LIGHT-DUTY 4-HOLE VANG

Primary use:

- Support shield wire suspension

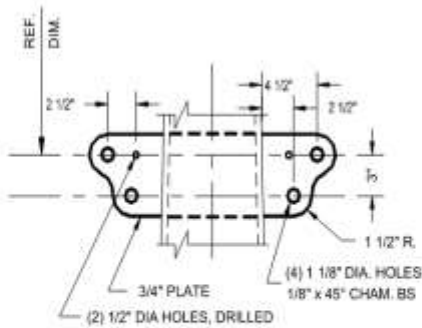
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Vang Details for Steel Poles



HEAVY-DUTY 4-HOLE VANG

Primary use:

Support shield wire deadend assemblies
Support conductor deadend assemblies
Support conductor deadend down guys
Support conductor bisector down guys
Support shield wire deadend down guys
Support shield wire bisector down guys
All conductor and shield wire vangs on structures with running
angle insulators (E, F and G)

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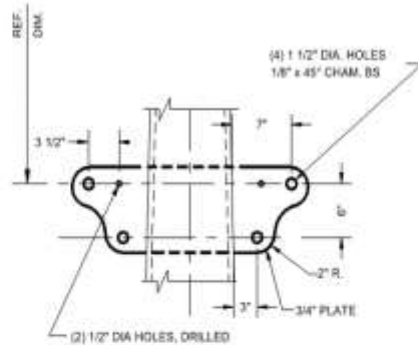
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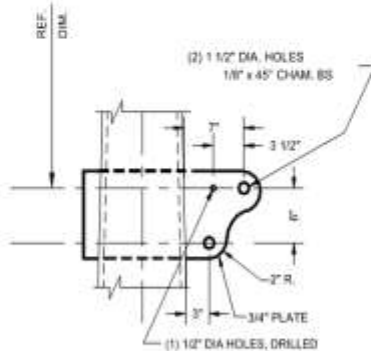
Vang Details for Steel Poles



HEAVY-DUTY 4-HOLE VANG FOR TRIPLE BUNDLE SINGLE POINT DEAD ENDS

Primary use:

Support 500kv conductor dead end assemblies where guys will be at the same elevation as the conductors and when guys are not specified.



HEAVY-DUTY 2-HOLE VANG FOR TRIPLE BUNDLE SINGLE POINT DEAD ENDS

Primary use:

Support 500kv conductor dead end assemblies and guys where guys are specified and will attach at locations below the conductors. Do not install guy vangs on unguyed structures with this type of vang unless specified by Entergy.

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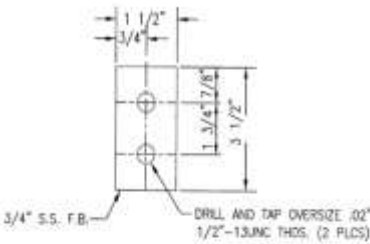
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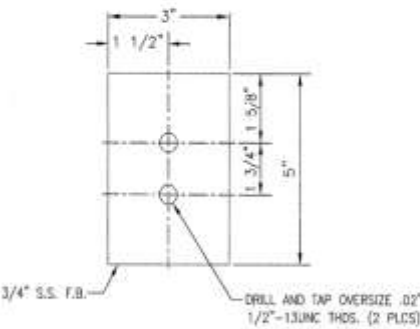
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NEMA Pad Details for Steel Poles or Caissons



SMALL NEMA 2-HOLE PAD



LARGE NEMA 2-HOLE PAD

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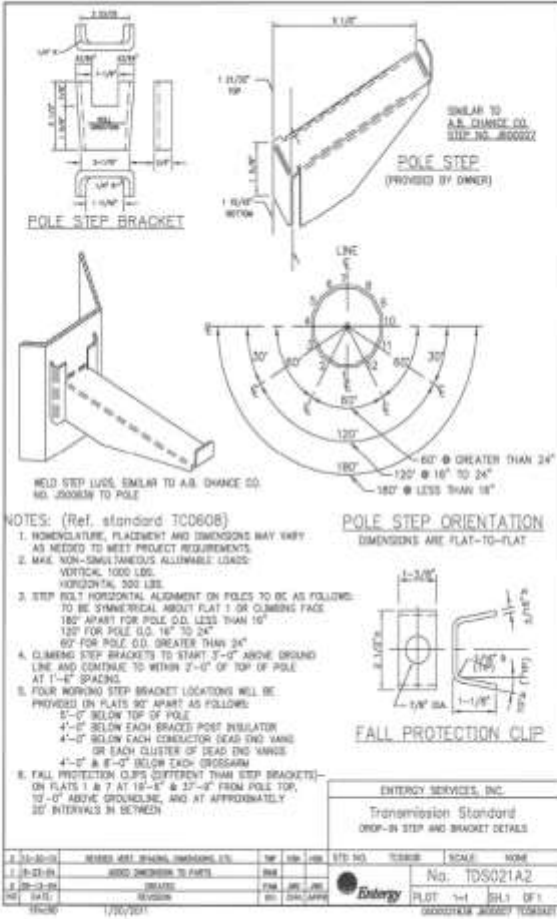
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Climbing Details

TDS021A1, Step and Bracket Details, represents the Entergy specifications for drop-in steps.



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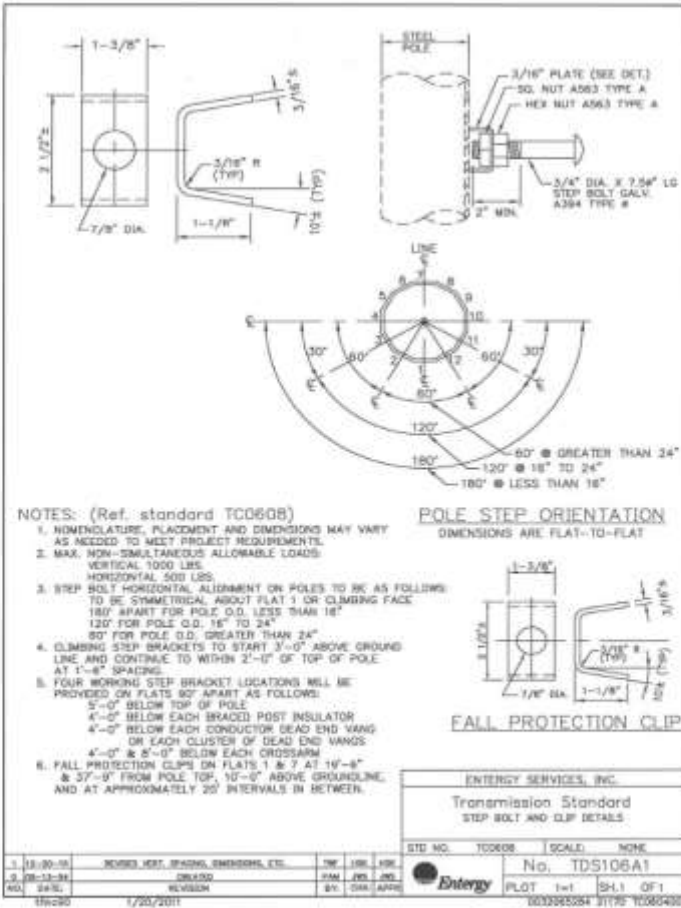
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Climbing Details

TDS106A1, Step Bolt Details, represents the Entergy specifications for pole steps.



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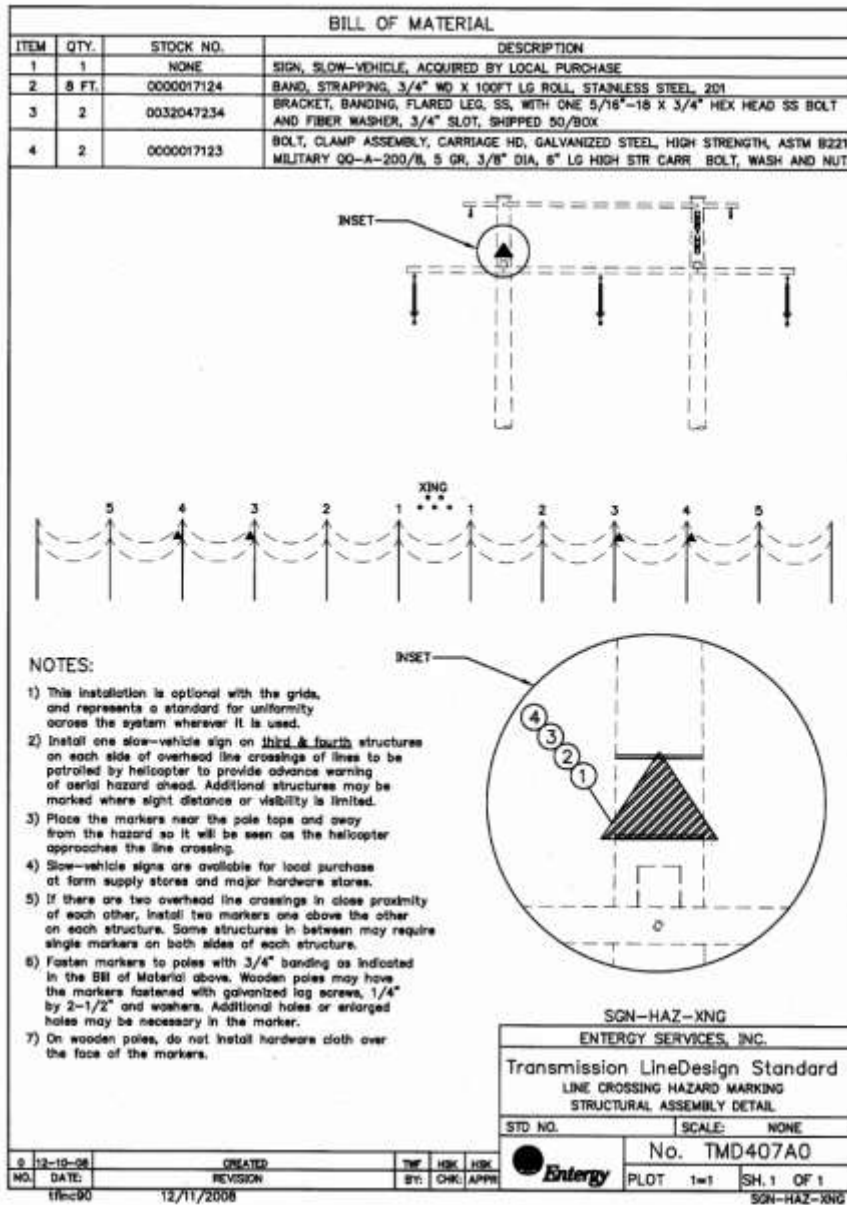
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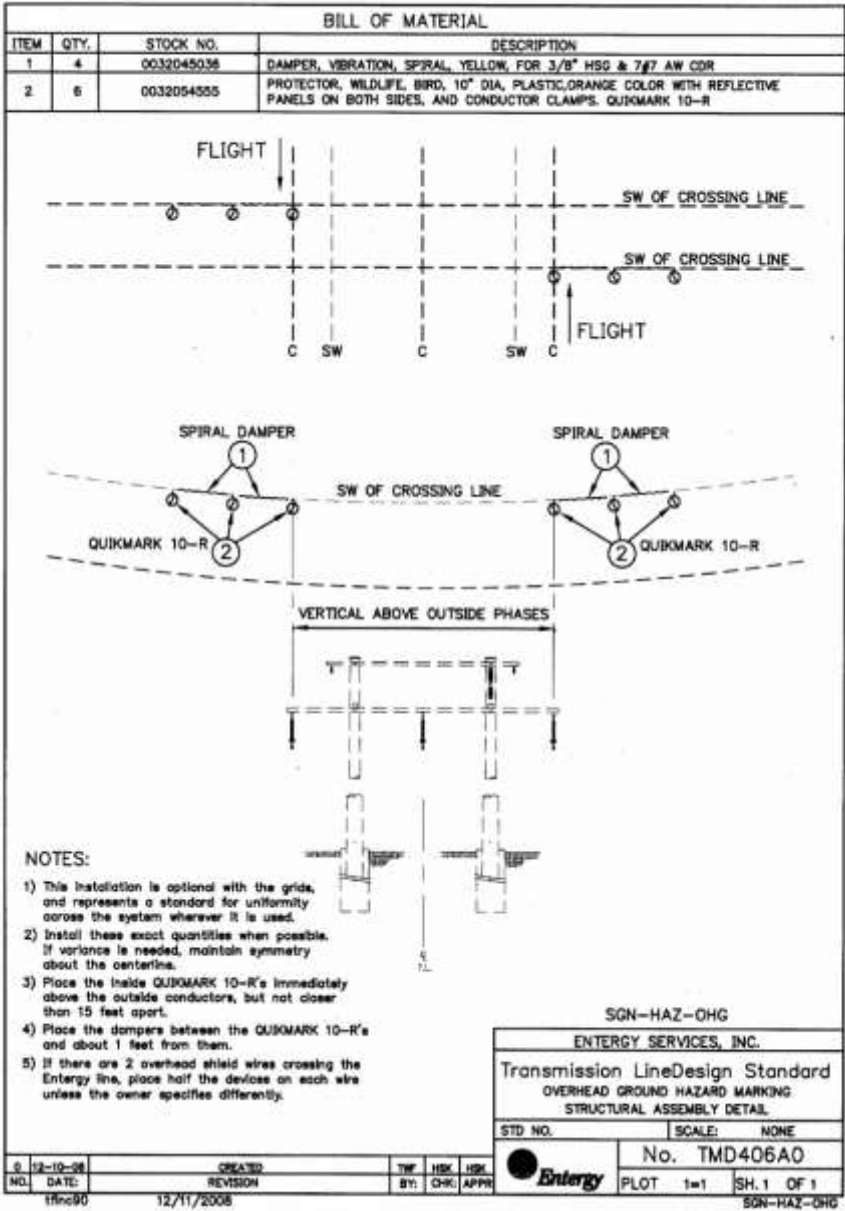


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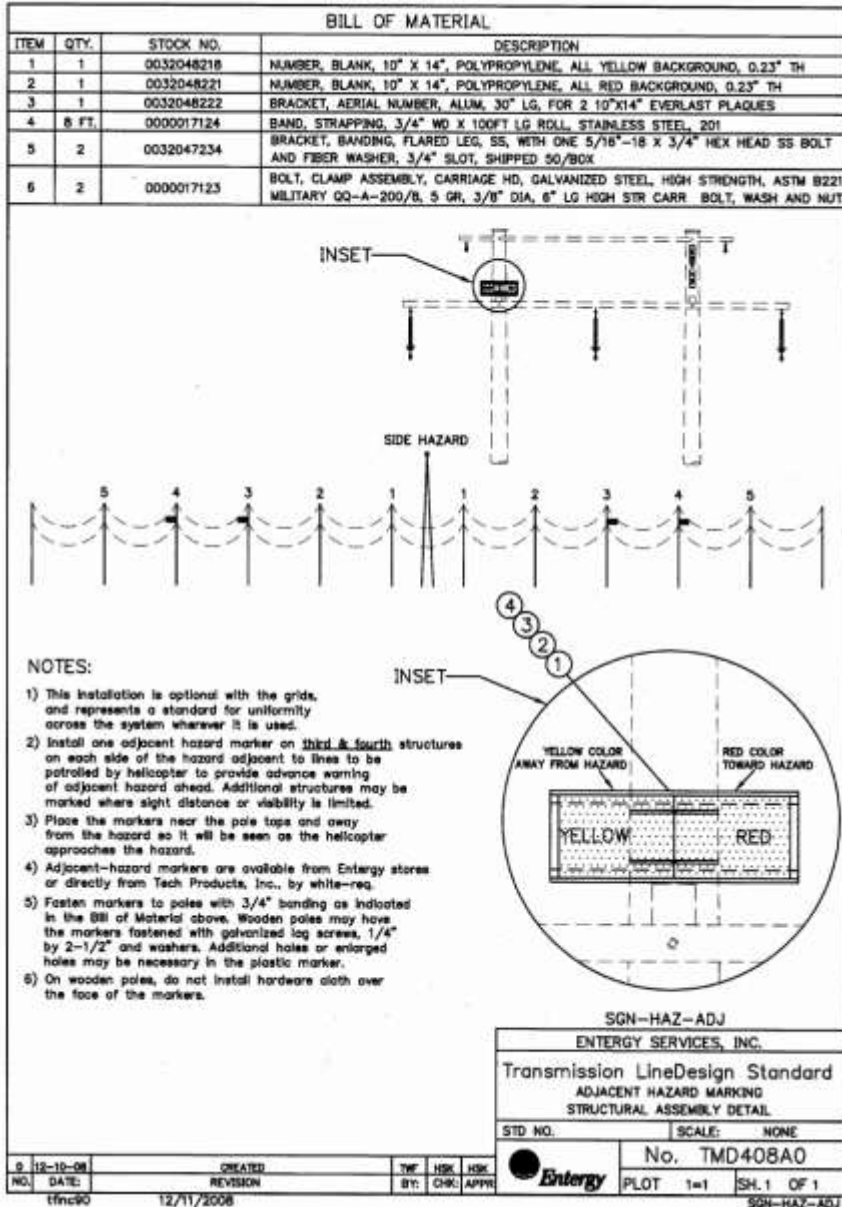
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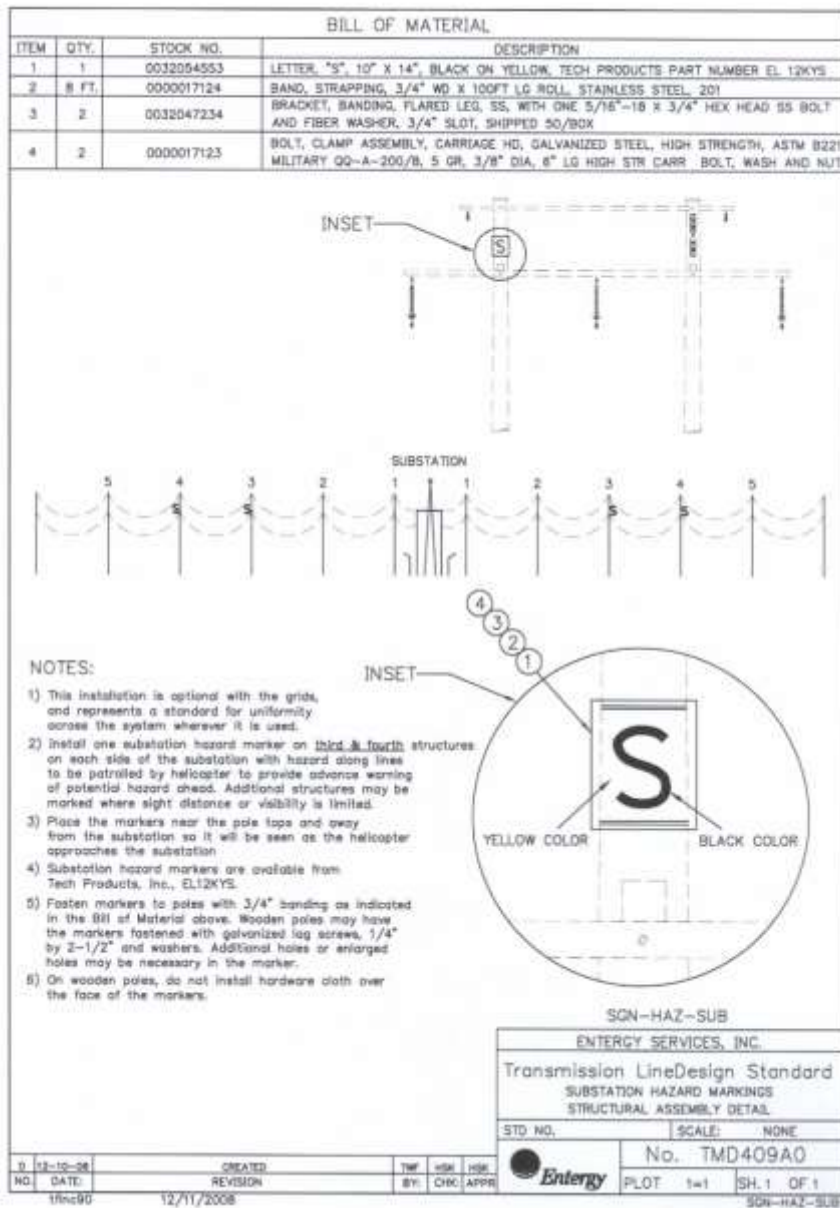
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Attachment 2: NESC and Entergy Clearance Requirements

ATTACHMENT 2
NESC AND ENTERGY CLEARANCE REQUIREMENTS

Basic NESC Clearance Requirements

Rule 230A2, Emergency Vertical Clearances to Ground							
	69	115	138	161	230	345	500
Truck Accessible	16.2	17.1	17.6	18.0	19.4	21.7	24.9
Pedestrian Only	9.7	10.6	11.1	11.5	12.9	15.2	18.4

RULE 232B&C - Vertical Clearance over Ground, Roadway, Rail or Water Surfaces							
	69	115	138	161	230	345	500
Railroad	27.16	28.09	28.56	29.02	30.41	32.74	35.87
Roads	19.16	20.09	20.56	21.02	22.41	24.74	27.87
Other Area Traversed by Vehicles	19.16	20.09	20.56	21.02	22.41	24.74	27.87
Accessible to Pedestrian Traffic Only	15.16	16.09	16.56	17.02	18.41	20.74	23.87

Attachment 2: NESC and Entergy Clearance Requirements

RULE 233C - Vertical Clearance over Another Wire With or Without Wind

	69	115	138	161	230	345	500
0	2.66	3.59	4.06	4.52	5.91	8.24	11.85
13.8	2.93	3.86	4.32	4.79	6.18	8.50	12.12
34.5	3.32	4.25	4.72	5.18	6.58	8.90	12.52
69	4.06	4.98	5.45	5.91	7.31	9.63	13.25
115	4.98	5.91	6.38	6.84	8.24	10.56	14.18
138	5.45	6.38	6.84	7.31	8.70	11.03	14.64
161	5.91	6.84	7.31	7.77	9.17	11.49	15.10
230	7.31	8.24	8.70	9.17	10.56	12.89	16.50
345	9.63	10.56	11.03	11.49	12.89	15.21	18.82
500	13.25	14.18	14.64	15.10	16.50	18.82	22.44

RULE 234B, C & G - Vertical Clearance over Various Structures

	69	115	138	161	230	345	500
Lighting Supports	5.23	6.16	6.62	7.09	8.48	10.80	13.94
Traffic Signal Supports	5.23	6.16	6.62	7.09	8.48	10.80	13.94
Supporting Structures of Other Lines	5.23	6.16	6.62	7.09	8.48	10.80	13.94
Intermediate Poles in Skip-Span Construction	5.23	6.16	6.62	7.09	8.48	10.80	13.94
Building Roofs not Accessible to Pedestrians	13.16	14.09	14.56	15.02	16.41	18.74	21.87
Building Areas Accessible to Pedestrians	14.16	15.09	15.56	16.02	17.41	19.74	22.87
Building Areas Accessible to Vehicles (not Trucks)	14.16	15.09	15.56	16.02	17.41	19.74	22.87
Building Areas Accessible to Trucks	19.16	20.09	20.56	21.02	22.41	24.74	27.87

Attachment 2: NESC and Entergy Clearance Requirements

Signs, Chimneys, Billboards, Radio and TV antennas, Flagpoles and Flags, Banners, Tanks with Catwalks	14.16	15.09	15.56	16.02	17.41	19.74	22.87
Signs, Chimneys, Billboards, Radio and TV antennas, Flagpoles and Flags, Banners, Tanks without Catwalks	8.66	9.59	10.06	10.52	11.91	14.24	17.37

RULE 234B, C & G - Horizontal Clearance to Various Structures with No Wind

	69	115	138	161	230	345	500
Lighting Supports	5.00	5.66	6.12	6.59	7.98	10.30	13.44
Traffic Signal Supports	5.00	5.66	6.12	6.59	7.98	10.30	13.44
Supporting Structures of Other Lines	5.00	5.66	6.12	6.59	7.98	10.30	13.44
Intermediate Poles in Skip Span Construction	5.00	5.66	6.12	6.59	7.98	10.30	13.44
Buildings	8.16	9.09	9.56	10.02	11.41	13.74	16.87
Signs, Chimneys, Billboards, Radio and TV Antennas, Flagpoles & Flags	8.16	9.09	9.56	10.02	11.41	13.74	16.87
Banners, Tanks	8.16	9.09	9.56	10.02	11.41	13.74	16.87

RULE 234B, C & G - Horizontal Clearance to Various Structures with Wind

	69	115	138	161	230	345	500
Lighting Supports	5.16	6.09	6.56	7.02	8.41	10.74	13.87
Traffic Signal Supports	5.16	6.09	6.56	7.02	8.41	10.74	13.87
Supporting Structures of Other Lines	5.16	6.09	6.56	7.02	8.41	10.74	13.87
Intermediate Poles in Skip Span Construction	5.16	6.09	6.56	7.02	8.41	10.74	13.87
Buildings	5.16	6.09	6.56	7.02	8.41	10.74	13.87
Signs, Chimneys, Billboards, Radio and TV Antennas, Flagpoles & Flags	5.16	6.09	6.56	7.02	8.41	10.74	13.87
Banners, Tanks	5.16	6.09	6.56	7.02	8.41	10.74	13.87

Attachment 2: NESC and Entergy Clearance Requirements

RULE 235B - Horizontal Clearance Between ~~wires~~Wires Supported on the Same Structure

	69	115	138	161	230	345	500
0	2.08	2.96	3.41	3.85	5.18	7.39	10.37
13.8	2.34	3.23	3.67	4.11	5.44	7.66	10.64
34.5	2.74	3.63	4.07	4.51	5.84	8.05	11.04
69	3.41	4.29	4.73	5.18	6.50	8.72	11.70
115	4.29	5.18	5.62	6.06	7.39	9.60	12.59
138	4.73	5.62	6.06	6.50	7.83	10.05	13.03
161	5.18	6.06	6.50	6.95	8.27	10.49	13.47
230	6.50	7.39	7.83	8.27	9.60	11.82	14.80
345	8.72	9.60	10.05	10.49	11.82	14.03	17.01
500	11.70	12.59	13.03	13.47	14.80	17.01	20.00

RULE 235C2b1 - Vertical Clearance Between Wires Supported at Different Levels on the Same Structures

	69	115	138	161	230	345	500
0	2.03	2.58	3.02	3.47	4.79	7.01	9.99
13.8	2.03	2.85	3.29	3.73	5.06	7.27	10.25
34.5	2.36	3.24	3.69	4.13	5.46	7.67	10.65
69	3.02	3.91	4.35	4.79	6.12	8.33	11.32
115	3.91	4.79	5.24	5.68	7.01	9.22	12.20
138	4.35	5.24	5.68	6.12	7.45	9.66	12.64
161	4.79	5.68	6.12	6.56	7.89	10.10	13.09
230	6.12	7.01	7.45	7.89	9.22	11.43	14.42
345	8.33	9.22	9.66	10.10	11.43	13.65	16.63
500	11.32	12.20	12.64	13.09	14.42	16.63	19.61

RULE 233B1 - Horizontal Clearance to Other Wires (With or without Wind)

	69	115	138	161	230	345	500
0	5.66	6.59	7.06	7.52	8.91	11.24	14.37
13.8	5.94	6.87	7.33	7.80	9.19	11.52	14.65
34.5	6.36	7.29	7.75	8.22	9.61	11.94	15.07
69	7.06	7.98	8.45	8.91	10.31	12.63	15.76
115	7.98	8.91	9.38	9.84	11.24	13.56	16.69
138	8.45	9.38	9.84	10.31	11.70	14.03	17.16
161	8.91	9.84	10.31	10.77	12.17	14.49	17.62
230	10.31	11.24	11.70	12.17	13.56	15.89	19.02
345	12.63	13.56	14.03	14.49	15.89	18.21	21.34
500	15.76	16.69	17.16	17.62	19.02	21.34	24.47

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Attachment 2: NESC and Entergy Clearance Requirements

Vertical Clearance Requirements; NESC 2012 & Entergy Design Clearance

	69 kV ⁽¹⁾		115/138/161 kV ⁽¹⁾		230 kV ⁽¹⁾		345 kV ⁽¹⁾		500 kV ⁽¹⁾ (3)	
	NESC ⁽²⁾ @ Max. Sag(ft.)	ETR @ Max. Sag(ft.)	NESC ⁽²⁾ @ Max. Sag(ft.)	ETR @ Max. Sag(ft.)	NESC ⁽²⁾ @ Max. Sag(ft.)	ETR @ Max. Sag(ft.)	NESC ⁽²⁾ @ Max. Sag(ft.)	ETR @ Max. Sag(ft.)	NESC ⁽²⁾ @ Max. Sag(ft.)	ETR @ Max. Sag(ft.)
Railroads	27.16	33.00	29.02	35.00	30.41	37.00	32.74	41.00	35.87	48.00
Roads	19.16	28.00	21.02	30.00	22.41	32.00	24.74	33.00	27.87	40.00
Other Land										
Traversed by any kind of Vehicle	19.16	24.00	21.02	26.00	22.41	28.00	24.74	33.00	27.87	40.00
Cultivated										
Farmland	19.16	27.00	21.02	29.00	22.41	31.00	24.74	33.00	27.87	40.00
Land accessible										
to pedestrians only	15.16	24.00	17.02	26.00	18.41	28.00	20.74	29.00	23.87	36.00
Water Areas Suitable for sailboats:										
Less than 20										
acres	21.16	24.00	23.02	26.00	24.41	28.00	26.74	35.00	29.87	42.00
20-200 acres	29.16	32.00	31.02	34.00	32.41	36.00	34.74	43.00	37.87	50.00
200-2000 acres	35.16	37.00	37.02	40.00	38.41	42.00	40.74	49.00	43.87	56.00
Over 2000 acres	41.16	44.00	43.02	46.00	44.41	48.00	46.74	55.00	49.87	62.00
Sailboat launch sites adjacent to water: Add 5.5'										
Less than 20										
acres	26.16	29.00	28.02	31.00	29.41	33.00	31.74	40.00	34.87	47.00
20-200 acres	34.16	37.00	36.02	39.00	37.41	41.00	39.74	48.00	42.87	53.00
200-2000 acres	40.16	43.00	42.02	45.00	43.41	47.00	45.74	54.00	48.87	61.00
Over 2000 acres	46.16	49.00	48.02	51.00	49.41	53.00	51.74	60.00	54.87	67.00
Other supply										
lines 34.5kV and under	2.66	8.00	4.52	10.00	5.91	15.00	8.24	17.00	11.85	23.00
Other supply lines:										
69 kV	4.06	10.00	5.91	11.00	7.31	16.00	9.63	18.00	13.25	20.00
115/138/161 kV	5.91	11.00	7.77	13.00	9.17	18.00	11.49	20.00	15.10	22.00
230 kV	7.31	16.00	9.17	18.00	10.56	20.00	12.89	22.00	16.50	24.00
345 kV	9.63	18.00	11.49	20.00	12.89	22.00	15.21	24.00	18.82	26.00
500 kV	13.25	20.00	15.10	22.00	16.50	24.00	18.82	26.00	22.44	28.00

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Attachment 2: NESC and Entergy Clearance Requirements

Guys, Neutrals and shield wires	2.66	8.00	4.52	10.00	5.91	15.00	8.24	17.00	11.85	19.00
Communication lines	5.66	10.00	7.52	12.00	8.91	15.00	11.24	17.00	14.37	19.00

Notes:

- (1) Conductor Temperature: 100°C for ACSR, see table 7.1(b) for other conductor types
- (2) NESC Vertical Clearance = Basic Clearance + Voltage Adder; Voltage Adder = 0.4"/kV in excess of 22kV; refer to 2012 NESC Clearance Calculations.
- (3) For 500 kV, the NESC clearance is approximately equal to the clearance requirements derived from a Switching Surge factor of 2.6.

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**~~ATTACHMENT 3 – QUICK ESTIMATING
CORONA LOSS CURVES~~**



Fig. 31—Quick-Estimating Corona-Loss Curves. Curves based on Peterson's formula with a few check points from the Carrol and Rockwell paper for comparison.

Attachment 2: NESC and Entergy Clearance Requirements

Attachment 2: NESC and Entergy Clearance Requirements

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Attachment

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~~Attachment 3: Quick Estimating Corona Loss Curves~~

~~Attachment 3: Quick Estimating Corona Loss Curves~~

ATTACHMENT 3
QUICK ESTIMATING CORONA LOSS CURVES

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Fig. 31—Quick-Estimating Carcone-Loes Curves. Curves based on Peterson's formula with a few check points from the Carrol and Rockwell paper for comparison.

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Attachment 4: Example ROW

ATTACHMENT 4 — **EXAMPLE**
EXAMPLE, **ROW**

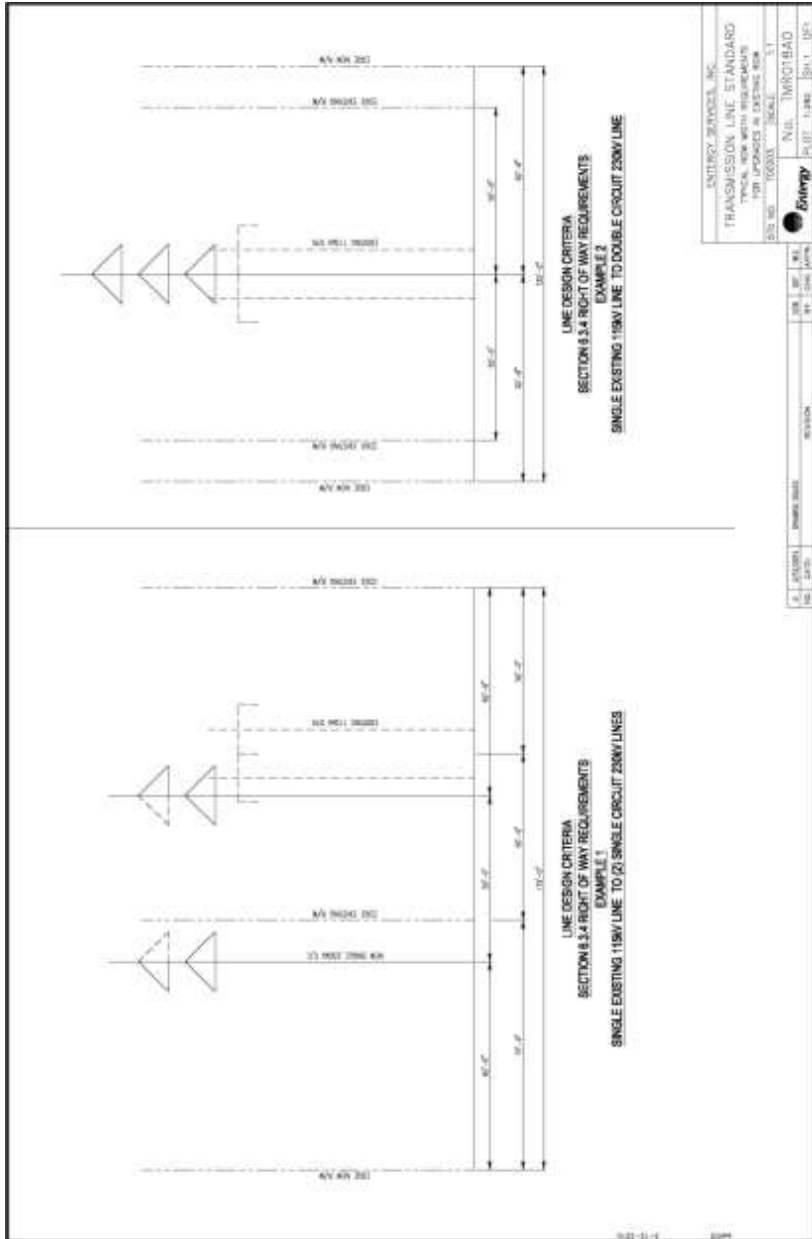
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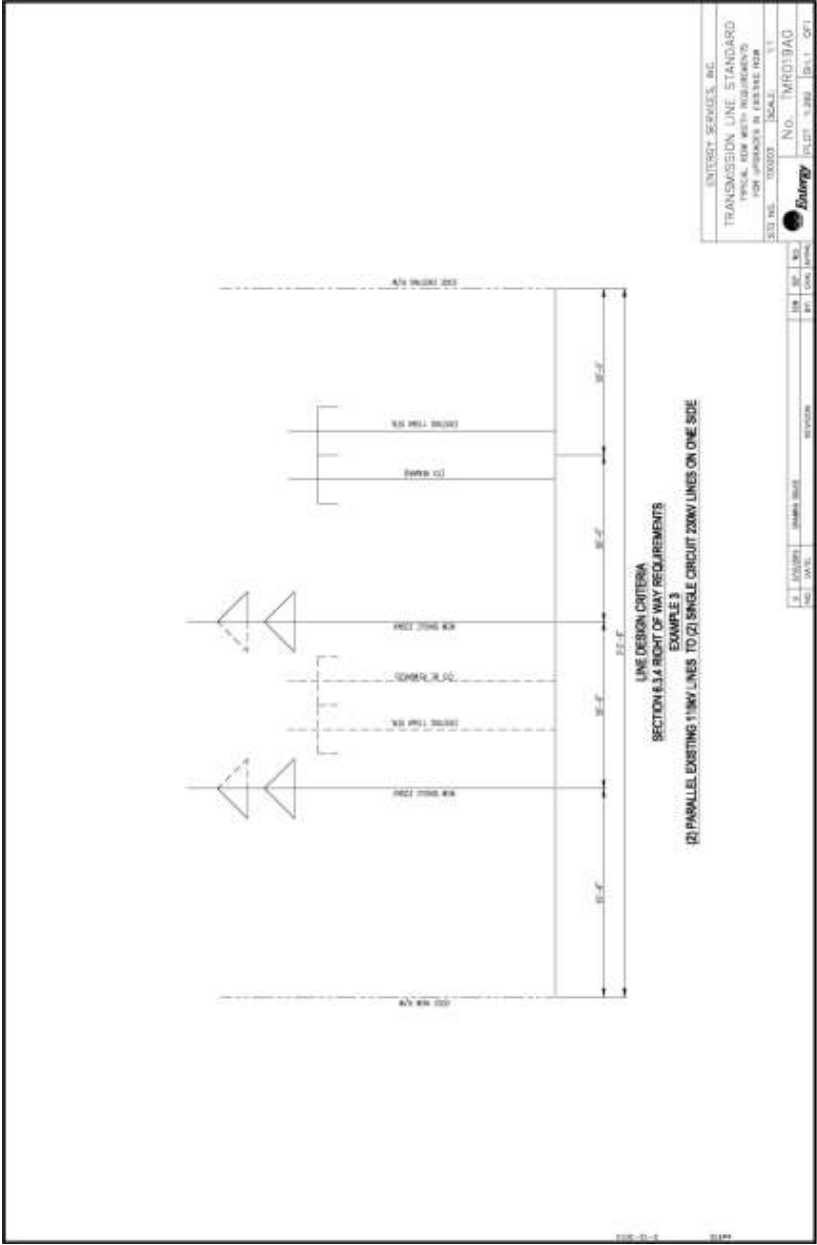
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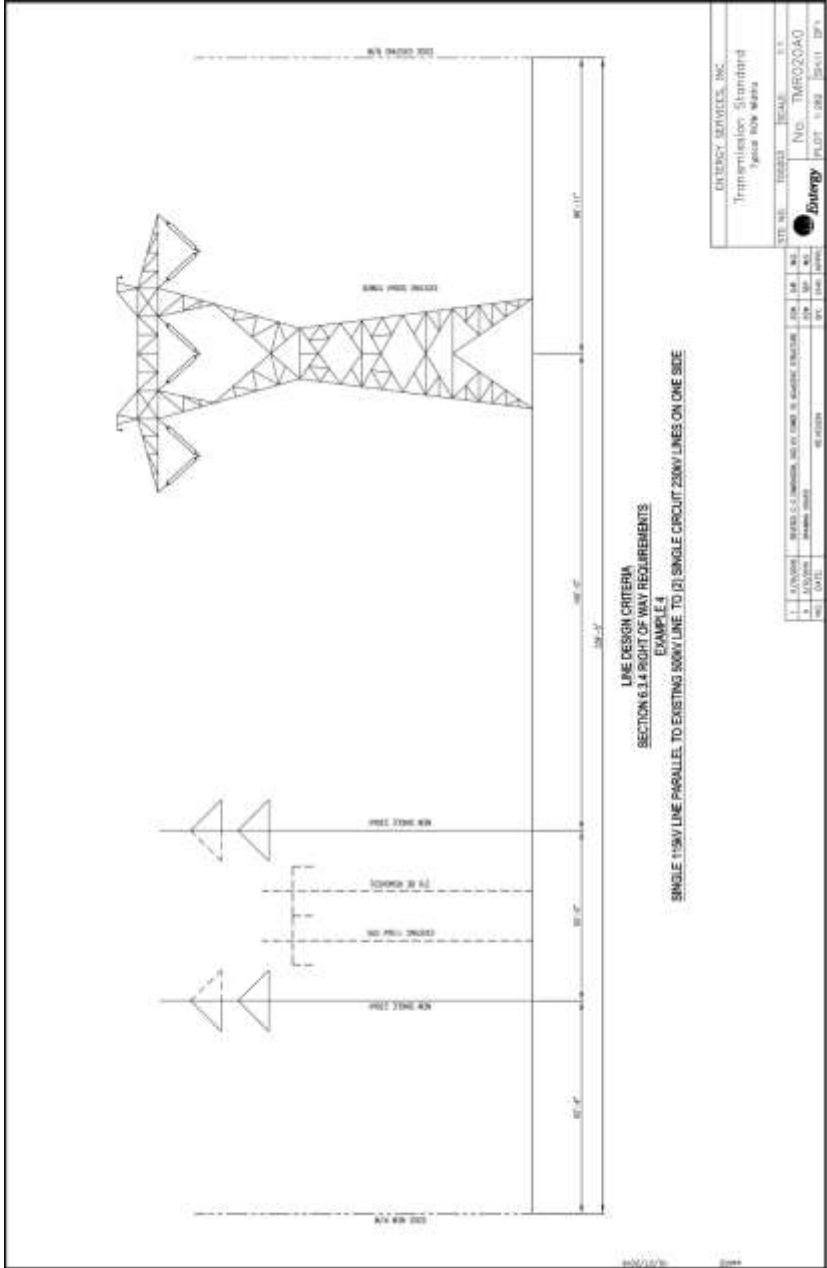
Attachment 4: Example ROW



Attachment 4: Example ROW



Attachment 4: Example ROW



Attachment 5: Approved Vendor List

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~~ATTACHMENT 5 – APPROVED VENDOR LIST~~

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Attachment 5: Approved Vendor List

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Attachment ~~5: Approved Vendor List~~4: Example ROW

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~~ATTACHMENT 6 – ENTERGY LOADING DISTRICTS~~

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Attachment 5: Approved Vendor List4: Example ROW

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State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
AR	Arkansas	100		M		1	LC-2
AR	Ashley	100		M		1	LC-2
AR	Baxter	100			H	1	LC-1
AR	Benton	100			H	1	LC-1
AR	Boone	100			H	1	LC-1
AR	Bradley	100		M		1	LC-2
AR	Calhoun	100		M		1	LC-2
AR	Carroll	100			H	1	LC-1
AR	Chicot	100		M		1	LC-2
AR	Clark	100			H	1	LC-1
AR	Clay	100			H	1	LC-1
AR	Cleburne	100			H	1	LC-1
AR	Cleveland	100		M		1	LC-2
AR	Columbia	100		M		1	LC-2
AR	Conway	100			H	1	LC-1
AR	Craighead	100		M		1	LC-2
AR	Crawford	100			H	1	LC-1
AR	Crittenden	100		M		1	LC-2
AR	Cross	100		M		1	LC-2
AR	Dallas	100		M		1	LC-2
AR	Desha	100		M		1	LC-2
AR	Drew	100		M		1	LC-2
AR	Faulkner	100			H	1	LC-1
AR	Franklin	100			H	1	LC-1
AR	Fulton	100			H	1	LC-1
AR	Garland	100			H	1	LC-1
AR	Grant	100		M		1	LC-2
AR	Greene	100			H	1	LC-1
AR	Hempstead	100			H	1	LC-1
AR	Hot Spring	100			H	1	LC-1
AR	Howard	100			H	1	LC-1
AR	Independence	100			H	1	LC-1
AR	Izard	100			H	1	LC-1
AR	Jackson	100			H	1	LC-1
AR	Jefferson	100		M		1	LC-2
AR	Johnson	100			H	1	LC-1
AR	Lafayette	100		M		1	LC-2
AR	Lawrence	100			H	1	LC-1
AR	Lee	100		M		1	LC-2
AR	Lincoln	100		M		1	LC-2
AR	Little River	100			H	1	LC-1
AR	Logan	100			H	1	LC-1
AR	Lonoke	100		M		1	LC-2

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Attachment 5: Approved Vendor List4: Example ROW

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State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
AR	Madison	100			H	1	LC-1
AR	Marion	100			H	1	LC-1
AR	Miller	100		M		1	LC-2
AR	Mississippi	100		M		1	LC-2
AR	Monroe	100		M		1	LC-2
AR	Montgomery	100			H	1	LC-1
AR	Nevada	100		M		1	LC-2
AR	Newton	100			H	1	LC-1
AR	Ouachita	100		M		1	LC-2
AR	Perry	100			H	1	LC-1
AR	Phillips	100		M		1	LC-2
AR	Pike	100			H	1	LC-1
AR	Poinsett	100		M		1	LC-2
AR	Polk	100			H	1	LC-1
AR	Pope	100			H	1	LC-1
AR	Prairie	100		M		1	LC-2
AR	Pulaski	100			H	1	LC-1
AR	Randolph	100			H	1	LC-1
AR	St. Francis	100		M		1	LC-2
AR	Saline	100			H	1	LC-1
AR	Scott	100			H	1	LC-1
AR	Searcy	100			H	1	LC-1
AR	Sebastian	100			H	1	LC-1
AR	Sevier	100			H	1	LC-1
AR	Sharp	100			H	1	LC-1
AR	Stone	100			H	1	LC-1
AR	Union	100		M		1	LC-2
AR	Van Buren	100			H	1	LC-1
AR	Washington	100			H	1	LC-1
AR	White	100			H	1	LC-1
AR	Woodruff	100		M		1	LC-2
AR	Yell	100			H	1	LC-1
MO	Dunklin	100			H	1	LC-1
MO	New Madrid	100			H	1	LC-1
MO	Oregon	100			H	1	LC-1
MO	Pemiscot	100			H	1	LC-1
MO	Stoddard	100			H	1	LC-1
MO	Taney	100			H	1	LC-1

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Attachment 5: Approved Vendor List4: Example ROW

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State	Parish	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
LA	Acadia	140	L			0.5	LC-3
LA	Allen	110	L			0.5	LC-3F
LA	Ascension	140	L			0.5	LC-3
LA	Assumption	140	L			0.5	LC-3
LA	Avoyelles	110	L			0.5	LC-3F
LA	Beauregard	110	L			0.5	LC-3F
LA	Bienville	100		M		0.75	LC-2D
LA	Bossier	100		M		0.75	LC-2D
LA	Calcasieu	140	L			0.5	LC-3
LA	Caldwell	100		M		0.75	LC-2D
LA	Cameron	140	L			0.5	LC-3
LA	Catahoula	100	L			0.5	LC-3E
LA	Claiborne	100		M		0.75	LC-2D
LA	Concordia	100	L			0.5	LC-3E
LA	Desoto	100		M		0.75	LC-2D
LA	East Baton Rouge	140	L			0.5	LC-3
LA	East Carrol	100		M		0.75	LC-2D
LA	East Feliciana	110	L			0.5	LC-3F
LA	Evangeline	110	L			0.5	LC-3F
LA	Franklin	100		M		0.75	LC-2D
LA	Grant	100	L			0.75	LC-2C
LA	Iberia	140	L			0.5	LC-3
LA	Iberville	140	L			0.5	LC-3
LA	Jackson	100		M		0.75	LC-2D
LA	Jefferson	150	L			0.5	LC-3D
LA	Jefferson Davis	140	L			0.5	LC-3
LA	Lafayette	140	L			0.5	LC-3
LA	Lafourche	150	L			0.5	LC-3D
LA	Lasalle	100	L			0.75	LC-3C
LA	Lincoln	100		M		0.75	LC-2D
LA	Livingston	125	L			0.5	LC-3B
LA	Madison	100	L			0.75	LC-3C
LA	Morehouse	100		M		0.75	LC-2D
LA	Natchitoches	100		M		0.75	LC-2D
LA	Orleans	140	L			0.5	LC-3
LA	Ouachita	100		M		0.75	LC-2D
LA	Plaquemines	150	L			0.5	LC-3D
LA	Point Coupee	110	L			0.5	LC-3F
LA	Rapides	100	L			0.5	LC-3E
LA	Red River	100		M		0.75	LC-2D
LA	Richland	100		M		0.75	LC-2D
LA	Sabine	100		M		0.75	LC-2D
LA	St. Bernard	150	L			0.5	LC-3D
LA	St. Charles	140	L			0.5	LC-3

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Attachment 5: Approved Vendor List4: Example ROW

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State	Parish	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
LA	St. Helena	110	L			0.5	LC-3F
LA	St. James	140	L			0.5	LC-3
LA	St. John the Baptist	140	L			0.5	LC-3
LA	St. Landry	110	L			0.5	LC-3F
LA	St. Martin, North	140	L			0.5	LC-3
LA	St. Martin, South	140	L			0.5	LC-3
LA	St. Mary	140	L			0.5	LC-3
LA	St. Tammany	140	L			0.5	LC-3
LA	Tangipahoa	125	L			0.5	LC-3B
LA	Tensas	100	L			0.5	LC-3E
LA	Terrebonne	150	L			0.5	LC-3D
LA	Union	100		M		0.75	LC-2D
LA	Vermillion	140	L			0.5	LC-3
LA	Vernon	100	L			0.5	LC-3E
LA	Washington	125	L			0.5	LC-3B
LA	Webster	100		M		0.75	LC-2D
LA	West Baton Rouge	140	L			0.5	LC-3
LA	West Carrol	100		M		0.75	LC-2D
LA	West Feliciana	110	L			0.5	LC-3F
LA	Winn	100		M		0.75	LC-2D

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State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Energy Load Case
			Light	Medium	Heavy		
MS	Adams	100	L			0.5	LC-3E
MS	Amite	110	L			0.5	LC-3F
MS	Attala	100	L			0.5	LC-3E
MS	Benton	100		M		1	LC-2
MS	Bolivar	100		M		1	LC-2
MS	Calhoun	100		M		1	LC-2
MS	Carroll	100		M		1	LC-2
MS	Chickasaw	100		M		1	LC-2
MS	Choctaw	100		M		1	LC-2
MS	Clairborne	100	L			0.5	LC-3E
MS	Clay	100		M		1	LC-2
MS	Coahoma	100		M		1	LC-2
MS	Copiah	100	L			0.5	LC-3E
MS	Covington	110	L			0.5	LC-3F
MS	Desoto	100		M		1	LC-2
MS	Franklin	100	L			0.5	LC-3E
MS	Grenada	100		M		1	LC-2
MS	Hinds	100	L			0.5	LC-3E
MS	Holmes	100		M		1	LC-2
MS	Humphreys	100		M		1	LC-2
MS	Issaquena	100	L			1	LC-3G
MS	Jefferson	100	L			0.5	LC-3E
MS	Jefferson Davis	110	L			0.5	LC-3F
MS	Lafayette	100		M		1	LC-2
MS	Lawrence	110	L			0.5	LC-3F
MS	Leake	100	L			0.5	LC-3E
MS	Leflore	100		M		1	LC-2
MS	Lincoln	110	L			0.5	LC-3F
MS	Madison	100	L			0.5	LC-3E
MS	Marion	110	L			0.5	LC-3F
MS	Marshall	100		M		1	LC-2
MS	Montgomery	100		M		1	LC-2
MS	Neshoba	100	L			0.5	LC-3E
MS	Newton	100	L			0.5	LC-3E
MS	Panola	100		M		1	LC-2
MS	Pike	110	L			0.5	LC-3F
MS	Pontotoc	100		M		1	LC-2
MS	Quitman	100		M		1	LC-2
MS	Rankin	100	L			0.5	LC-3E
MS	Scott	100	L			0.5	LC-3E
MS	Sharkey	100	L			0.75	LC-3C
MS	Simpson	100	L			0.5	LC-3E
MS	Smith	110	L			0.5	LC-3F

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Attachment 5: Approved Vendor List4: Example ROW

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State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
MS	Sunflower	100		M		1	LC-2
MS	Tallahatchie	100		M		1	LC-2
MS	Tate	100		M		1	LC-2
MS	Tippah	100		M		1	LC-2
MS	Tunica	100		M		1	LC-2
MS	Union	100		M		1	LC-2
MS	Walthall	110	L			0.5	LC-3F
MS	Warren	100	L			0.5	LC-3E
MS	Washington	100		M		1	LC-2
MS	Webster	100		M		1	LC-2
MS	Wilkinson	110	L			0.5	LC-3F
MS	Winston	100	L			0.5	LC-3E
MS	Yalobusha	100		M		1	LC-2
MS	Yazoo	100	L			0.75	LC-3C

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Attachment 5: Approved Vendor List4: Example ROW

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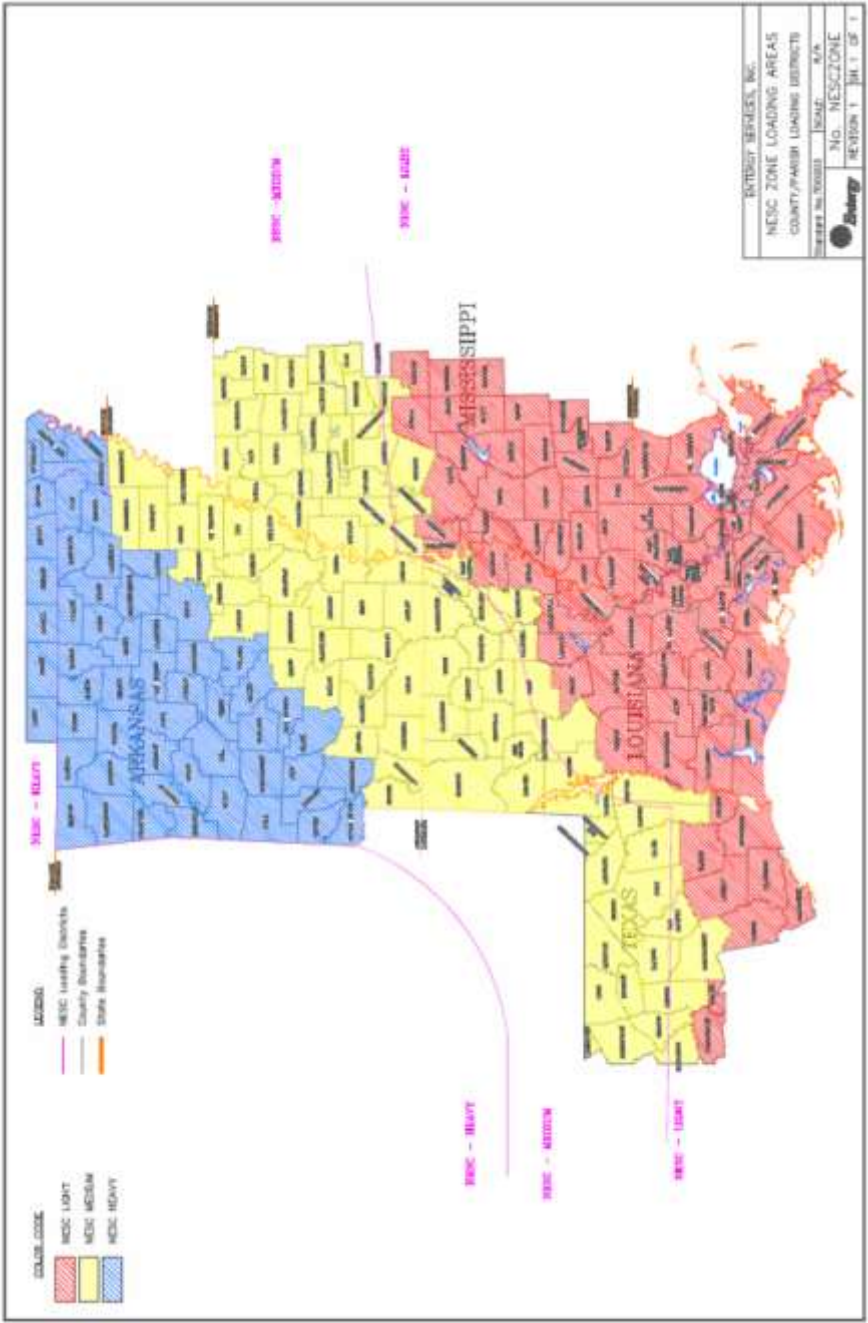
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State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
TX	Angelina	100		M		0.75	LC-2D
TX	Brazos	100		M		0.75	LC-2D
TX	Burleson	100		M		0.5	LC-2B
TX	Chambers	140	L			0.5	LC-3
TX	Galveston	140	L			0.5	LC-3
TX	Grimes	100		M		0.75	LC-2D
TX	Hardin	125	L			0.5	LC-3B
TX	Harris	125	L			0.5	LC-3B
TX	Houston	100		M		0.75	LC-2D
TX	Jasper	125		M		0.5	LC-2C
TX	Jefferson	140	L			0.5	LC-3
TX	Leon	100		M		0.75	LC-2D
TX	Liberty	125	L			0.5	LC-3B
TX	Limestone	100		M		0.75	LC-2D
TX	Madison	100		M		0.75	LC-2D
TX	Montgomery	110		M		0.5	LC-2A
TX	Nacogdoches	100		M		0.75	LC-2D
TX	Newton	125		M		0.5	LC-2C
TX	Orange	140	L			0.5	LC-3
TX	Polk	110		M		0.75	LC-2E
TX	Robertson	100		M		0.75	LC-2D
TX	Sabine	100		M		0.75	LC-2D
TX	San Augustine	100		M		0.75	LC-2D
TX	San Jacinto	100		M		0.75	LC-2D
TX	Trinity	100		M		0.75	LC-2D
TX	Tyler	110		M		0.75	LC-2E
TX	Walker	100		M		0.75	LC-2D
TX	Waller	110	L			0.5	LC-3F
TX	Washington	100	L			0.5	LC-3E

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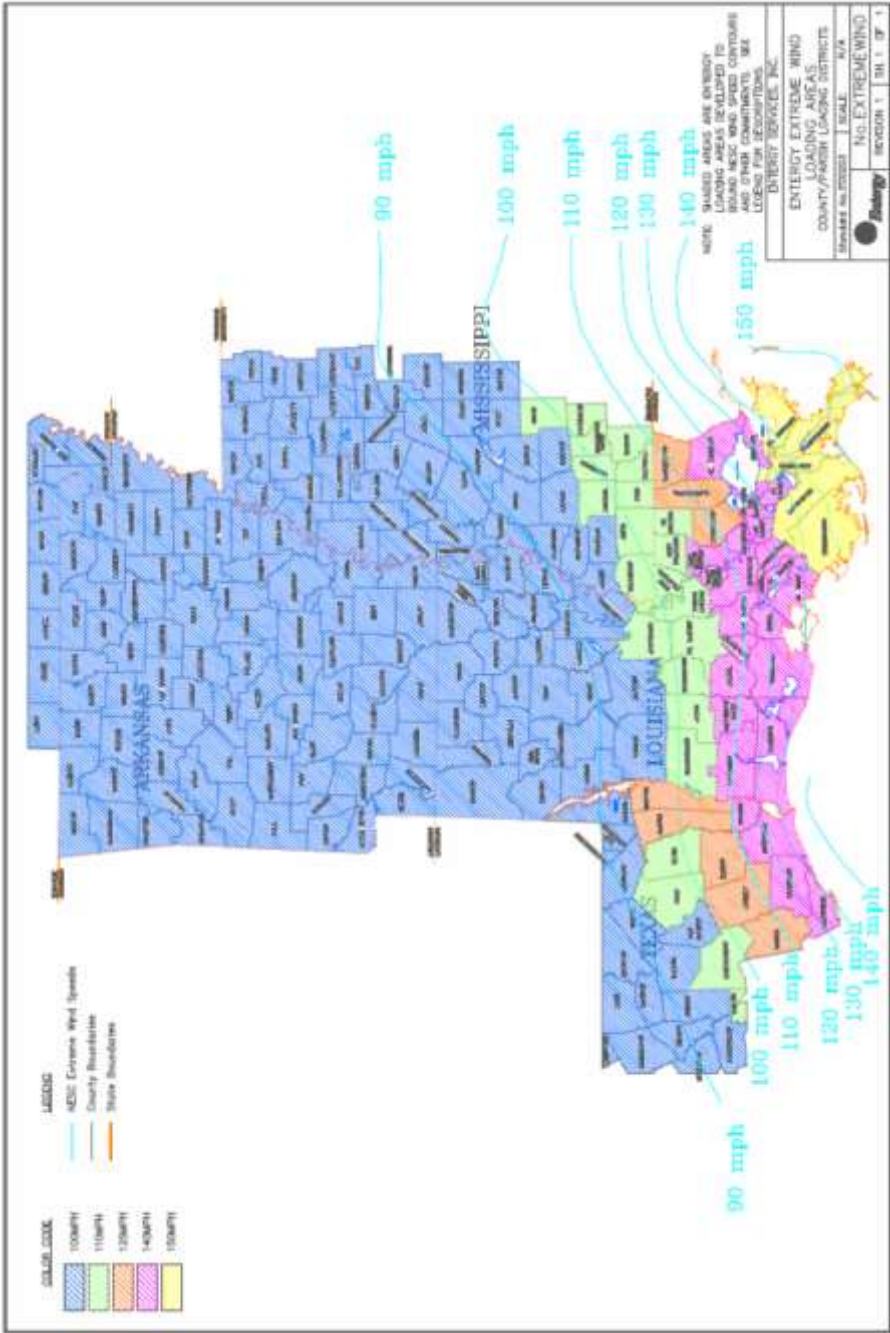
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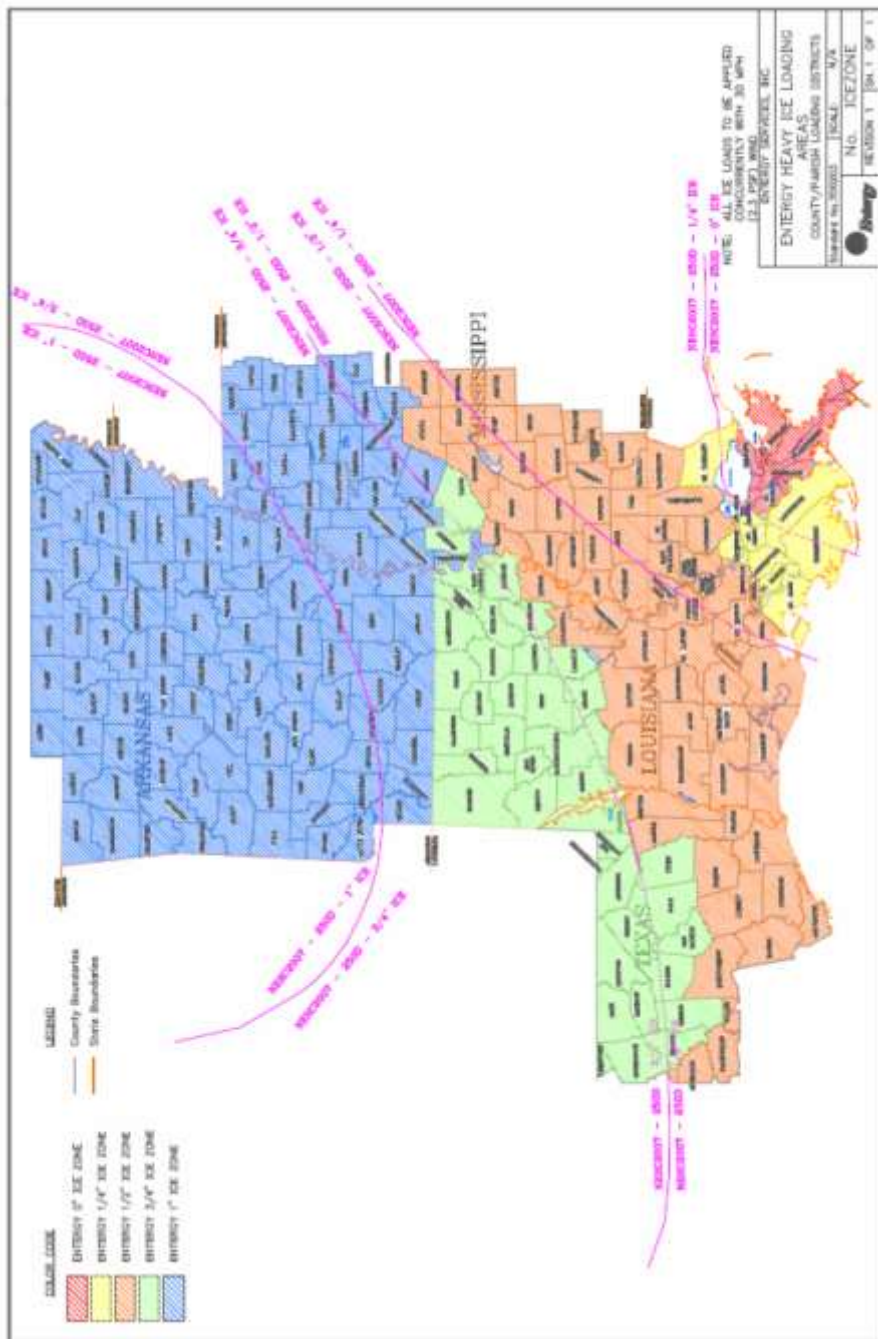
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~~Attachment 5: Approved Vendor List~~4: Example ROW



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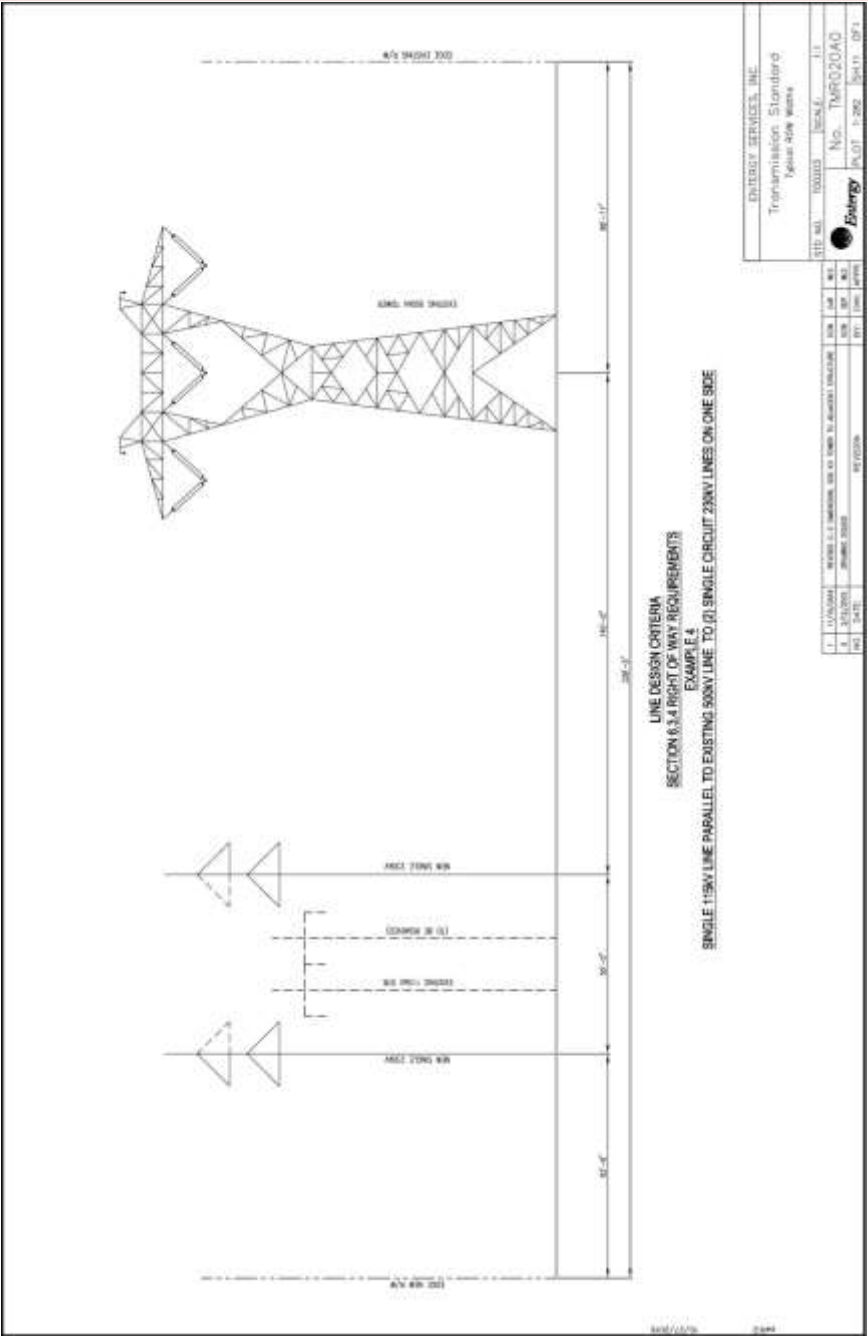
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ATTACHMENT 6

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Attachment 6: Entergy Loading Districts

ENTERGY LOADING DISTRICTS

State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
AR	Arkansas	100		M		1	LC-2
AR	Ashley	100		M		1	LC-2
AR	Baxter	100			H	1	LC-1
AR	Benton	100			H	1	LC-1
AR	Boone	100			H	1	LC-1
AR	Bradley	100		M		1	LC-2
AR	Calhoun	100		M		1	LC-2
AR	Carroll	100			H	1	LC-1
AR	Chicot	100		M		1	LC-2
AR	Clark	100			H	1	LC-1
AR	Clay	100			H	1	LC-1
AR	Cleburne	100			H	1	LC-1
AR	Cleveland	100		M		1	LC-2
AR	Columbia	100		M		1	LC-2
AR	Conway	100			H	1	LC-1
AR	Craighead	100		M		1	LC-2
AR	Crawford	100			H	1	LC-1
AR	Crittenden	100		M		1	LC-2
AR	Cross	100		M		1	LC-2
AR	Dallas	100		M		1	LC-2
AR	Desha	100		M		1	LC-2
AR	Drew	100		M		1	LC-2
AR	Faulkner	100			H	1	LC-1
AR	Franklin	100			H	1	LC-1
AR	Fulton	100			H	1	LC-1
AR	Garland	100			H	1	LC-1
AR	Grant	100		M		1	LC-2
AR	Greene	100			H	1	LC-1
AR	Hempstead	100			H	1	LC-1
AR	Hot Spring	100			H	1	LC-1
AR	Howard	100			H	1	LC-1
AR	Independence	100			H	1	LC-1
AR	Izard	100			H	1	LC-1
AR	Jackson	100			H	1	LC-1
AR	Jefferson	100		M		1	LC-2
AR	Johnson	100			H	1	LC-1
AR	Lafayette	100		M		1	LC-2
AR	Lawrence	100			H	1	LC-1
AR	Lee	100		M		1	LC-2
AR	Lincoln	100		M		1	LC-2
AR	Little River	100			H	1	LC-1
AR	Logan	100			H	1	LC-1
AR	Lonoke	100		M		1	LC-2

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Attachment 6: Entergy Loading Districts

State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
AR	Madison	100			H	1	LC-1
AR	Marion	100			H	1	LC-1
AR	Miller	100		M		1	LC-2
AR	Mississippi	100		M		1	LC-2
AR	Monroe	100		M		1	LC-2
AR	Montgomery	100			H	1	LC-1
AR	Nevada	100		M		1	LC-2
AR	Newton	100			H	1	LC-1
AR	Ouachita	100		M		1	LC-2
AR	Perry	100			H	1	LC-1
AR	Phillips	100		M		1	LC-2
AR	Pike	100			H	1	LC-1
AR	Poinsett	100		M		1	LC-2
AR	Polk	100			H	1	LC-1
AR	Pope	100			H	1	LC-1
AR	Prairie	100		M		1	LC-2
AR	Pulaski	100			H	1	LC-1
AR	Randolph	100			H	1	LC-1
AR	St. Francis	100		M		1	LC-2
AR	Saline	100			H	1	LC-1
AR	Scott	100			H	1	LC-1
AR	Searcy	100			H	1	LC-1
AR	Sebastian	100			H	1	LC-1
AR	Sevier	100			H	1	LC-1
AR	Sharp	100			H	1	LC-1
AR	Stone	100			H	1	LC-1
AR	Union	100		M		1	LC-2
AR	Van Buren	100			H	1	LC-1
AR	Washington	100			H	1	LC-1
AR	White	100			H	1	LC-1
AR	Woodruff	100		M		1	LC-2
AR	Yell	100			H	1	LC-1
MO	Dunklin	100			H	1	LC-1
MO	New Madrid	100			H	1	LC-1
MO	Oregon	100			H	1	LC-1
MO	Penasco	100			H	1	LC-1
MO	Stoddard	100			H	1	LC-1
MO	Taney	100			H	1	LC-1

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Attachment 6: Entergy Loading Districts

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State	Parish	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
LA	Acadia	140	L			0.5	LC-3
LA	Allen	110	L			0.5	LC-3F
LA	Ascension	140	L			0.5	LC-3
LA	Assumption	140	L			0.5	LC-3
LA	Avoyelles	110	L			0.5	LC-3F
LA	Beauregard	110	L			0.5	LC-3F
LA	Bienville	100		M		0.75	LC-2D
LA	Bossier	100		M		0.75	LC-2D
LA	Calcasieu	140	L			0.5	LC-3
LA	Caldwell	100		M		0.75	LC-2D
LA	Cameron	140	L			0.5	LC-3
LA	Catahoula	100	L			0.5	LC-3E
LA	Claiborne	100		M		0.75	LC-2D
LA	Concordia	100	L			0.5	LC-3E
LA	Desoto	100		M		0.75	LC-2D
LA	East Baton Rouge	140	L			0.5	LC-3
LA	East Carrol	100		M		0.75	LC-2D
LA	East Feliciana	110	L			0.5	LC-3F
LA	Evangeline	110	L			0.5	LC-3F
LA	Franklin	100		M		0.75	LC-2D
LA	Grant	100	L			0.75	LC-2C
LA	Iberia	140	L			0.5	LC-3
LA	Iberville	140	L			0.5	LC-3
LA	Jackson	100		M		0.75	LC-2D
LA	Jefferson	150	L			0.5	LC-3D
LA	Jefferson Davis	140	L			0.5	LC-3
LA	Lafayette	140	L			0.5	LC-3
LA	Lafourche	150	L			0.5	LC-3D
LA	Lasalle	100	L			0.75	LC-3C
LA	Lincoln	100		M		0.75	LC-2D
LA	Livingston	125	L			0.5	LC-3B
LA	Madison	100	L			0.75	LC-3C
LA	Morehouse	100		M		0.75	LC-2D
LA	Natchitoches	100		M		0.75	LC-2D
LA	Orleans	140	L			0.5	LC-3
LA	Ouachita	100		M		0.75	LC-2D
LA	Plaquemines	150	L			0.5	LC-3D
LA	Point Coupee	110	L			0.5	LC-3F
LA	Rapides	100	L			0.5	LC-3E
LA	Red River	100		M		0.75	LC-2D
LA	Richland	100		M		0.75	LC-2D
LA	Sabine	100		M		0.75	LC-2D
LA	St. Bernard	150	L			0.5	LC-3D
LA	St. Charles	140	L			0.5	LC-3

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Attachment 6: Entergy Loading Districts

State	Parish	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
LA	St. Helena	110	L			0.5	LC-3F
LA	St. James	140	L			0.5	LC-3
LA	St. John the Baptist	140	L			0.5	LC-3
LA	St. Landry	110	L			0.5	LC-3F
LA	St. Martin, North	140	L			0.5	LC-3
LA	St. Martin, South	140	L			0.5	LC-3
LA	St. Mary	140	L			0.5	LC-3
LA	St. Tammany	140	L			0.5	LC-3
LA	Tangipahoa	125	L			0.5	LC-3B
LA	Tensas	100	L			0.5	LC-3E
LA	Terrebonne	150	L			0.5	LC-3D
LA	Union	100		M		0.75	LC-2D
LA	Vermilion	140	L			0.5	LC-3
LA	Vernon	100	L			0.5	LC-3E
LA	Washington	125	L			0.5	LC-3B
LA	Webster	100		M		0.75	LC-2D
LA	West Baton Rouge	140	L			0.5	LC-3
LA	West Carrol	100		M		0.75	LC-2D
LA	West Feliciana	110	L			0.5	LC-3F
LA	Winn	100		M		0.75	LC-2D

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Attachment 6: Entergy Loading Districts

State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
MS	Adams	100	L			0.5	LC-3E
MS	Amite	110	L			0.5	LC-3F
MS	Attala	100	L			0.5	LC-3E
MS	Benton	100		M		1	LC-2
MS	Bolivar	100		M		1	LC-2
MS	Calhoun	100		M		1	LC-2
MS	Carroll	100		M		1	LC-2
MS	Chickasaw	100		M		1	LC-2
MS	Choctaw	100		M		1	LC-2
MS	Clatborne	100	L			0.5	LC-3E
MS	Clay	100		M		1	LC-2
MS	Coahoma	100		M		1	LC-2
MS	Copiah	100	L			0.5	LC-3E
MS	Covington	110	L			0.5	LC-3F
MS	Desoto	100		M		1	LC-2
MS	Franklin	100	L			0.5	LC-3E
MS	Grenada	100		M		1	LC-2
MS	Hinds	100	L			0.5	LC-3E
MS	Holmes	100		M		1	LC-2
MS	Humphreys	100		M		1	LC-2
MS	Issaquena	100	L			1	LC-3G
MS	Jefferson	100	L			0.5	LC-3E
MS	Jefferson Davis	110	L			0.5	LC-3F
MS	Lafayette	100		M		1	LC-2
MS	Lawrence	110	L			0.5	LC-3F
MS	Leake	100	L			0.5	LC-3E
MS	Leflore	100		M		1	LC-2
MS	Lincoln	110	L			0.5	LC-3F
MS	Madison	100	L			0.5	LC-3E
MS	Marion	110	L			0.5	LC-3F
MS	Marshall	100		M		1	LC-2
MS	Montgomery	100		M		1	LC-2
MS	Neshoba	100	L			0.5	LC-3E
MS	Newton	100	L			0.5	LC-3E
MS	Panola	100		M		1	LC-2
MS	Pike	110	L			0.5	LC-3F
MS	Pontotoc	100		M		1	LC-2
MS	Quitman	100		M		1	LC-2
MS	Rankin	100	L			0.5	LC-3E
MS	Scott	100	L			0.5	LC-3E
MS	Sharkey	100	L			0.75	LC-3C
MS	Simpson	100	L			0.5	LC-3E
MS	Smith	110	L			0.5	LC-3F

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Attachment 6: Entergy Loading Districts

State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
MS	Sunflower	100		M		1	LC-2
MS	Tallahatchie	100		M		1	LC-2
MS	Tate	100		M		1	LC-2
MS	Tippah	100		M		1	LC-2
MS	Tunica	100		M		1	LC-2
MS	Union	100		M		1	LC-2
MS	Walthall	110	L			0.5	LC-3F
MS	Warren	100	L			0.5	LC-3E
MS	Washington	100		M		1	LC-2
MS	Webster	100		M		1	LC-2
MS	Wilkinson	110	L			0.5	LC-3F
MS	Winston	100	L			0.5	LC-3E
MS	Yalobusha	100		M		1	LC-2
MS	Yazoo	100	L			0.75	LC-3C

State	County	Extreme Wind mph	NESC District			Extreme Ice inches	Entergy Load Case
			Light	Medium	Heavy		
TX	Angelina	100		M		0.75	LC-2D
TX	Brazos	100		M		0.75	LC-2D
TX	Burleson	100		M		0.5	LC-2B
TX	Chambers	140	L			0.5	LC-3
TX	Galveston	140	L			0.5	LC-3
TX	Grimes	100		M		0.75	LC-2D
TX	Hardin	125	L			0.5	LC-3B
TX	Harris	125	L			0.5	LC-3B
TX	Houston	100		M		0.75	LC-2D
TX	Jasper	125		M		0.5	LC-2C
TX	Jefferson	140	L			0.5	LC-3
TX	Leon	100		M		0.75	LC-2D
TX	Liberty	125	L			0.5	LC-3B
TX	Limestone	100		M		0.75	LC-2D
TX	Madison	100		M		0.75	LC-2D
TX	Montgomery	110		M		0.5	LC-2A
TX	Nacogdoches	100		M		0.75	LC-2D
TX	Newton	125		M		0.5	LC-2C
TX	Orange	140	L			0.5	LC-3
TX	Polk	110		M		0.75	LC-2E
TX	Robertson	100		M		0.75	LC-2D
TX	Sabine	100		M		0.75	LC-2D
TX	San Augustine	100		M		0.75	LC-2D
TX	San Jacinto	100		M		0.75	LC-2D
TX	Trinity	100		M		0.75	LC-2D
TX	Tyler	110		M		0.75	LC-2E
TX	Walker	100		M		0.75	LC-2D
TX	Waller	110	L			0.5	LC-3F
TX	Washington	100	L			0.5	LC-3E

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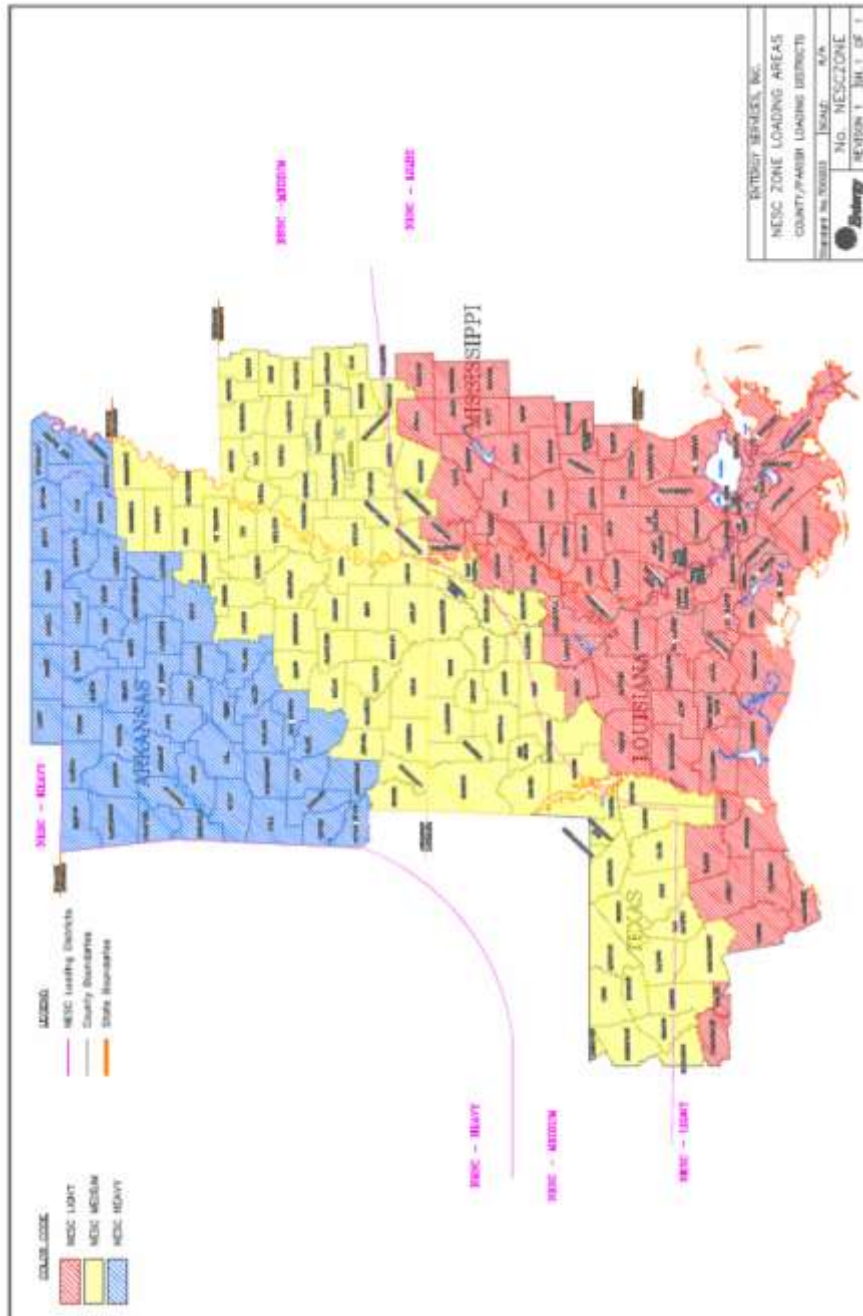
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Attachment 6: Entergy Loading Districts



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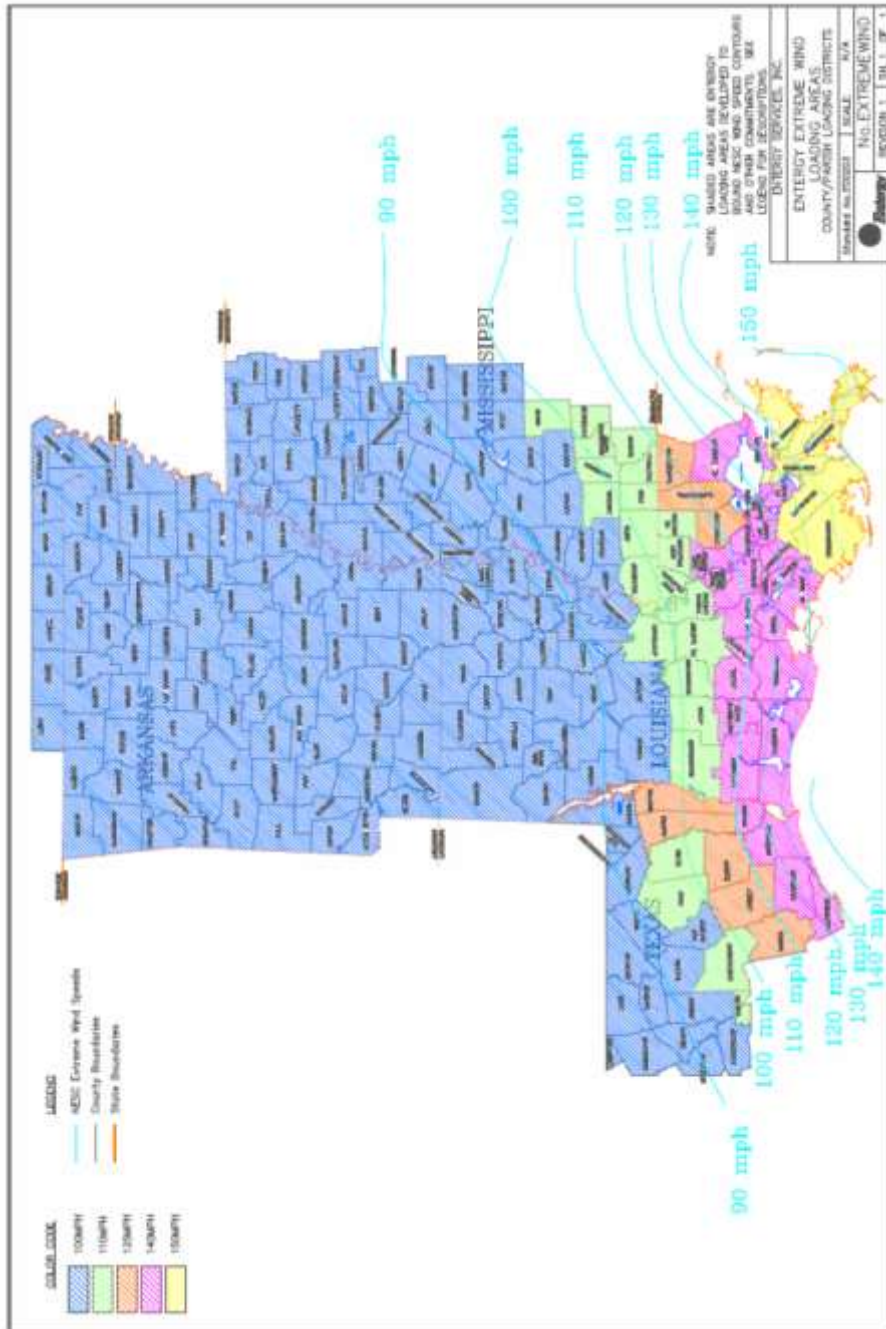
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PROPRIETARY, CONFIDENTIAL, OR PRIVILEGED INFORMATION

Attachment 6: Entergy Loading Districts



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PROPRIETARY, CONFIDENTIAL, OR PRIVILEGED INFORMATION

***** END OF APPENDIX 10 *****

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